

APPENDIX Q

BLASTING IMPACT ASSESSMENT REPORT



BLASTING IMPACT ASSESSMENT: FUTURE BLASTING OPERATIONS AT THE MOOSE RIVER OPEN PIT GOLD MINE DEVELOPMENT SITE

**TOUQUOY GOLD PROJECT
MOOSE RIVER, HALIFAX COUNTY, NOVA SCOTIA**

**Prepared For:
DDV Gold Limited**

**Prepared by:
Conestoga-Rovers
& Associates**

651 Colby Drive
Waterloo, Ontario
Canada N2V 1C2

Office: (519) 884-0510
Fax: (519) 884-0525

web: <http://www.CRAworld.com>

**OCTOBER 2007
REF. NO. 820933 (6)**

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1.0 INTRODUCTION

Conestoga-Rovers & Associates (CRA) has undertaken an Environmental Impact Assessment (Assessment) of the future blasting operations at the Touquoy Gold Project at the Moose River Gold Mines development (Site) in Halifax County, Nova Scotia. The mine will be operated by DDV Gold Limited (DDV).

The Assessment presented herein provides an evaluation of the potential air blast overpressure and ground vibration impacts from the proposed blasting operations within the open pit mine on sensitive receptors located nearest to the Site. The Assessment was prepared consistent with the Nova Scotia Department of Environment and Labour (NSDEL) *Pit and Quarry Guidelines* (1999).

2.0 SITE DESCRIPTION

The Facility is located at Moose River Gold Mines in Halifax County. The proposed surface footprint of the Site is approximately 300 ha and encompasses the settlement of Moose River Gold Mines, part of a small provincial park and undeveloped forest. It is bounded to the west by the Moose River and surrounded on all other sides by forested land in varying degrees of re-growth due to logging. A Site Plan identifying the surrounding land use is provided as Figure 1.

2.1 SENSITIVE RECEPTORS

All existing residential buildings on the Site have been purchased by DDV, or are in the process of being acquired. Construction will not move forward until all of the lands are under the ownership of DDV. At that time, the nearest receptor will be a point in Scraggy Lake 1,880 metres (m) southeast of the open pit mine, where a camper may be located on a short-term basis. Additional receptors include a children's overnight camp and a residence located approximately 4.3 kilometres (km) and 5 km, respectively, northwest of the open pit mine.

The NSDEL specifies that no blasting operations shall occur within:

- 30 m of the boundary of any public or common highway;
- 30 m of the bank of any watercourse or the ordinary high water mark;
- 800 m of the foundation or base of a structure located off site; or
- 15 m of the property boundary when a structure on the abutting property is not involved.

Based on the Site Plan provided as Figure 1, it can be seen that the open pit mine (where all blasting occurs) is suitably sited to ensure that the above minimum separation distances are maintained.

3.0

QUARRY BLASTING OPERATIONS AND MONITORING

3.1 BLAST DESIGN

The following table summarizes the blast design proposed at the Site:

| | |
|----------------------------|-----------------------|
| Holes per blast | 100 |
| Explosives (ANFO) per hole | 51.7 kg |
| Holes per delay | 4 |
| Blast frequency | 1 blast/day Mon - Fri |

The NSDEL *Pit and Quarry Guidelines* (1999) specifies that no blasting shall occur on Sunday, a statutory holiday prescribed by the Province, or on any day between the hours of 1800 hours and 0800 hours.

3.2 BLAST MONITOR DATA

There is no historic seismograph information available for this Site.

4.0 EFFECTS AND IMPACTS OF BLASTING OPERATIONS

4.1 GROUND VIBRATION

Ground vibration caused by blasting operations is defined as the speed of excitation of particles within the ground resulting from vibratory motion. The intensity of ground vibrations is measured in units of peak particle velocity. The unit of peak particle velocity is generally measured in millimetres per second (mm/s).

When explosives detonate in a borehole, shock waves (energy from the detonation) radiate outward from the borehole and crush the material adjacent to the borehole. Energy not used in the fracturing and displacement of bedrock dissipates in the form of ground and air vibrations (concussion). Under typical conditions, the blasting vibration intensity diminishes with distance, at a rate of about one third of its previous value each time the distance from the vibration source is doubled.

Some of the factors and parameters that affect the proper fragmentation of the rock and the impacts of blasting include:

- The explosive type, loading densities and weights;
- The detonator delays and firing sequence;
- The decking lengths;
- The spacing of holes;
- The distance between the holes and the free or open face;
- The geology (type and condition) of the bedrock and
- The depth and composition of the earth covering deposit (soil).

The NSDEL *Pit and Quarry Guidelines* provides a maximum peak particle velocity of 12.5 mm/s measured below grade or less than 1 m above grade in any part of the nearest structure not located on the property where the blasting occurs.

Ground vibration is estimated for a specific location using the following equation:

$$PPV = \beta (SD)^\alpha \quad (1)$$

Where:

PPV = Peak Particle Velocity (mm/s);

SD = Scaled Distance ($m/kg^{1/2}$); and

α and β are site-specific constants based on the geology of the terrain.

Scaled Distance is defined as:

$$SD = D/w^{1/2} \quad (2)$$

Where:

D = Distance between the closest blast hole to the receptor (m); and

w = maximum weight of explosive detonated per delay (kg).

The constants, α and β , are site-specific and must be determined by conducting a blast study at the Site. A blast study includes multiple test blasts conducted on-site while measuring particle velocities at varying distances and charge weights for each blast. The resulting data can then be used to create a log-log plot of peak particle velocity versus scaled distance where the slope of the line-of-best-fit through the data is equal to the constant α and the value of the y-intercept is equal to β .

The following figure depicts an example of this type of graph prepared by Lucole and Dowding (1979), with their analysis of over 2500-recorded blasts:

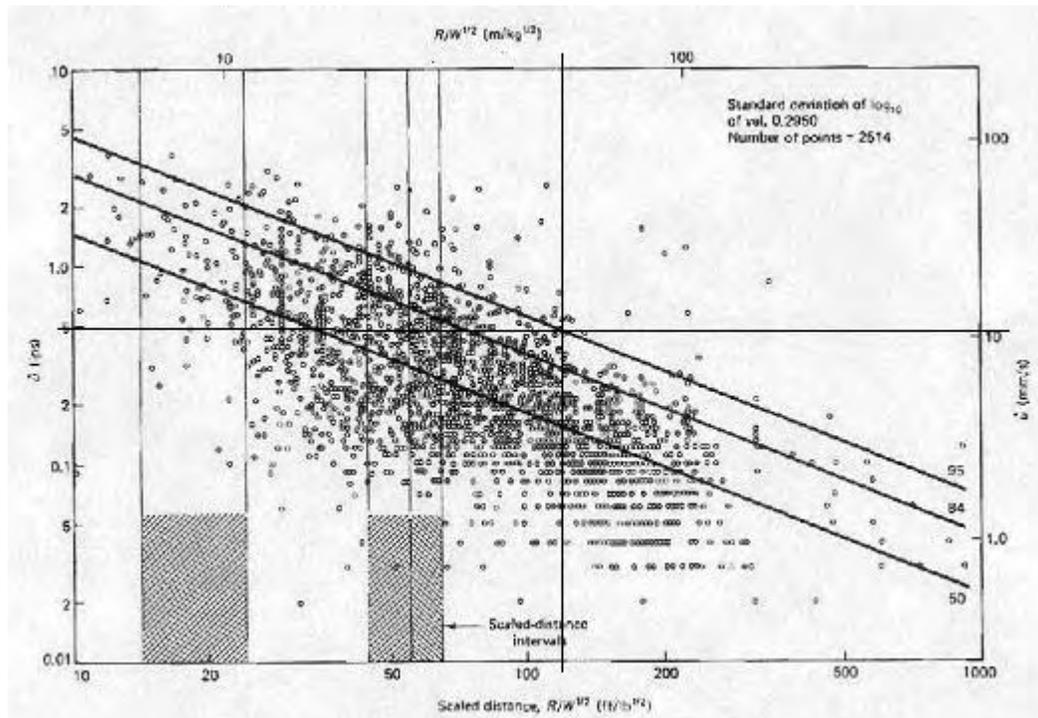


Figure 2 - Variation of particle velocities for blasting in general (resultant values)

Since test blasts have not been conducted at the Site and no seismograph information is available, it is not possible to obtain the site-specific propagation constants, α and β . Therefore, the maximum allowable charge weight per delay may be estimated assuming a minimum safe scaled distance, SD.

Information obtained from the United States (U.S.) Office of Surface Mining provides a minimum safe scaled distance of 70 ft/lb^{1/2} (31.7 m/kg^{1/2}) for a maximum allowable peak particle velocity of 0.50 inches/s (12.7 mm/s). Another document, entitled "Technical Engineering and Design Guides as Adapted from the U.S. Army Corps of Engineers, No. 16" from the American Society of Civil Engineers, suggests a minimum safe scaled distance of 50 ft/lb^{1/2} for a maximum allowable peak particle velocity of 2 inches/s (50.8 mm/s). Using the seismograph information from Figure 2, it can be seen that a minimum safe scaled distance for a maximum particle velocity of 12.5 mm/s at the 95 percent confidence level is 60 m/kg^{1/2}. Therefore, 60 m/kg^{1/2} was chosen to provide a conservative estimate for the purpose of this evaluation.

Substituting this minimum safe scaled distance into equation (2) and the known separation distance (1,880 m) to the nearest sensitive receptor and solving for w , results in a maximum allowable weight of explosives per delay of 900 kg.

The proposed blast design for the Site utilizes a maximum of 206.8 kg/delay. Therefore, based on this Assessment, there is no potential for adverse effects due to ground vibration to nearby receptors resulting from the blasting operations to be conducted on-site. These calculations do not take into consideration any attenuation measures.

Alternatively, this can be roughly verified using the graph presented as Figure 2 by simply finding the actual scaled distance of 130.7 m/kg^{1/2} on the upper x-axis and locating the corresponding y-axis value using the 95 percent confidence line. The estimated value determined graphically is 5 mm/s. This estimated peak particle velocity is below the NSDEL criteria of 12.5 mm/s.

4.2 AIR BLAST

Another undesirable effect of blasting operations is the generation of air blasts. Air blasts cause an atmospheric overpressure that travels through the air. Air blast is increased by exposed detonating cord, lack of sufficient stemming in blast holes, insufficient burden, heavy low-level cloud cover, high winds, and atmospheric temperature inversions.

The overpressure propagates at the speed of sound and has an audible noise level. Thus, air blasts are measured in decibels. Many structures have natural resonant frequencies close to or equivalent to the overpressure wave. This possibility of resonance causes repetitive pressures on the adjacent structures, which produces the vibration effects of ground-transmitted vibrations.

The NSDEL *Pit and Quarry Guidelines* provides a maximum concussion (air blast) of 128 dBA within 7 m of the nearest structure not located on the property where the blasting operations occur.

Air blast is estimated for a specific location using the following equation:

$$\text{APL} = \beta (\text{SD})^\alpha \quad (3)$$

Where:

APL = Air Pressure Level (dBL);

SD = Scaled Distance ($\text{m}/\text{kg}^{1/3}$); and

α and β are site-specific constants based on the geology of the terrain.

Scaled distance is defined as:

$$\text{SD} = D/w^{1/3} \quad (4)$$

Where:

D = Distance between the closest blast hole to the monitoring receptor (m); and

w = maximum weight of explosive detonated per delay period (kg).

Scaled distances for air blasts are generally calculated by dividing the separation distance with the cube root of the maximum charge weight, as opposed to dividing by the square root of the maximum charge weight when determining the scaled distance for peak particle velocity.

Similar to the procedure for determining the propagation constants for ground vibrations, a blast study measuring overpressure (dBA) with varying distances and charge weights for each blast will provide the required information to generate a log-log plot of maximum overpressure versus scaled distance, where the slope of the line-of-best-fit through the data is equal to α and the value of the y-intercept is equal to β .

The following figure depicts an example of this type of graph, developed by Siskind et al. 1980a, based on the plot of overpressure versus scaled distance.

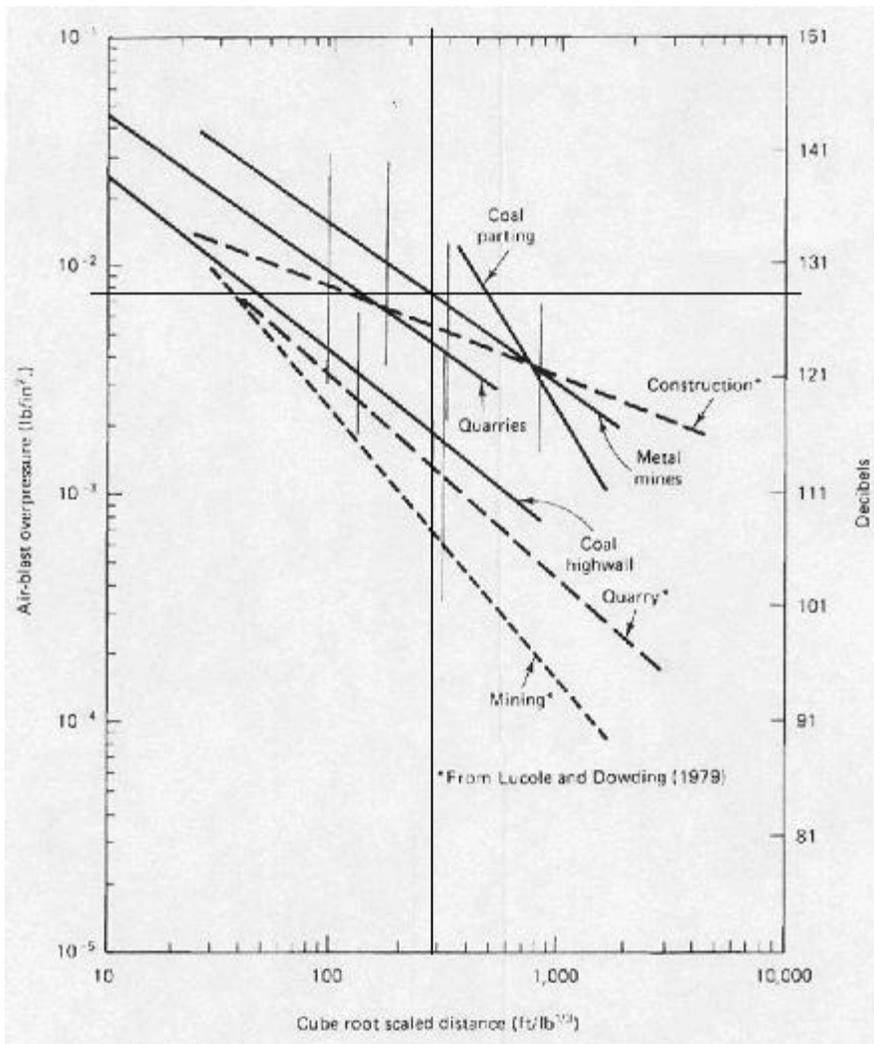


Figure 3 - Air Blast propagation from various types of mining (0.1-Hz high-pass)

Since test blasts have not been conducted at the Site and no seismograph information is available, it is not possible to obtain the site-specific propagation constants, α and β . Therefore, the maximum allowable charge weight per delay may be estimated assuming a minimum safe scaled distance, SD.

The information pertaining to a minimum safe scaled distance when determining air blast is limited. Therefore, using the seismograph information from Figure 3, it can be seen that a minimum safe scaled distance for a maximum overpressure of 128 dBA is observed to be just under 300 ft/lb^{1/3} (119.0 m/kg^{1/3}) for the metal mines graph. The metal mines graph was selected to provide a conservative estimate of the minimum safe

scaled distance. As a conservative estimate, 300 ft/lb^{1/3} (119.0 m/kg^{1/3}) was used as the minimum safe scaled distance (SD) for the purpose of this evaluation.

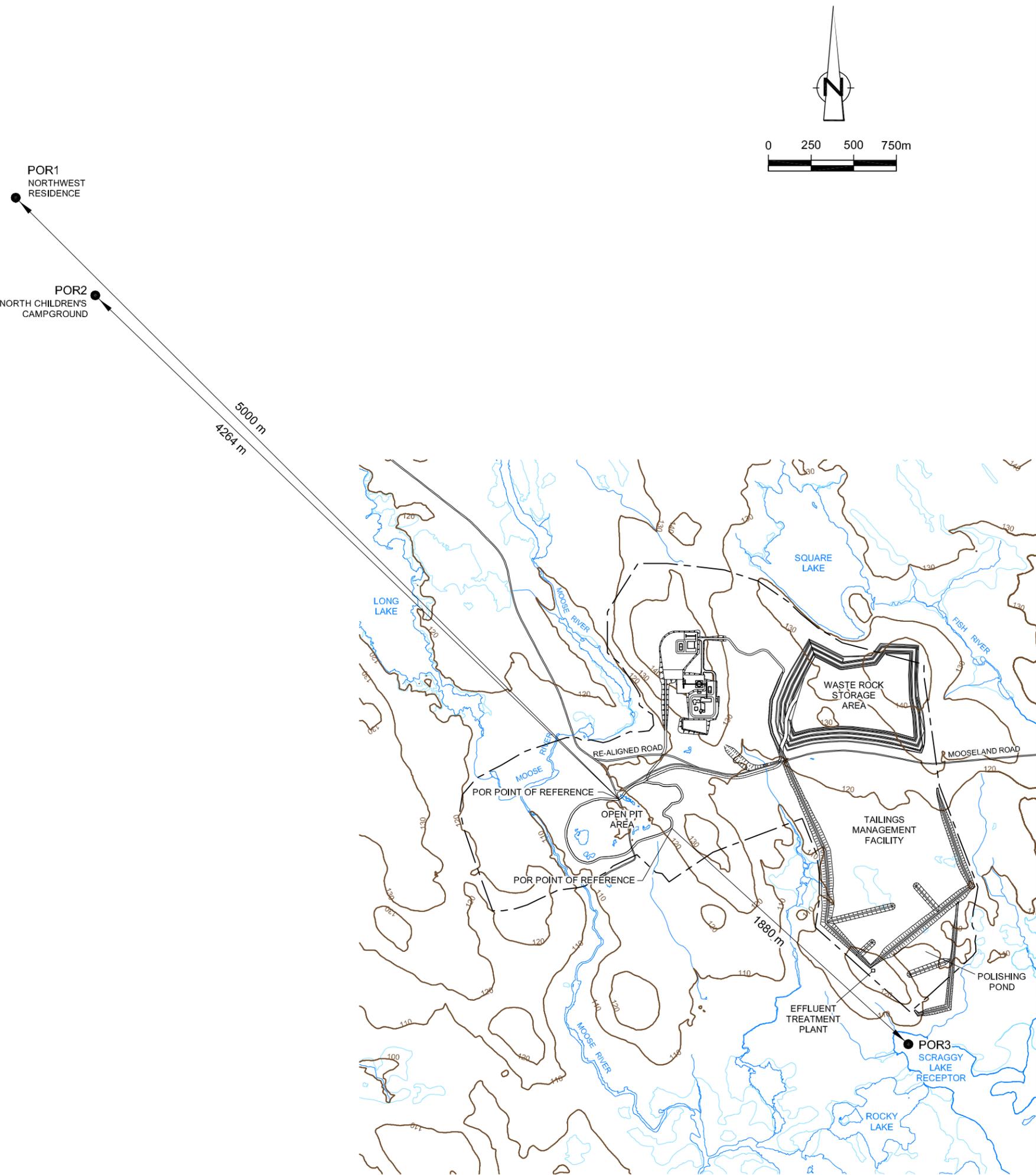
Substituting this minimum safe scaled distance into equation (4) and the known separation distance to the nearest sensitive receptor (1,880 m) and solving for *w*, results in a maximum allowable weight of explosives per delay of approximately 3,900 kg.

The proposed blast design for the Site utilizes a maximum of 206.8 kg/delay. Therefore, based on this Assessment, there is no potential for adverse effects due to air blast on nearby receptors resulting from the blasting operations to be conducted on-site. These calculations do not take into consideration any attenuation measures.

Alternatively, this can be roughly verified using the graph presented as Figure 3 by simply finding the actual scaled distance of 800 ft/lb^{1/3} (317.9 m/kg^{1/3}) on the lower x-axis and locating the corresponding y-axis value using the metal mines graph line. The estimated value determined graphically is approximately 122 dB. This estimated air blast overpressure is below the NSDEL criteria of 128 dBA.

5.0 CONCLUSION

The results from this Assessment indicate that the proposed blasting operations at the Site will be in compliance with the NSDEL *Pit and Quarry Guidelines* (1999) based on the worst-case estimates described in Sections 4.1 and 4.2.



LEGEND
 - - - - - SITE BOUNDARY
 ● POR2 POINT OF RECEPTION

figure 1
 SITE AND POINT OF RECEPTION PLAN
 VIBRATION IMPACT ASSESSMENT
 TOUQUOY GOLD PROJECT
 Moose River, Nova Scotia



APPENDIX R
GEOCHEMICAL STUDY

Golder Associates Ltd.

2390 Argentia Road
Mississauga, Ontario, Canada L5N 5Z7
Telephone: (905) 567-4444
Fax: (905) 567-6561



(Version 2)

REPORT ON

**GEOCHEMICAL STUDY
STATIC AND KINETIC TESTING OF WASTE ROCK
AND TAILINGS
TOUQUOY PROJECT
NOVA SCOTIA, CANADA**

Submitted to:

Atlantic Gold NS.
Suite 701, 220 Pacific Highway
Crows Nest
NSW 2065 Australia

DISTRIBUTION:

2 Copies - Atlantic Gold NS
2 Copies - Golder Associates Ltd.

August, 2007

06-1118-041c



EXECUTIVE SUMMARY

A geochemical characterization program was undertaken for Atlantic Gold NL (Atlantic) for the Touquoy Project. The current mine plan calls for extraction of gold ore by open pit mining. The Touquoy site is located in Moose River Gold Mines region of Halifax County in the central part of Nova Scotia, Canada, approximately 140 km northeast of Halifax. The primary objective of the geochemical characterization program is to provide sufficient data for chemical stability evaluation of the various materials expected to be produced in mining and mineral processing.

The testing program described in this report was designed to evaluate the metal leaching potential and acid generating capacity of the waste rock, marginal ore and tailings that may be deposited on site. The characterization of the mine wastes was completed using samples selected to represent specific rock types, and to evaluate the deposit characteristics on a scale that is relevant to the proposed mining operations (e.g. in addition to specific rock-type samples, composite samples over the expected open pit bench height intervals are used in the assessment). The geochemistry test work includes both short term (static) and long-term (kinetic) tests to determine the chemical stability of these materials. The implications of these results with respect to the Touquoy Project are discussed, as are possible mitigation measures.

Results show that with respect to acid generation, the Touquoy site is significantly different from other maritime mining projects such as Voisey's Bay, or from around Halifax. The rock sequences at Touquoy do not contain the massive sulphides of a Voisey Bay type deposit, nor do they contain the sulphide rich slates of the Halifax Formation which are responsible for ARD at the Halifax Airport. Overall sulphide contents at the Touquoy project are low.

Only a small proportion of the potential waste materials from the proposed Touquoy project are acid generating (2% based on samples collected to date), and given that the majority of buffering minerals are carbonate minerals for which excess neutralization potential is readily available, it is considered that overall the waste materials from the Touquoy project will be non acid generating with excess neutralizing capacity. Additional evidence that AG will not be prevalent is available from the net acid generation testing completed as well as the bulk sample pit on site. The water quality from this pit remains neutral after several years exposed to the environment (Atlantic 2007 – pers. Com with Peter Carter).

Results of the trace metal analyses and leach test results indicate arsenic is the main parameter of concern for the Touquoy project. With respect to water quality values, based on the short term testing, NAG test results, and humidity test cell results, overall, values of long term and short term leachate for most parameters are neutral with low concentrations of dissolved parameters relative to other mining properties. Although some parameters (e.g. Al, As, Zn) are elevated in the short term and longer term leach testing it is important to keep in mind that these values must

be taken in the context of the overall site water quality and potential site discharge. Evaluation of these parameters is currently underway as part of an overall site water quality model.

Based on the results and conclusions as presented herein recommendations are as follows:

- As opportunity presents itself (as infilling drilling occurs) a few additional confirmation samples of fresh rock in the western zones of the pit should be collected and analysed for sulphide content. Should the pit design change, the sample set and analytical results will need to be reviewed to determine if supplementary collection and geochemical characterization of samples is required.
- Monitoring should include periodic evaluation of conditions on site with respect to visual indicators of acid generating conditions such as ferric hydroxide precipitation on the waste materials and in water courses or streams.
- Monitoring of water quality from the site and tailings should be conducted regularly during operations and for a period after closure.
- Management strategies for waste rock and tailings should be re-evaluated periodically during operations and adjusted or updated if necessary based on the results of the monitoring data.

Should acid generation be observed in the materials on the surface of the pile, it is considered that the overall NP of the pile will limit vertical migration of acidic conditions in the pile. Mitigation/remediation of these small areas of the pile would involve relocation of the acid generating materials, within areas of the pile that are non-acid generating, or covering the materials to maintain clean surface runoff and limit oxidation of the materials.

It is recommended that appropriate treatment options for arsenic and other parameters be implemented if deemed necessary once an evaluation of overall site water quality is completed. This overall water quality evaluation, and an evaluation of treatment options is currently underway.

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1.0 INTRODUCTION

This report provides information regarding the geochemical characterization of the Touquoy Gold deposit in the Moose River Gold Mines district of Nova Scotia, Canada. Golder Associates (Golder) was retained by Atlantic Gold NL (Atlantic) to provide a geochemical characterization of the anticipated mine waste materials at the Touquoy property in support of Feasibility Studies, currently in progress.

1.1 Background Theory Regarding Geochemistry of Mine Waste

In mining operations, the natural weathering of soils and rock is typically accelerated as these materials are disturbed and exposed to the atmosphere. This enhanced weathering may result in impacts to water resources (i.e., groundwater, surface water). It is therefore necessary to evaluate the quantity and composition of possible runoff and leachate from the disturbed material to assess the potential implications to mine design and the environment. The results may influence the mine plan and may have ramifications with respect to the overall acceptance by the appropriate regulatory agencies. If a potential problem is identified, mitigation measures can often be developed to prevent, reduce or eliminate the impact.

During geochemical evaluation of mine wastes the presence or absence of sulphide minerals is important to note, since environmental impacts of most concern are commonly those associated with the presence of reactive sulphide minerals. When sulphides are exposed to the atmosphere, they have the potential to react with oxygen and water to produce acid rock drainage (ARD). The resulting acidity may then be neutralized by minerals that contain buffering capacity. Also important to note in the evaluation is the presence of carbonate minerals or other buffering minerals since carbonate minerals are generally the most effective in counteracting acidic conditions, but other minerals (e.g., silicates) may contribute as well. If insufficient buffering minerals are present, significant quantities of acidity, sulphate and metals may be released from the mine wastes.

In addition to evaluation of acid generation, metal leaching must also be assessed since metal leaching can also occur in the absence of reactive sulphides under non-acidic conditions due to dissolution of soluble mineral phases. Release of nutrients (e.g., ammonia, nitrate) may take place due to the presence of residual explosives and is also of interest in the geochemical evaluation.

1.2 Scope of Work - Geochemistry

The primary objective of the geochemical characterization program is to provide sufficient data for chemical stability evaluation of the various materials expected to be produced in mining and mineral processing. This evaluation will allow for comparisons to be made with existing environmental conditions so that the potential for environmental impacts can be evaluated.

Other specific objectives of the baseline geochemistry program include:

- Development of a defensible geochemical database sufficient for mine planning and decision making purposes;
- Development of estimates of the potential for ARD and metal leaching for use in site water quality assessments; and,
- Development of appropriate data to support decisions related to environmental management strategies, material handling strategies or mitigation measures, as required.

The testing program described in this report was designed to evaluate the metal leaching potential and acid generating capacity of the waste rock, marginal ore and tailings that may be deposited on site. The characterization of the mine wastes was completed using samples selected to represent specific rock types, and to evaluate the deposit characteristics on a scale that is relevant to the proposed mining operations (e.g. in addition to specific rock-type samples, composite samples over the expected open pit bench height intervals are used in the assessment).

The geochemistry test work includes both short term (static) and long-term (kinetic) tests to determine the chemical stability of these materials. The implications of these results with respect to the Touquoy Project are discussed, as are possible mitigation measures and follow-up work that should be considered as the project progresses into operations.

The geochemistry work included and discussed in this report was initiated in Mid-2006 with completion of an on-site sampling program. M. Herrell of Golder Associates visited site and reviewed available drill core to select samples to be representative of potential materials from the deposit under the direction of K. DeVos of Golder Associates. Following selection of samples a static test program was initiated with results presented in December of 2006. Following completion of the static test program 10 waste rock samples of various lithologies were selected for longer term kinetic testing to evaluate potential changes in chemistry over time. Results for the initial 20 weeks of testing are included in this report as are available results for tailings samples as provided by SGS Lakefield in Ontario, Canada, under the direction of Atlantic's metallurgist, Sydney-based Peter Lewis and Associates.

2.0 BACKGROUND GEOLOGY AND PROJECT DEVELOPMENT

2.1 Project Overview

The project overview and background geology as summarized below is based on the draft project description (Atlantic, 2006a) and discussions with Atlantic Gold personnel. The Touquoy Gold deposit is located approximately 140 km northeast of Halifax in the Moose River Gold Mines district in the Halifax County, Nova Scotia, Canada. The proposed site lease area is 320ha, with a proposed approximate footprint of 265 ha. The Touquoy site is mainly characterized by low-relief and hummocky topography. The site is located inland, sheltered from the immediate effects of the Atlantic Ocean, such that climate conditions are characterized by warmer summers and cooler winters. A Meteorological Service of Canada climate station (ID#8203535) is located approximately 15 kilometres from the site location near Middle Musquodoboit. A 35 year climate record from 1968-2003 indicated monthly temperatures vary from -6.2°C in January to 18.4°C in July and average monthly precipitation varies from 97 mm in June to approximately 138 mm in December.

Based on the Atlantic 2006 project description, ore will be extracted through an open pit operation with an anticipated mine life of 5 to 7 years and a mill capacity of 4,000 – 5,000 tpd. The Touquoy property has an estimated total resource of approximately 9.76 Mt at a grade of 1.8 g/t and is expected to yield approximately 554,500 oz gold. The ore is disseminated throughout the sedimentary host rocks and is visually indistinguishable from waste materials. During operations, the ore will have to be delineated through grade control drilling for each bench as the pit evolves (Atlantic, 2006a).

The project description indicates that gold will be removed from the ore in a process involving the following two stages: gravity concentration and carbon-in-leach (CIL) procedure. Tailings produced during process will be detoxified using the INCO SO₂/Air procedure before being deposited as a slurry at approximately 50% solids into the tailings management facility (TMF).

2.2 Background Geology

The Touquoy deposit is formed in the Meguma Group sediments of Nova Scotia. Meguma Group sediments consist of a series of greywacke and argillite sedimentary rocks underlying approximately half of the province of Nova Scotia. Two main lithological units occur at the Touquoy Project: argillite and greywacke. Varying degrees of interbedding occur within these two units and the above can be further subdivided as follows:

- Argillite (<5% greywacke interbeds)
- Argillite (5-49% greywacke interbeds)
- Greywacke (<20% argillite interbeds)
- Greywacke (20-50% argillite interbeds)

Minor quartz veining is also present in the Touquoy deposit; however, unlike the majority of gold deposits in Meguma sediments, mineralization at Touquoy is found disseminated throughout the sediments and is not associated with quartz veining. Of note is that the deposit does not encounter the slates of the Halifax Formation which contribute to much of the acid generation issues in Nova Scotia.

The bedrock geology is overlain by approximately 3 metres of glacial till. The overlying sediments are mainly composed of quartzite with drumlins composed of local and foreign materials. The quartzite is described by Atlantic (2006a) as bluish-grey, loose, cobbly silt-sand till which grades into a sandier, coarser till with occasional clay inclusions.

Topsoil at the Touquoy site is part of the Danesville and Wolfville series and primarily consists of loams to sandy loams and sandy clay loams with some gravelly and stony areas.

Table 1 outlines the initial percentages of the waste rock, ore and tailings materials expected to be encountered during mining (Atlantic, 2006b). These tonnages formed the basis of waste rock distribution. It should be noted that the percentages of each lithology are based on the estimated distribution of ore among the various lithologies and the waste rock to be extracted during operations is also considered to be distributed in the same proportion (Atlantic, 2006b).

2.3 Rock/Overburden Use

All rock types are anticipated to be directed to the waste rock storage facility (WRSF) unless designated as ore. Topsoil will be stockpiled for later use in site reclamation activities or used in the construction of an annular safety berm approximately 30m outwards from the open pit. The underlying till will also be used in the construction of the safety berm and in the construction of other site infrastructure such as tailings dam embankments and for site levelling.

3.0 METHODS

3.1 Sample Selection

Waste Rock

Waste rock sample selection was conducted to meet the following objectives:

- Identify the major waste rock units and those units that will potentially be exposed on the open pit surface and in the waste rock disposal area(s); and
- Collect samples from these units that are spatially and compositionally representative of each rock type.

During the site visit, a review of the background data (geologic and design information) was conducted to develop an understanding of site components and lithologic units/alteration types that might affect the overall geochemistry of the site. Consultation with site personnel in addition to reviewing logs, cross sections and core made available, aided in the identification of major lithologies. The following prevalent lithologies types were identified:

- Argillite (<5% greywacke interbeds)
- Argillite (5-49% greywacke interbeds)
- Greywacke (<20% argillite interbeds)
- Greywacke (20-50% argillite interbeds)
- Massive quartz veins
- Argillite and greywacke composites.

The massive quartz vein is defined as an individual unit when it present for at least 50% of a one meter drill interval (Diamond Ventures NL, 2004). The argillite and greywacke composites represent sections of core where the lithology was too variable over the sample interval that no one lithological classification could be used. Composite samples were collected in areas of the pit where the composite lithologies are expected to contribute significantly to the waste rock.

In order to obtain samples of the different rock types to be encountered, Golder used the available cross-sections to evaluate rock type distribution. Samples were targeted within a preliminary pit outline (Mining Solutions Consultancy Pty Ltd., 2006) available as a trace on the cross-sections. Older core from the western area of the proposed pit was not sampled since it had been exposed to weathering on surface for some time.

The sample list was generated based on cross-sections from the central portion of the pit and the margins of the pit. A visual estimate of the lithology from the cross-sections was used as a guide

to collect samples in proportion to the distribution of the various lithologies. These proportions will be checked for representativeness after the finalization of the mining sequence plan. Based on the review of drill logs and the cross sections provided it is expected that the existing samples provide a good overview of potential conditions in the overall pit, including the western portion of the pit, however during future in-fill drilling programs it is recommended that a few confirmation samples from this area of the pit be collected and evaluated for sulphide content.

Samples were selected across the length and depth of the intended pit to obtain spatial variability to the extent possible using available core. Drillholes selected from the cross-section were sampled at length from near surface to near the pit bottom to provide a depth distribution. In general, samples were comprised of 10-m intervals of core. This interval length was chosen to mirror a typical bench height that might be used during open pit excavations.

Marginal Ore

In addition to waste rock sampling, marginal ore samples were also collected on site for geochemical characterization material that could report to the marginal ore stockpile. It was determined on site by Atlantic personnel that marginal ore would be defined by grades ranging from 0.7 to 0.9 g/t (Atlantic, 2006c). The geologic sections were reviewed to target continuous sections of core with grades in the range of 0.7 to 0.9 g/t trying to maintain an average grade of approximately 0.7 to 0.8 g/t. Occasionally, rock with grades >0.9g/t or <0.7g/t were included in some of the targeted lengths since it is expected that this material may also end up in the marginal ore pile. Marginal ore samples were identified over an appropriate interval which would maintain the marginal gold grade average.

Tailings

Two tailings samples were provided for geochemical testing. Initially, a master-composite head sample provided by Atlantic was leached and detoxified by SGS Lakefield in Ontario, Canada, under the direction of Atlantic's metallurgist, Sydney-based Peter Lewis and Associates to produce a tailings sample (CND 2) reported to be representative of the expected process by-product at the Touquoy site (Lewis, 2006). Due to the expected homogeneity of the Touquoy deposit, only one tailings sample was prepared to represent the tailings materials that will be produced during operations (Lewis, 2006). Following analyses of this sample, and discussions with Atlantic Gold and their metallurgists it was determined that additional samples would be required for evaluation of cyanide degradation rates, and to help assess potential variability in tailings materials, hence materials for a second tailings sample were shipped to SGS Lakefield. These materials were analysed for static test parameters and a second tailings sample "CNI CND1-7" was prepared using the "TWB" material from the "western section bottom" of the pit, as this was expected to be the last material that would be removed from the pit. The tailings

sample was prepared for testing by SGS Lakefield under the direction of Peter Lewis and Associates.

3.1.1 Sample Collection

Waste Rock & Marginal Ore

Once a final list of samples was assembled, lengths of core from the identified boreholes were retrieved from storage and laid out. Golder personnel then reviewed the core to evaluate the sample lithology visually relative to the core record. Waste rock samples were collected over approximately 10-m intervals. Some intervals were shorter, depending on the overall condition of the core and core recovery.

Two to three kilogram samples were collected comprising several smaller sub-samples (approximately 10-cm lengths) collected at regular intervals (approximately at each metre) across the length of each sample. The sub-samples were visually representative of the sub-interval from which they originated. Samples were placed in bags and were clearly labelled with a unique sample number in indelible marker. The bags were sealed and samples were then gathered into larger bags and labelled with shipment details. As samples were removed from the core, the core box was marked to indicate where the sample was removed. All samples were shipped from site to the analytical laboratory in Lakefield, Ontario (SGS Lakefield).

A total of 83 waste rock and 11 marginal ore samples were collected. Initially 84 waste rock samples were targeted but, based on a review of the average gold grades in the samples, one waste rock sample (06-008) was more representative of material that may be classified as marginal ore. This sample had grades ranging from 0.012 to 2.01 g/t with an average of 0.62 g/t. Table 2 provides a summary of waste rock and marginal ore samples collected from the site.

Tailings

A wet head sample to be leached and detoxified was initially shipped directly by Metcon Laboratories in Australia to the analytical laboratory, SGS Lakefield, in Lakefield, Ontario, Canada in 2006 for tailings testing. The resulting leached sample was labelled "CND2" and was subjected to environmental testing as reported herein.

Following discussion with Atlantic Gold a second tailings sample was prepared. On March 6th SGS Lakefield received from Metcon Labs in Australia 1kg each of samples labelled TWT, TWM, TET and TEB which represent the different zones of the proposed pit. These samples were subjected to the static testing. Also received was a sample of approximately 20kg labelled TWB (or TWB CN Feed) which represents material from the lower western section of the

proposed pit. This sample was subjected to the same static tests which were completed prior to CN detox work.

The 20 kg TWB sample was then used by the SGS Lakefield metallurgical group for cyanide destruction/detox (CND work). Various tests are run during the detox process and samples from these tests were labelled as CND1, CND2, CND3, with a final completed tailings sample generated and labelled "CN1 CND1-7". Static testing was completed on this sample as was a 45 day age test. Humidity cell testing of this sample is currently underway.

Table 2 summarizes the details of these samples.

3.2 Laboratory Testing Methods

Selected samples were submitted for static testing and longer-term kinetic testing, and the tailings samples were submitted for kinetic testing. These tests are summarized below. Additional details on these test procedures are provided in Price (1997), MEND (2005) and in ASTM (2001). The geochemical testing was conducted by SGS Lakefield Research in Lakefield, Ontario.

3.2.1 Static Testing

Static tests are "one-time" analyses used to determine the general geochemical characteristics of a sample. These tests are typically the first step in the assessment and prediction of acidic drainage and metal leaching. For an individual sample this testing might comprise a combination of the following:

- Elemental Analysis on Solids and/or Whole Rock Analyses – used to determine the total amount of metals in the solid phase of the rock samples;
- Mineralogy – used to identify mineral assemblages as they have a large influence on acid generating and buffering reactions.
- Modified Acid Base Accounting (Modified ABA) – used to develop estimates of the potential for acid generation based on the balance between acid producing and acid buffering minerals;
- Short-Term Leach Testing – used to develop initial estimates of metal leaching from weathered materials; and,
- Net Acid Generation tests – used to estimate the acid generation potential and water quality resulting from the complete oxidation of all sulphide minerals and dissolution of all neutralizing phases in a sample. NAG test leachates represent possible late stage (or terminal) water qualities that are environmentally conservative.

Modified ABA

Acid-base accounting (ABA) testing was conducted to determine the acid generation potential of the waste rock and tailings. ABA testing included the following parameters:

- Paste pH;
- Sulphur species (including total sulphur, sulphide sulphur and sulphate);
- Neutralization potential (NP) by the modified Sobek method;
- Carbonate NP (CaNP) by carbon dioxide analysis; and
- Calculation of acid potential (AP), net neutralization potential (NNP), neutralization potential ratio (NPR, or NP/AP), and carbonate neutralization potential ratio (CaNP/AP).

ABA is used to determine the balance between the acid-generating potential (AP) and acid neutralizing potential (NP) of a particular material. There are a number of standard protocols used for the determination of ABA as summarized in Price (1997). For this characterization, a modified Sobek method was used (based on Sobek et al., 1978). Rather than calculating an AP based on total sulphur, the AP is calculated using sulphide-sulphur. This assumes that all the sulphide sulphur is present as pyrite and that each mole of pyrite generates four moles of hydrogen ions upon oxidation. This assumption is supported by the mineralogical characterization performed by SGS Lakefield (Appendix D). Using sulphide sulphur instead of total sulphur values avoids the over-estimation of the AP that may occur by incorporating other oxidized, non-reactive forms of sulphur.

The NP is generally determined by sample acidification with sulphuric acid and back-titration to identify acid consumption as described in Sobek et al. (1978). A common alternative method for the estimation of NP makes use of carbonate analysis. On the assumption that all carbonate represents calcite [CaCO_3] (Appendix D), a conversion is performed to calculate the amount of calcite. This form of NP is thus referred to as carbonate neutralization potential (CaNP). Use of CaNP is considered to be a more conservative measure of available neutralizing potential than the "bulk" NP Sobek methods. In many cases, the Sobek method has been shown to overestimate available neutralizing capacity due to the dissolution and subsequent acid consumption by silicate minerals during the test. However, under ambient conditions, dissolution of silicate minerals is generally too slow to provide effective buffering capacity, and only the readily-available CaNP is released.

Paste pH is a test to measure the pH that a sample generates upon contact with water. The pH is measured in a paste formed by mixing water and a crushed rock sample (Steffen et al., 1989). This test is a qualitative indicator of the capacity of the sample for the immediate dissolution of calcium carbonate as well as the presence of stored acidity.

A number of criteria have been proposed for assigning an ARD potential to a material using ABA results. The most common approaches are those based on the use of the neutralization potential ratio ($NPR = NP/AP$). For several reasons, no single ratio of NPR values has been identified to have universal applicability with respect to acid generation prediction. The actual threshold values for a particular solid are material specific, and depend on factors including the amounts and type of acid generating and neutralizing materials, morphology, crystallinity, grain size, chemical composition, paragenesis, texture and site-specific exposure conditions.

For the purpose of this study, acid generation potential (AP) was calculated using sulphide-sulphur (modified Sobek method). Sulphide-sulphur is used for this purpose, as it is considered to represent the reactive sulphur component. NPR guidelines suggested by Price (1997) are summarized below:

| Potential for ARD | Criteria | Comments |
|-------------------|---------------|---|
| Likely | $NPR < 1$ | Likely acid generating, unless sulphide minerals are non-reactive. |
| Uncertain | $1 < NPR < 2$ | Possibly acid generating if NP is insufficiently reactive or is depleted at a rate faster than sulphides. |
| Low | $2 < NPR < 4$ | Not potentially acid generating unless significant preferential exposure of sulphides along fractures planes, or extremely reactive sulphides in combination with insufficiently reactive NP. |
| None | $NPR > 4$ | Not expected to generate acidity |

In addition, the relationship between paste pH and sulphide-sulphur content was considered. Materials with a sulphide-sulphur content of less than 0.3 wt.% and a paste pH greater than 5.5 may be classified as non-acid generating (Price, 1997) except where the rock matrix consists of base poor minerals (e.g., quartz), or where the sulphide minerals contain metals that may leach under weakly acidic to alkaline conditions.

Net Acid Generation

NAG testing was performed on a sub-set of samples. Samples were selected for NAG testing based on ABA results. The purpose of NAG testing was to assist in evaluating the long term acid generation potential of these rock types. The test uses hydrogen peroxide to accelerate sulphide oxidation. The neutralizing minerals dissolve in response to the acidity released during sulphide oxidation. Since the acid generating reactions go to completion the results of NAG tests are considered to be indicators of longer term pH, water quality and acid generation potential.

Elemental Analysis

Elemental analysis was performed to determine the solid-phase content of most metals in a material or the reservoir of an element in the material, to characterize the chemical composition of the rock samples. Two analytical methods were used. XRF was used to quantify the major oxide content of the rock and ICP was used to quantify trace metals.

The elemental composition provides a basis for comparison between and within lithologies. In addition, if necessary, element data can be used in conjunction with results from leach tests to develop predictive, quantitative relationships between metal content and leaching rate. Results were also compared to average crustal abundances as presented in Price (1997).

Short-Term Leach Testing (Modified SPLP)

Short-term leach tests are primarily used as a screening tool for qualitative identification of elements of potential environmental concern and to evaluate the extent of weathering of the core. The results of this type of testing do not translate directly to the expected environmental behaviour of the rock because of the small size of the test, the reduced grain size of the materials, the short duration, and the enhanced contact between the liquid and the solid test charge during the test.

The short-term leach test utilized in this characterization program was a modified version of the U.S. EPA Method 1312 Synthetic Precipitation Leach Procedure (SPLP) (U.S.EPA, 1998). The modification involved the use of a water to rock ratio of 4:1 (by weight) rather than the standard ratio of 20:1. This was done to reduce the possibility of inadvertently diluting solutes to concentrations below their respective detection limits. A 100 g of solid sample was mixed with 400 mL of a dilute sulphuric/nitric acid solution at a pH of 5. The sample container was then rotated end-over-end in an agitator for 18 hours after which, the leachate samples were collected, filtered and analyzed using ICP-MS.

Results of short-term leach tests are very sensitive to the methodology and can therefore exhibit considerable variability related to the specific test methodology used. As such, the SPLP test does not represent field conditions. In particular, the solid to solution ratio can have a profound effect on leachate composition, and anticipated relationships between the degree of dilution and leachate quality are rarely observed. In addition, the SPLP simulates metals leaching by simple dissolution of readily-soluble mineral phases in response to a single, natural precipitation event (e.g., a "first flush" event). The test is therefore not intended to simulate transient conditions and reactions, such as sulphide oxidation. To assess reaction rates and long term conditions, results from the laboratory kinetic tests are typically used.

Despite these limitations, results from the SPLP test are useful in that they provide a first indication of elements of potential environmental concern. However, since the leachate compositions cannot be directly related to full-scale, ambient operational or post-closure conditions they should not be quantitatively compared to water quality guidelines.

Mineralogy

Mineralogy is a controlling factor in the geochemical behaviour of a material. For example, iron identified in the trace metal analysis may occur in acid generating pyrite, or acid neutralizing calcium-iron carbonate, or some other form of oxide. Mineralogy testing is performed to better understand the composition of the material.

3.2.2 Kinetic Testing

Kinetic tests are repetitive leach tests on a representative sample designed to evaluate potential material reactivity, mass loading and/or leachate water quality of the sample over time.

Laboratory Humidity Cell Tests

A humidity cell is a weathering chamber designed to provide simple control over air, temperature and moisture, while allowing for the removal of weathering products (principally oxidation products) in solution. For the laboratory testing, a standard humidity cell procedure as described in ASTM D5744-96 Standard Test Method for Accelerated Weathering of Solid Materials Using a Modified Humidity Cell (ASTM, 2001) is used. This type of laboratory testing also provides the fundamental data necessary to complete a preliminary evaluation of reaction rates for acid generating minerals, reaction rates for neutralizing minerals, metal leaching rates, mass loading rates and possible water quality implications.

The standard humidity cell test requires approximately 1 kg of sample (ASTM, 2001). Prior to placement in the test cell, the sample is wetted, flushed, and rinsed. This is followed by a weekly cycle of dry air, humid air, and flushing. The flushing takes place by adding 500 mL of the lixiviant to the top of the cell and allowing it to soak the samples for a specified period. The leachate resulting from the flushing is filtered and analyzed for a limited set of standard parameters on a weekly basis, as well as for a more comprehensive suite of analytes at greater time intervals.

Humidity cell tests have been completed for 11 samples in total: 1 tailings sample, and 10 waste rock samples. Humidity cell testing on one additional tailings sample is currently underway.

Tailings Supernatant Age Testing

The purpose of the ageing test analyses is to describe the natural attenuation of various parameters through time and to quantify the water quality of the process water being discharged to the tailings management facility. Tailings supernatant water, generated during leaching and detoxification of the ore head sample, is retained and scanned over time, generally on the following days: 0, 3, 7, 14, 31 and 45 for selected parameters.

4.0 RESULTS

This section presents the results of the static and kinetic test analyses for the Touquoy deposit. Detailed results from static testing are provided in Appendix A. Results from the kinetic test work are provided in Appendix B.

4.1 XRF and Trace Metals

The composition of the samples as determined by the XRF results and trace metals analyses are summarized in Tables 3 and 4. Histograms showing the distribution of metals for each rock type are presented in Figure 1 and 2. The squares on the figures represent static test results from the samples selected for short-term leach and kinetic testing.

Average elemental compositions of the principle rock types are similar as is expected in turbidite depositional sequences such as the Meguma Formation. This is supported in the varying degrees of interbedding of sandstone/argillite in the argillite and sandstone units. The elemental similarity between the rock units at the Touquoy site suggests lithologies differ in grain size and are likely derived from similar host rocks.

Elemental compositions were also compared to the average crustal abundances for clastic sedimentary rocks (Price, 1997). It is important to note that the average crustal abundances provide a basis of comparison and elements elevated relative to these values does not necessarily mean it will be an environmental concern.

Compared to the average elemental compositions for clastic sedimentary rocks, arsenic concentrations are elevated in all of the principle rock units. The overall arsenic average was 1042 ppm for waste rock and marginal ore samples collected from the Touquoy site. Arsenic concentrations were observed to be highest in the argillite (<5% greywacke interbeds) with an average of 1620 ppm and a maximum of 15,000 ppm. Although the maximum concentration skews the average in this unit, the median value of 340 ppm also remains elevated over the average crustal abundance of 13 ppm. Arsenic concentrations in the tailings samples ranged from 160 ppm in the blended overall sample to a maximum of 1300 ppm in the TET (eastern section top) sample.

The average concentrations of silver and selenium were also observed to be elevated relative to the average crustal abundances for clastic sedimentary rocks. Maximum average concentrations of silver (0.73 ppm) and selenium (2.3 ppm) occurred in the quartz vein and the marginal ore units respectively. Maximum concentrations of silver (1.1 ppm) and selenium (7.0 ppm) were observed in the argillite (<5% greywacke interbeds).

4.2 Mineralogy

Five samples were selected for mineralogical analysis. The purpose of performing this analysis was to quantify the mineralogical characteristics of the waste rock, specifically the sulphide and carbonate bearing mineral phases as these have the greatest influence on the acid generating/neutralization potential of the sample.

Samples selected for mineralogy include:

| Sample # | Hole # | From (m) | To | Lithology | Lithological Description |
|----------|-----------|----------|----|-----------|--|
| 06-034 | MR-05-091 | 10 | 20 | G/A | Greywacke (20-50% argillite interbeds) |
| 06-049 | MR-05-122 | 10 | 20 | AR | Argillite (<5% greywacke interbeds) |
| 06-073 | MR-05-094 | 12 | 22 | AR | Argillite (<5% greywacke interbeds) |
| 06-066 | MR-05-084 | 65 | 72 | GW | Greywacke (<20% argillite interbeds) |
| 06-070 | MR-05-083 | 68 | 75 | Comp | Composite (greywacke and argillite) |

Note:

Based on data from Lakefield (2006).

Based on Lakefield's mineralogical report (2006) (Appendix D), the three main sulphide minerals are pyrite, pyrrhotite and arsenopyrite. Examination of the textural associations of these minerals indicate that 50-80% of the pyrite and 50-100% of the pyrrhotite occurs locked within the silicate particles and may not be readily available to oxidize and produce acidity. Only a minor proportion of arsenopyrite (0-26%) occurs locked among silicate particles. Therefore, sulphide speciation (i.e., mineralogical association) in the waste rock materials will influence the acid producing potential of the samples. The following table presents the five samples selected for mineralogical analyses, the percentage of sulphide minerals in the sample, and the predominant sulphide mineral(s) encountered.

| Sample | Lithology | % sulphide minerals in sample (by weight) | Predominant Sulphides Observed |
|--------|--|---|--------------------------------|
| 06-034 | Greywacke (20-50% argillite interbeds) | 0.08 | Arsenopyrite |
| 06-049 | Argillite (<5% greywacke interbeds) | 0.22 | Pyrrhotite & Arsenopyrite |
| 06-073 | Argillite (<5% greywacke interbeds) | 0.55 | Pyrite & Arsenopyrite |
| 06-066 | Greywacke (<20% argillite interbeds) | 0.24 | Arsenopyrite |
| 06-070 | Composite (greywacke and argillite) | 0.37 | Pyrite |

Note:

Predominant sulphide minerals Based on data from Lakefield (2006). Sulphide content based on ABA test results.

Availability and the type of carbonate minerals will also influence the available neutralization potential of the samples. The predominant carbonate minerals present in the five samples submitted for mineralogical analyses are calcite, dolomite and ankerite. The distribution of the carbonate species is presented in the following table:

| Mineral | Sample Formula | 06-034 | | 06-049 | | 06-066 | | 06-070 | | 06-073 | |
|--------------|---|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| | | wt. % | Dist'n % |
| Calcite | CaCO ₃ | 4.49 | 99.8 | 3.24 | 78.7 | 3.38 | 78.9 | 3.17 | 68.3 | 5.26 | 68.8 |
| Dolomite | CaMg(CO ₃) ₂ | 0.0 | 0.1 | 0.48 | 11.8 | 0.83 | 19.5 | 1.46 | 31.4 | 0.66 | 8.6 |
| Ankerite | Ca(Fe,Mg,Mn)(CO ₃) ₂ | 0.0 | 0.1 | 0.39 | 9.4 | 0.06 | 1.5 | 0.01 | 0.2 | 1.71 | 22.4 |
| Siderite | FeCO ₃ | 0.001 | 0.0 | 0.01 | 0.1 | 0.01 | 0.1 | 0.002 | 0.1 | 0.02 | 0.2 |
| Total | | 4.5 | 100 | 4.1 | 100 | 4.3 | 100 | 4.6 | 100 | 7.7 | 100 |

Note:

Based on data from Lakefield (2006).

Although the textural relationship of the carbonate minerals suggests that approximately 53% to 78% are either liberated or exposed and are amenable to dissolution and neutralization (Lakefield, 2006), the carbonate species will influence the effectiveness of the neutralization potential. For example, calcite is readily soluble and is an effective neutralizing mineral; however, manganese and iron carbonates create acidity when they dissolve and no net alkalinity is produced (Price, 1997). Therefore, the predominant cation available in the ankerite carbonates during hydrolysis will influence the neutralization potential of this mineral. The percentage of carbonate available for neutralization is a function of the form of mineral as well as the amount of exposure of the mineral on faces of the larger grainsize particles.

4.3 Acid Generating Potential and Metal Leachability

ABA and short term leach testing was performed on waste rock and marginal ore to quantify the acid generating and metal leaching potential of these materials. The tailings samples were also submitted for ABA testing to characterize the tailings acid producing potential. Humidity cell testing was conducted for the tailings sample to quantify the expected leachability of the solids and subsequently, an aging test was completed on the supernatant to characterize the water quality of the process water.

Results of the ABA testing are summarized in Table 5 and in Figures 3 through 6. Metal leachability was assessed by short term leach tests (i.e., SPLP). Short term leach test results are summarized in Table 6 and are provided graphically in Figure 7. It is important to note that short-term leach analyses are aggressive leaching tests that generally produce elevated dissolved elemental concentrations that are not representative of what would occur under ambient

conditions. Comparisons relative to environmental guidelines are applied here for illustrative purposes only. Appendix C graphically shows the sample locations on cross sections.

NAG testing was performed in order to confirm the results of ABA and assess the metal leaching potential from each rock type under terminal conditions (i.e., after the complete oxidation of sulphide minerals and complete dissolution of neutralizing minerals). NAG test results, including comprehensive analysis of selected NAG leachates, are provided in Table 7.

Static and kinetic test results are discussed by lithology, followed by a more general discussion of the relationship of the results, including a discussion of the remaining lithologies that occur in minor amounts.

4.3.1 Argillite (<5% greywacke interbeds)

The argillite (<5% greywacke interbeds) unit, referred to here as the “argillite unit”, is expected to comprise 88% of the waste rock (Atlantic, 2006b) and as such, represents the majority of the sample population. Of the ore, 88% is also expected to occur in the argillite unit. In total, 39 argillite samples were collected from the three main areas of the open pit, including: 11 samples from the Western portion; 18 samples from the Central portion; and, 10 samples from the Eastern portion.

ABA results also exist for four samples previously collected by Atlantic and were included into the static results database.

Acid-Base Accounting

Results of the ABA testing for the argillite unit are presented in Table 5 and in Figures 3 through 6. Total sulphur and sulphide content was elevated in the argillite compared to the overall waste rock. The total sulphur content of the argillite samples reached a maximum of 1.6% with an overall average of 0.4% and a median value of 0.25%. As presented in Figure 3, the majority of this sulphur occurs as sulphide for samples containing lower total sulphur concentrations (e.g. <0.3%). As the total sulphur concentration increases, more of the sulphur is attributed to sulphate. The argillite unit has the lowest carbonate concentration compared to the principle rock types with an average concentration of 1.6%. This is slightly below the overall average of 1.8 %.

As can be seen in Figure 4, only a weak correlation exists between the bulk neutralizing potential (NP) and the carbonate neutralizing potential (CaNP), indicating the neutralizing source varies in the argillite unit. It is important to note that for some of the argillite samples, the CaNP is greater than the bulk-NP (Figure 4). This can be attributed to the difference in the determination methods of the two parameters. As described in Section 3.2.1, the bulk-NP (referred to as NP) measured during analysis by acidification of a sample, followed by back titration to determine the

amount of acid consumed. Calculation of CaNP is based on a theoretical stoichiometric conversion assuming all of the carbonate is in the form of calcite. Mineralogical analyses on two argillite samples (06-049 and 06-073) indicate that although the majority of the carbonates take the form of calcite, dolomite (maximum 11.8%) and ankerite (maximum 22.4%) are also present in the samples. Dolomite is less soluble than calcite, and iron and manganese ankerites produce no net neutralizing potential (Price, 1997), thus the CaNP could be overestimated on the basis of the stoichiometric conversion.

Comparing the NP to the acid producing potential (AP) provides an indication of the potential for a sample to generate acidity. CaNP/AP ratios provide a conservative estimate of the acid producing potential of a sample since it excludes the bulk NP component. Acid generation potential was assigned using the CaNP/AP and NP/AP ratios, based on the criteria of Price (1997). Using CaNP/AP, 18 of 39 samples have some potential to produce acidity (Figure 5), whereas only 12 of 39 are identified as having some acid potential using NP/AP ratios (Figure 6). Of the 18 samples that have some potential to produce acidity (i.e. CaNP/AP < 4), two are likely acid generating (CaNP/AP < 1), three are possibly acid generating (CaNP/AP between 1 and 2) and the remaining 13 have low acid producing potentials (CaNP/AP between 2 and 4). Based on these results between 5% and 13% of the samples are expected to be acid generating.

Short Term Leach Testing

Short term leach testing was done on a subset of 17 argillite samples and results of this testing are presented in Table 6 and Figure 7a. Based on the test results, average aluminium (0.4 mg/L) and arsenic (0.2 mg/L) and maximum concentrations of iron (0.4 mg/L), lead (0.0012 mg/L) and zinc (0.08 mg/L) exceeded CCME (1999) guideline values. The maximum concentration of arsenic (1.3 mg/L) exceeded the MMER (2002) guideline value of 0.5 mg/L. These parameters are being considered further as part of a treatment assessment and an overall water quality assessment currently underway.

Net Acid Generation Testing

Nineteen argillite (<5% greywacke) samples were submitted for NAG testing for the purpose of:

- assessing the acid generation potential of samples with “low” to “potential” propensities for acid generation under terminal conditions; and,
- assessing the terminal water quality associated with potentially acid generating and non-acid generating argillite.

NAG-pH is used as a qualitative indicator for acid generation potential under terminal conditions. NAG-pH is measured after the complete oxidation of sulphide minerals and dissolution of NP contributing phases, and as such is a measure of the terminal pH buffering capacity of a sample.

Four out of nineteen samples reported acidic NAG-pH values, less than pH 5 (Table 7). These samples were collected from the Western Pit, and had NP/AP ratios ranging from 0.4 to 1.8. The NAG-pH of samples with “low” to “possible” potentials for acid generation ranged from 6.85 to 10.43. Samples with NP/AP ratios greater than 4 had NAG-pH values that ranged from 7.67 to 10.8.

Three samples were submitted for comprehensive analysis of NAG leachate in order to assess terminal leachate characteristics. Concentrations of several metals exceeded the CCME guideline in potentially acid generating argillite (06-083), including aluminium, arsenic, cadmium copper, iron, nickel, lead, selenium and zinc. Terminal concentrations of aluminium and arsenic exceed the CCME guideline in non-acid generating samples 06-053 and 06-078 and are being further evaluated as part of ongoing work.

Humidity Cell Testing

Four argillite (<5% greywacke) samples were submitted for long-term leach testing: 06-006, 06-017, 06-049 and 06-079. Select results from each humidity cell are presented in Figures 8a through 8d. Complete analytical results are provided in Appendix B.

For discussion purposes, the results are compared to the MMER effluent guidelines and CCME freshwater receiving water guidelines for the protection of aquatic life.

Based on 20 weeks of testing, the data indicate the following:

- All argillite (<5% greywacke) humidity cells had neutral pH, ranging from 7.0 to 8.1 pH units;
- Sulphate concentrations of up to 55 mg/L were measured during the initial flushing of the cells, but have since decreased to a steady-state concentration of approximately 5 mg/L.
- No trace metal concentrations exceeded the MMER effluent guidelines in any of the argillite (<5% greywacke) cells;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L. Dissolved arsenic concentrations ranged from 0.0138 to 0.0481 mg/L in cell 06-006; 0.004 to 0.0276 mg/L in cell 06-049; 0.0341 to 0.106 mg/L in cell 06-079; and, 0.111 to 0.658 mg/L in cell 06-017;
- Dissolved aluminium concentrations were consistently elevated relative to the CCME guideline of 0.1mg/L for samples 06-006 (0.08 to 0.182 mg/L) and 06-049 (0.106 to 0.162 mg/L);
- Trace metals that have not stabilized at steady-state concentrations include zinc and manganese (06-006), zinc and cobalt (06-017), and zinc and lead (06-079). None of these metals occur at concentrations that exceed CCME or MMER criteria;

Depletion calculations were performed using the results of kinetic testing and tabulated in Appendix B-9. The production rate of sulphate and subsequent depletion rate of NP was calculated in order to assess the relative time to depletion of sulphide and NP-bearing minerals. Acidic conditions could result in the long term if NP depletes prior to sulphide.

- The depletion rate of NP exceeds that of AP in samples 06-006 and 06-017, therefore long-term acid generating conditions in these samples is possible; and
- The depletion rate of NP is approximately the same as that of sulphide in 06-049, and sulphide will deplete prior to NP in sample 06-017. NAG testing indicates that terminal leachate resulting from the complete oxidation of sulphide in these samples will not likely have an acidic pH.

The long term leach rates provide valuable input data which is used in the follow-up water quality assessment underway.

4.3.2 Greywacke (<20% argillite interbeds)

The greywacke (<20% argillite interbeds) unit, referred to here as the “greywacke unit”, is expected to account for 2% of the waste rock and ore (Atlantic, 2006b) in the current pit model. Ten samples in total were collected from this unit. All of the samples were collected from the Western portion of the current open pit design. Five existing samples collected by Atlantic were included in the greywacke unit statistical calculations.

Acid-Base Accounting

Results of the ABA testing for the greywacke unit are presented in Table 5 and in Figures 3 through 6. The maximum total sulphur content of the greywacke samples is 0.6%, with an overall average of 0.16%. Sulphide concentrations range from 0.03 to 0.6% and although a positive correlation exists between sulphide and total sulphur, sulphate concentrations also contribute a significant component to the total sulphur and range from 0.002 to 0.3% (Figure 3).

Carbonate concentrations in the greywacke unit range from 1.1 to 3.8% and contribute the majority of the bulk-NP (Figure 4). Compared to the acid producing potential of the greywacke unit (Figures 5 and 6), the greywacke contains sufficient neutralizing potential to buffer acid production and all of the samples are classified as unlikely to produce acidity using the criteria of Price (1997).

Short Term Leach Testing

Leach testing was done on a subset of three greywacke samples and results of this testing are presented in Table 6 and Figure 7b. Based on the test results, average aluminium (0.5 mg/L) and

arsenic (0.09 mg/L) and maximum concentrations of lead (0.0013 mg/L) and zinc (0.08 mg/L) exceeded CCME guideline values.

Net Acid Generation Testing

Three greywacke samples were submitted for NAG testing in order to assess terminal acid generation potential and leachate characteristics. All samples were non-acid generating, according to NP/AP (Table 7). Alkaline NAG-pH values were measured in all samples, indicative of a lack of long-term acid generation potential. Metals that occurred at concentrations exceeding CCME guidelines include aluminium (0.81 to 0.89 mg/L) and arsenic (0.02 to 0.33 mg/L).

Humidity Cell Testing

One sample of greywacke (<20% argillite) was submitted for humidity cell testing. Select results are presented in Figure 9. Full analytical results are provided in Appendix B. The first sixteen weeks of data on sample 06-068 indicate the following:

- The pH in the waste rock humidity cell has remained neutral throughout the duration of testing, ranging from 7.4 to 8.3 pH units;
- Sulphate concentrations initially increased to 32 mg/L during the initial flushing but have since decreased to a steady state concentration of approximately 3 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L, ranging from 0.03 to 0.20 mg/L;
- Dissolved aluminium concentrations were consistently elevated relative to the CCME guideline of 0.1 mg/L, ranging from 0.09 to 0.25 mg/L;
- Concentrations of several trace metals, including cobalt, copper and zinc have not stabilized at steady-state concentrations; and
- Depletion rates of NP and sulphide were calculated using the results of kinetic testing (Appendix B-9). It is possible that mineralogical sources of NP will deplete prior to sulphide, however the low sulphide content of the samples precludes generation of significant acidity, therefore the sample is expected to be non-acid generating in the long term.

4.3.3 Mixed Units

Mixed units at the Touquoy site collectively account for approximately 10% of the waste rock and ore that will be extracted from the open pit during operations (Atlantic, 2006b). For discussion purposes, the following are considered as mixed units: argillite (5-49% greywacke interbeds), greywacke (20-50% argillite interbeds) and composite samples. As the names suggest, the mixed argillite (5-49% greywacke interbeds) contains a higher proportion of greywacke and vice versa for the greywacke (20-50% argillite interbeds). Composite samples of the argillite, greywacke and interbedded units were collected in areas where the variability of these units was too high to be considered as one unit but are considered to provide a significant proportion of rock to the waste pile over that bench interval. The static test results of the three mixed units are discussed individually below.

4.3.4.1 Argillite (5-49% greywacke interbeds)

In total, six samples were collected from the argillite (5-49% greywacke interbeds) unit, referred to here as the “argillite/greywacke unit”. Of the six samples, one was from the Western portion, three were from the Central portion and two were from the Eastern portion relative to the current open pit design. One existing sample collected by Atlantic was included into the argillite/greywacke unit statistical calculations.

Acid-Base Accounting

Results of the ABA testing for the argillite/greywacke unit are presented in Table 5 and in Figures 3 through 6. The maximum total sulphur content of the argillite/greywacke samples is 0.7%, with an overall average of 0.2%. Similar to the argillite unit, there is a stronger correlation between total sulphur and sulphide sulphur for samples with total sulphur concentrations less than 0.3% (Figure 3). Two argillite samples with total sulphur concentrations greater than 0.3% have a relatively greater sulphate sulphur content. Carbonate concentrations in the argillite/greywacke unit range from 1.3 to 2.9%.

On average, the argillite/greywacke unit contains sufficient carbonate to neutralize acid production as a result of sulphide oxidation. Carbonate provides the majority of the neutralizing potential (Figure 4). Using the Price (1997) classification system, none of the samples have the potential to generate acidity based on the CaNP/AP ratio (Figure 5). Sample 06-082 was classified as having a low potential to generate acidity (i.e. $2 < \text{NP/AP} < 4$) relative to the available bulk NP (Figure 6). This particular sample has an elevated CaNP relative to the bulk-NP. It is likely that the CaNP is overestimated for this sample due to the presence of unreactive carbonates, such as ankerite or siderite. This sample should therefore be recognized as having a low potential to produce acidity.

Short Term Leach Testing

Leach testing was done on a subset of three argillite/greywacke samples and results of this testing are presented in Table 6 and Figure 7a. Based on the test results, average aluminum (0.2 mg/L) and arsenic (0.06 mg/L) concentrations have the potential to exceed the CCME guideline values of 0.1 mg/L and 0.005 mg/L respectively. Maximum zinc concentrations also exceeded the CCME guideline value of 0.03 mg/L.

Net Acid Generation Testing

Sample 06-082, which had a “possible” potential for acid generation, was submitted for NAG testing to confirm terminal acid generation characteristics (Table 7). The NAG-pH of this sample was 9.0, which indicates that long-term acid generation from this sample is unlikely. Metals that occurred at concentrations exceeding the CCME guidelines in terminal leachate include aluminium, arsenic, and copper.

Humidity Cell Testing

Select results of long-term leach testing of sample 06-012 are presented in Figure 10. Complete analytical results are provided in Appendix B. Data on sample 06-012 indicate the following:

- Humidity cell leachate has a neutral pH, ranging from 6.9 to 8.2 pH units;
- Sulphate concentrations increased to 40 mg/L during the initial flushing of the cell, but have since stabilized at approximately 2 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L, ranging from 0.01 to 0.02 mg/L;
- Generally, metal concentrations have steadily decreased since the first weeks of flushing of the cells; and,
- The depletion rate of NP exceeds that of sulphide (Appendix B-9), however the low sulphide content of the samples precludes generation of significant acidity, therefore the sample is expected to be non-acid generating in the long term.

4.3.4.2 Greywacke (20-50% argillite interbeds)

In total, twelve samples were collected from the greywacke (20-50% argillite interbeds) unit, referred to here as the “greywacke/argillite unit”. Eleven of the samples were collected from the Central portion and one was collected from the Western portion of the current open pit design. One sample was previously collected by Atlantic and was included in the greywacke/argillite database.

Acid-Base Accounting

Results of the ABA testing for the greywacke/argillite unit are presented in Table 5 and in Figures 3 through 6. The maximum total sulphur content of the greywacke/argillite samples is 0.6%, with an overall average of 0.2%. In general, the majority of the total sulphur can be attributed to the sulphide component (Figure 3). The average sulphate concentrations in the greywacke/argillite unit are 0.05% with a maximum of 0.14%.

Carbonate concentrations in the greywacke/argillite unit range from 1.68 to 3.62%. Although the majority of carbonate concentrations in the greywacke/argillite provide a significant proportion of the bulk-NP (Figure 4), sulphide concentrations were high enough in three of the samples (06-001, 06-039 & DA0472) to produce CaNP/AP ratios less than four (Figure 5). Only one sample (06-039) in the greywacke/argillite unit is classified as possibly acid generating ($1 < \text{NP/AP} < 2$) (Figure 6).

Three samples (06-002, 06-026 & 06-039) had CaNP values greater than bulk-NP (Figure 4). The CaNP of these samples are likely overestimated due to non-reactive carbonate minerals such as ankerite and siderite.

Short Term Leach Testing

Leach testing was done on a subset of two greywacke/argillite samples. The results of this testing are presented in Table 6 and Figure 7b. Based on the test results, average aluminum (0.3 mg/L) and arsenic (0.2 mg/L) were found elevated to the CCME guideline values 0.1 mg/L and 0.005 mg/L respectively. The maximum concentration of lead (0.0012 mg/L) was marginally above the CCME guideline value of 0.001 mg/L.

Net Acid Generation Testing

Three samples were submitted for NAG testing, including two non-acid generating samples ($\text{NP/AP} > 4$), and one potentially acid generating sample ($\text{NP/AP} \sim 2$). The NAG-pH of greywacke/argillite samples ranged from 8.1 to 11.3, indicative of an unlikely propensity for long-term acid generation. Terminal NAG leachates had concentrations of aluminum (0.01 to 2.11 mg/L), arsenic (0.01 to 4.72 mg/L) and zinc (0.003 to 0.03 mg/L) that exceeded CCME guidelines.

Humidity Cell Testing

Select results of kinetic testing of sample 06-039 are presented in Figure 11. Complete analytical results are provided in Appendix B. The data from sample 06-039 indicates the following:

- pH in the waste rock humidity cell ranged from 7.3 to 8.3 pH units;
- Sulphate concentrations ranged from 65 mg/L during the initial flushing of the cell to a stabilized concentration of approximately 5 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L, ranging from 0.05 to 0.41 mg/L;
- Dissolved aluminium concentrations were occasionally elevated relative to the CCME guideline of 0.1mg/L, ranging from 0.04 to 0.14 mg/L;
- Concentrations of arsenic, aluminum, zinc and lead are increasing after 16 weeks of testing; and
- Depletion rates of NP and sulphide, calculated using the results of humidity cell testing (Appendix B-9), indicate that NP will likely deplete prior to sulphide, which may result in long-term acid generating conditions. However, NAG testing of sample 06-039 indicates that terminal water quality, resulting from the complete oxidation of all sulphide minerals and dissolution of NP-contributing phases, will likely have a neutral pH.

4.3.4 Composite Samples

In total, fifteen composite waste rock samples were collected from the Touquoy site. Seven of these were from the Western portion, five from the Central portion and three from the Eastern portion of the current open pit design.

Acid-Base Accounting

Results of the ABA testing for the composite samples are presented in Table 5 and in Figures 3 through 6. The maximum total sulphur content of the composite samples is 0.5%, with an overall average of 0.2% which is lower compared to the other principal lithologies. The majority of the total sulphur can be attributed to sulphide (Figure 3). Similar to other units, samples with total sulphur concentrations greater than 0.3% have a higher preponderance of sulphate. The average sulphate concentration in the composite samples is 0.05% with a maximum of 0.21%.

On average, the composite samples had sufficient carbonate concentrations to neutralize acid production as a result of sulphide oxidation. Using the Price (1997) classification system (See Section 3.2.1), only one sample (06-070) of the fifteen is classified as possibly having the potential to generate acidity based on the CaNP/AP ratio (Figure 5) and relative to the bulk NP (Figure 6). The remaining samples were classified as non-acid generating with average CaNP/AP and NP/AP values of 7.6 and 9.1 respectively.

CaNP and bulk-NP are well correlated (Figure 4) which indicates that most of the neutralising potential comes from carbonate minerals.

Short Term Leach Testing

Leach testing was done on a subset of five composite samples and results of this testing are presented in Table 6 and Figure 7c. Based on the test results, average aluminum (0.3 mg/L) and arsenic (0.06 mg/L) were found elevated to the CCME guideline values of 0.1 mg/L and 0.005 mg/L respectively. The maximum concentration of lead (0.0015 mg/L) was marginally above the CCME guideline value of 0.001 mg/L.

Net Acid Generation Testing

Two composite samples were submitted for NAG testing, one considered non-acid generating based on ABA results and the other with a potential for acid generation. Both samples reported alkaline NAG-pH values (Table 7), which is indicative of an unlikely propensity for long-term acid generation. Aluminium (0.58 to 1.43 mg/L) and arsenic (0.003 to 0.08 mg/L) concentrations exceeded CCME guidelines in NAG leachate.

Humidity Cell Testing

Select results of kinetic testing of samples 06-051 and 06-070 are presented in Figures 12a and 12b. Complete analytical results are provided in Appendix B. The results from samples 06-051 and 06-070 are as follows:

- pH ranges from 7.0 to 7.9 pH units in sample 06-051, and 6.9 to 7.7 in sample 06-070;
- During the initial flushing of cell 06-051, sulphate concentrations increased to 130 mg/L, but have since decreased to around 5 mg/L. The initial sulphate concentration in sample 06-070 peaked at 40 mg/L, and stabilized at approximately 5 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L for sample 06-070, ranging from 0.01 to 0.015 mg/L. Arsenic concentrations rarely exceed the CCME guideline in 06-051, ranging from 0.002 to 0.007 mg/L;
- Generally, metal concentrations have steadily decreased since the first weeks of flushing for sample 06-051, but have increased slightly during week 20. Trace lead concentrations have not stabilized in sample 06-070; and
- The rate of depletion of sulphide exceeds the depletion rate of NP in sample 06-070. NAG testing of this sample indicates that terminal leachate will have a neutral pH. Depletion calculations indicate that sulphide will deplete in approximately the same amount of time required to deplete NP in sample 06-051.

4.3.5 Marginal Ore

It is expected that a marginal ore stockpile will be present on site. Eleven marginal ore samples were collected to quantify the acid producing potential of these materials. The samples were selected over intervals that were dictated by the average grade and were collected where they were available and not according to lithology or location. However, nine of the eleven samples were collected from the argillite unit since this unit host the majority of the ore (approximately 88%). The remaining two samples are composite samples.

Acid-Base Accounting

Results of the ABA testing for the marginal ore samples are presented in Table 5 and in Figures 3 through 6. The maximum total sulphur content of the marginal ore is 0.6%, with an overall average of 0.4%. Sulphide concentrations range from 0.08 to 0.42%. Although a positive correlation exists between sulphide and total sulphur, sulphate concentrations contribute a significant component to the total sulphur, ranging from 0.04 to 0.36% (Figure 3).

Carbonate concentrations range from 0.7 to 2.3%, and contribute the majority of the bulk-NP (Figure 4). Based on the CaNP/AP ratios calculated for the marginal ore samples and employing the criteria of Price (1997), five samples have some potential to produce acidity (Figure 5) whereas only four are identified as having some acid potential using NP/AP ratios (Figure 6). Of the five samples that are described as having some potential to produce acidity (i.e. CaNP/AP < 4), one is possibly acid generating and the remaining four have low acid producing potentials.

One marginal ore sample (06-088) was observed to have a CaNP value greater than bulk-NP value (Figure 4), however some of the CaNP is likely in the form of non-reactive carbonate minerals.

Short Term Leach Testing

Leach testing was done on a subset of three marginal ore samples and results of this testing are presented in Table 6 and Figure 7c. Based on the test results, average aluminum (0.6 mg/L) and arsenic (0.06 mg/L) and maximum concentrations of iron (0.6 mg/L) and zinc (0.07 mg/L) exceeded CCME guideline values.

Net Acid Generation Testing

Four marginal ore samples were submitted for NAG testing. Based on the results of ABA, three samples had a potential for acid generation, and one was considered unlikely to generate acid. All samples reported neutral to alkaline NAG-pH values (Table 7), indicative of an unlikely

potential for long-term acid generation. Aluminum (0.57 to 0.67 mg/L) and arsenic (0.007 to 0.02 mg/L) occurred in concentrations that exceeded the CCME guidelines.

Humidity Cell Testing

Figure 13 presents select results of kinetic testing of sample 06-085. Complete analytical results are provided in Appendix B. The first sixteen weeks of data on sample 06-085 indicate the following:

- pH in the waste rock humidity cell has remained neutral, ranging from 6.6 to 7.7 pH units;
- Sulphate concentrations initially increased to 40 mg/L during the initial flushing but have since decreased to around 10 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations were consistently elevated relative to the CCME guideline of 0.005 mg/L, ranging from 0.008 mg/L to 0.02 mg/L;
- With the exception of zinc and copper, metal concentrations have steadily decreased since the first weeks of flushing; and
- Depletion calculations completed using the results of kinetic testing indicate that sulphide will likely deplete prior to the mineralogical sources of NP; therefore long-term acid generation is unlikely.

4.3.6 Ore

Nine ore samples were previously collected by Atlantic and their acid generating potential was assessed based on ABA testing. Results of this testing are presented in Table 5 and in Figures 3 through 6. Total sulphur concentrations ranged from 0.14 to 0.98% with an average value of 0.48%. Most of the total sulphur was in the form of sulphide (Figure 3). Carbon concentrations in the ore range from 0.8 to 3.27% and account for approximately half of the bulk-NP (Figure 4). Based on the CaNP/AP ratios calculated for the ore samples and employing the criteria of Price (1997), all samples with the exception of one have some potential to produce acidity (Figure 5) whereas only six of the nine are identified as having some acid potential using NP/AP ratios (Figure 6).

4.3.7 Tailings

Results of the elemental analyses for the tailings samples are presented in Tables 3 and 4. XRF analyses indicate that the bulk chemistry of the tailings sample is analogous to the waste rock samples. This is expected since the ore is disseminated throughout the sedimentary rock as opposed to being associated with post-depositional veining (Atlantic, 2006a). ICP trace element analyses indicate that the arsenic concentration in tailings and head composite samples is elevated

(160 ppm to 1300) ppm relative to the average crustal abundances for clastic sedimentary rocks (Price, 1997). The following metals were also elevated in the tailings sample relative to the overall sample averages and compared to the average crustal abundances: chromium, copper, manganese and molybdenum.

Acid-Base Accounting

Results of the ABA testing for the tailings samples are presented in Table 5 and in Figures 3 through 6. The sulphide content of the tailings samples ranges from 0.03 to 0.12 wt. % sulphide (Figure 3). The tailings samples have sufficient carbonate concentrations (0.7 to 1.6 %), which provided the majority of the neutralizing potential (Figure 4), to neutralize acid production as a result of sulphide oxidation. Using the Price (1997) classification system, the tailings are not expected to be acid generating due to the lack of sulphide minerals and the availability of carbonate minerals.

Supernatant Aging Results

Tailings supernatant water, generated during leaching and detoxification of the ore head sample, was retained and scanned on the following days: 0, 3, 7, 14, 31 and 45 for selected parameters. Results of this testing are presented in Table 8. Likewise, tailings supernatant water from treatment of the TWB sample was scanned on days: 0, 1, 3, 7, 15, 30 and 44. Results of this testing are presented in Table 9. The purpose of the aging test analyses was to describe the natural attenuation of various parameters through time and to quantify the water quality of the process water being discharged to the tailings management facility. It appears that for CND 2, on day 31 several of the parameter concentrations and instrument detection limits increased as a result of an analytical or reporting error. Results from day 31 are therefore not included in the following discussion. Although the process water will not be discharged directly to the environment, for discussion purposes, aging test results were compared to the MMER effluent guidelines and CCME freshwater receiving water guidelines for the protection of aquatic life.

Weak acid dissociable cyanide (CN-wad) concentrations in the tailings were detoxified to <1 ppm for sample CND 2. For sample CN1 CND1-7 detoxification to 10 ppm cyanide was attempted to evaluate degradation rates of this higher cyanide concentration, however the cyanide destruction process for the tailings samples consistently resulted in total cyanide concentrations of less than 1 ppm. This is less than the MMER guideline value of 1.0 mg/L for total cyanide (CN-tot). Therefore, concentrations of CN-tot in the tailings supernatant water never exceeded this limit during the test period. As opposed to the MMER guideline, the CCME guideline of 0.005 mg/L governs the maximum allowable concentration of free cyanide (CN-free). In the analysis of the tailings supernatant water from the master composite sample (CND2), a CN-free detection limit of <0.03 to <0.05 mg/L was used. Since CN-free concentrations remained below detection throughout the test period, for comparison purposes, CN-wad was compared to the CCME

guideline value. CN-wad ranged from 0.03 to 0.04 mg/L, which is above the maximum allowable concentration, however natural degradation of cyanide in the polishing pond will occur and is expected to result in significant additional reduction in these values. Cyanide concentrations are currently under further evaluation in the context of the overall site water quality.

All of the measured parameters from the tailings supernatant waters met the MMER effluent guidelines with the exception of dissolved arsenic on CND 2 - day 0 (0.53 mg/L); dissolved arsenic for CN1 CND1-7 day 1 (0.9 mg/L) and copper for CN1 CND1-7 day 0,1,3 and 7 (1.2, 1.2, 1.2, and 0.8 mg/L respectively). The CCME values for discharge of arsenic and copper are 0.5 mg/L and 0.3 mg/L respectively. It is expected that treatment of arsenic will result in significant reductions of both of these concentrations, and other concentrations prior to discharge of the waters.

All of the total and dissolved parameters from the supernatant solutions are being assessed within the context of the overall site discharge water quality.

Humidity Cell Testing

Humidity cell results from the tailings samples CN1 CND1-7 and CND 2 are shown in Figures 14 and 15 for select parameters. Results from the master composite sample (CND 2), expected to be representative of the overall tailings products, indicate the following:

- pH in the tailings humidity cell has remained slightly acidic to neutral, ranging from 6.3 to 7.8 pH units for CN1 CND1-7 and from 6.9 to 7.8 pH units for CND 2;
- Sulphate concentrations initially peaked at 50 mg/L for CN1 CND1-7 and increased to 100 mg/L during week two for CND 2, but have since decreased to around 20 mg/L;
- No metal concentrations exceeded the MMER effluent guidelines;
- Dissolved arsenic concentrations ranged from 0.009 to 0.07 mg/L for CN1 CND1-7 and from 0.003 to 0.05 mg/L for CND 2. The steady state concentration of arsenic for CND 2 was approximately 0.005 mg/L, which is equal to the CCME guideline;
- Dissolved copper concentrations were elevated relative to the CCME guideline of 0.002 mg/L during the initial flushing with 0.002 to 0.004 mg/L for CN1 CND1-7 and 0.004 mg/L for CND 2;
- There is insufficient data to show trends for sample CN1 CND1-7. Generally, metal concentrations have steadily decreased since the first weeks of flushing for CND2 (except for manganese); and,
- There is not sufficient data to calculate depletion rates for CN1 CND1-7. Depletion calculations completed using the results of kinetic testing indicate that sulphide will likely deplete prior to the mineralogical sources of NP for CND 2. Based on the

depletion rates and the low sulphide content it is considered that the tailings will be non-acid generating in the long-term.

Suspended Solids

In addition to standard testing the suspended solids of the CND2 (Master Composite) treated solution from the tailings was measured at day 7 following production and found to be 29 mg/L. Treatment is expected to further result in reductions in TSS concentrations.

4.3.8 Minor Units

Quartz veining occurs randomly within waste rock materials. One sample of the quartz vein was collected to characterize the acid producing potential of this material. Since this is considered to be a minor unit relative to the other lithologies, only ABA testing was done and no leach testing was done on this sample to assess the acid generating potential of the sample. Results of this testing are provided in Table 5 and Figures 3 through 6 and are summarized as follows.

The total sulphur content of the quartz vein was 0.4%, of which 0.3% was attributed to sulphide and the remaining 0.1% to sulphate (Figure 3). The carbonate concentration of the quartz sample was 1.1% and accounts for the majority of the bulk-NP (Figure 4). When the neutralizing potentials of this sample are compared to the acid producing potential, the CaNP/AP ratio (1.9) indicates this sample is possibly acid generating (Figure 5) whereas the NP/AP ratio (2.8) indicates the quartz vein has low acid producing potential (Figure 6).

One quartz vein sample was submitted for NAG testing to confirm long-term acid generation potential. This sample had a NAG-pH of 9.0, and is considered unlikely to generate acid in the long-term.

4.4 Discussion of Overall Results

With respect to the overall materials evaluated, mineralogy and solids analysis indicate that calcite is the dominant control on buffering capacity. This suggests that even at NPR's between 2 and 4, net neutral conditions will likely be realized since calcite is quite effective at providing neutralizing capacity, as confirmed by the NAG test results.

Arsenic is the main parameter of concern at the Touquoy project and has the potential to exceed both the MMER guideline value of 0.5 mg/L and the CCME guideline values of 0.005 mg/L (Figure 16). Figure 16 is a plot of the solid arsenic component versus the dissolved concentrations derived from the short-term leach testing. It is important to understand that leach testing occurs under limited oxidization potential and only the readily available arsenic will be leached. The Lakefield (2006) mineralogy report indicates that arsenopyrite is a significant

sulphide component in the Touquoy waste rock materials and is mainly liberated or exposed. Therefore, the majority of arsenopyrite is readily available to be oxidized and during this process additional arsenic may be released under oxidizing conditions, as is observed in the NAG test results.

Although some parameters exceed the CCME guidelines in the short-term leach testing, supernatant aging tests and in the tailings humidity cell, this water is not expected to be discharged directly to the environment. Furthermore, apart from arsenic (As) concentrations, no other metals were found to exceed MMER levels. A detailed water quality assessment in the context of the site wide water balance currently underway.

5.0 CONCLUSIONS AND RECOMMENDATIONS

Overall waste rock units have similar solid chemistries and the geochemical behaviour of the units is expected to be similar. The units are therefore only distinguished based on grain size, and the greywacke and argillite of the Touquoy deposit are likely derived from similar host rocks. A review of the expected waste rock tonnages in Table 1 relative to the distribution of selected samples show the lithological distribution of samples provides a reasonable representation of the respective rock types and tonnages anticipated to be encountered in the pit based on the information available.

With respect to acid generation, the Touquoy site is significantly different from other maritime mining projects such as Voisey's Bay, or from around Halifax. The rock sequences at Touquoy do not contain the massive sulphides of a Voisey Bay type deposit, nor do they contain the sulphide rich slates of the Halifax Formation which are responsible for ARD at the Halifax Airport. Overall sulphide contents at the Touquoy project are low.

Given that only a small proportion of the potential waste materials are acid generating (2% based on samples collected to date), and given that the majority of buffering minerals are carbonate minerals for which excess neutralization potential is readily available, it is considered that overall the waste materials from the Touquoy project will be non acid generating with excess neutralizing capacity.

Additional evidence that AG will not be prevalent is available from the NAG testing completed as well as the bulk sample pit on site. The water quality from this pit remains neutral after several years exposed to the environment (Atlantic 2007 – pers. Com with Peter Carter), confirmation sampling of the water quality in this pit should be completed periodically.

Results of the trace metal analyses and leach test results indicate arsenic is the main parameter of concern for the Touquoy project. With respect to water quality values, based on the short term testing, NAG test results, and humidity test cell results, overall, values of long term and short term leachate for most parameters are neutral with low concentrations of dissolved parameters relative to other mining properties. Although some parameters (e.g. Al, As, Zn) are elevated in the short term and longer term leach testing it is important to keep in mind that these values must be taken in the context of the overall site water quality and potential site discharge. Evaluation of these parameters is currently underway as part of an overall site water quality model.

Based on the results and conclusions as presented herein recommendations are as follows:

- As opportunity presents itself (as infilling drilling occurs) a few additional confirmation samples of fresh rock in the western zones of the pit should be collected and analysed for sulphide content. Should the pit design change, the sample set and analytical results will

need to be reviewed to determine if supplementary collection and geochemical characterization of samples is required.

- Monitoring should include periodic evaluation of conditions on site with respect to visual indicators of acid generating conditions such as ferric hydroxide precipitation on the waste materials and in water courses or streams.
- Monitoring of water quality from the site and tailings should be conducted regularly during operations and for a period after closure.
- Management strategies for waste rock and tailings should be re-evaluated periodically during operations and adjusted or updated if necessary based on the results of the monitoring data.

Should acid generation be observed in the materials on the surface of the pile, it is considered that the overall NP of the pile will limit vertical migration of acidic conditions in the pile. Mitigation/remediation of these small areas of the pile would involve relocation of the acid generating materials, within areas of the pile that are non-acid generating, or covering the materials to maintain clean surface runoff and limit oxidation of the materials.

It is recommended that appropriate treatment options for arsenic and other parameters be implemented if deemed necessary once an evaluation of overall site water quality is completed. This overall water quality evaluation, and an evaluation of treatment options is currently underway.

GOLDER ASSOCIATES LTD.

Original signed by:

Aurelia Lebegin, M.Sc.
Project Scientist

Original signed by:

Ken DeVos, M.Sc., P.Geo
Associate, Hydrogeochemist

AL/MKH/KJD/co/dh

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TABLES

Table 1
Summary of Ore and Waste Rock Tonnes

| Lithology | Expected Rock Tonnes | Tonnage | | Percentage | | Number of Samples Collected | | | Waste Rock and Tailings Testing Analysis | | | | | | | | |
|--|----------------------|-----------|------------|------------|-------|-----------------------------|-----------------------|---------|--|--------------------|-----------------------------|-----|------------|-------------------|---------------|----|----|
| | | Ore | Waste | Ore | Waste | Individual Samples | Atlantic Gold Samples | Total | Modified ABA | Trace Metals (CFP) | Whole Rock Short-Term Leach | MAG | Microscopy | Supernatant Aging | Hardness Data | | |
| | | | | | | Western | Central | Eastern | | | | | | | | | |
| Argillite (<5% greywacke interbeds) | 21,208,000 | 6,688,000 | 14,520,000 | 88% | 88% | 11 | 18 | 10 | 4 | 43 | 43 | 7 | 7 | 6 | 3 | 2 | 4 |
| Argillite (5-49% greywacke interbeds) | | | | | | 1 | 3 | 2 | 1 | 7 | 7 | 7 | 7 | 6 | 3 | 1 | 1 |
| Greywacke (20-50% argillite interbeds) | 2,410,000 | 760,000 | 1,650,000 | 10% | 10% | 1 | 11 | - | 1 | 13 | 13 | 13 | 13 | 12 | 2 | 1 | 1 |
| Composite Samples | | | | | | 7 | 5 | 3 | - | 15 | 15 | 15 | 15 | 15 | 5 | 2 | 2 |
| Greywacke (<20% argillite interbeds) | 482,000 | 152,000 | 330,000 | 2% | 2% | 10 | - | - | 5 | 15 | 15 | 15 | 15 | 10 | 3 | 2 | 1 |
| Massive Quartz Vein | - | - | - | - | - | - | 1 | - | - | 1 | 1 | 1 | 1 | 1 | - | - | - |
| Marginal Ore | - | - | - | - | - | - | - | - | - | 11 | 11 | 11 | 11 | 11 | 3 | 2 | 1 |
| Ore | 7,600,000 | 7,600,000 | - | 100% | 0% | - | - | - | 9 | 9 | 9 | 9 | 9 | - | - | - | - |
| Tailings | - | - | - | - | - | - | - | - | - | 7 | 7 | 7 | 7 | 7 | 6 | 6 | 2 |
| Total | 24,100,000 | 7,600,000 | 16,500,000 | 100% | 100% | 30 | 38 | 15 | 20 | 121 | 121 | 121 | 121 | 101 | 39 | 18 | 12 |

Note:
Expected ore and waste tonnages provided by Atlantic (2006).

Table 2
Summary of Samples Collected for Geochemical Testing

| Sample # | Hole # | Section | Location | From (m) | To (m) | Lithology | Lithological Description |
|-------------------------------------|-----------|------------|-------------|----------|--------|-----------|--|
| ARGILLITE (5-49%) GREYWACKE | | | | | | | |
| 06-012 | MR-04-039 | 21900 East | Central Pit | 14 | 17 | A/G | Argillite with 5-49% greywacke interbeds |
| 06-016 | MR-04-039 | 21900 East | Central Pit | 50 | 59 | A/G | Argillite with 5-49% greywacke interbeds |
| 06-021 | MR-05-101 | 21900 East | Central Pit | 12 | 15 | A/G | Argillite with 5-49% greywacke interbeds |
| 06-040 | MR-05-125 | 22075 East | Eastern Pit | 11 | 15 | A/G | Argillite with 5-49% greywacke interbeds |
| 06-042 | MR-03-018 | 22075 East | Eastern Pit | 15 | 25 | A/G | Argillite with 5-49% greywacke interbeds |
| 06-082 | MR-03-002 | 21650 East | Western Pit | 15 | 19 | A/G | Argillite with 5-49% greywacke interbeds |
| ARGILLITE (<5% GREYWACKE) | | | | | | | |
| 06-004 | MR-05-114 | 21975 East | Central Pit | 10 | 20 | AR | Argillite (<5% Greywacke) |
| 06-005 | MR-05-105 | 21975 East | Central Pit | 35 | 45 | AR | Argillite (<5% Greywacke) |
| 06-006 | MR-05-106 | 21975 East | Central Pit | 15 | 25 | AR | Argillite (<5% Greywacke) |
| 06-009 | MR-05-071 | 21975 East | Central Pit | 20 | 30 | AR | Argillite (<5% Greywacke) |
| 06-010 | MR-05-071 | 21975 East | Central Pit | 40 | 50 | AR | Argillite (<5% Greywacke) |
| 06-014 | MR-04-039 | 21900 East | Central Pit | 26 | 35 | AR | Argillite (<5% Greywacke) |
| 06-017 | MR-05-102 | 21900 East | Central Pit | 10 | 20 | AR | Argillite (<5% Greywacke) |
| 06-019 | MR-05-102 | 21900 East | Central Pit | 48 | 58 | AR | Argillite (<5% Greywacke) |
| 06-022 | MR-05-101 | 21900 East | Central Pit | 15 | 21 | AR | Argillite (<5% Greywacke) |
| 06-025 | MR-05-100 | 21900 East | Central Pit | 12.5 | 20 | AR | Argillite (<5% Greywacke) |
| 06-028 | MR-05-100 | 21900 East | Central Pit | 58 | 68 | AR | Argillite (<5% Greywacke) |
| 06-029 | MR-05-103 | 21900 East | Central Pit | 5 | 15 | AR | Argillite (<5% Greywacke) |
| 06-030 | MR-05-103 | 21900 East | Central Pit | 30 | 40 | AR | Argillite (<5% Greywacke) |
| 06-031 | MR-05-093 | 21900 East | Central Pit | 11 | 21 | AR | Argillite (<5% Greywacke) |
| 06-032 | MR-05-092 | 21900 East | Central Pit | 20 | 30 | AR | Argillite (<5% Greywacke) |
| 06-033 | MR-05-092 | 21900 East | Central Pit | 30 | 40 | AR | Argillite (<5% Greywacke) |
| 06-036 | MR-05-091 | 21900 East | Central Pit | 39 | 44 | AR | Argillite (<5% Greywacke) |
| 06-038 | MR-05-091 | 21900 East | Central Pit | 49 | 59 | AR | Argillite (<5% Greywacke) |
| 06-041 | MR-05-125 | 22075 East | Eastern Pit | 15 | 25 | AR | Argillite (<5% Greywacke) |
| 06-043 | MR-03-018 | 22075 East | Eastern Pit | 33 | 42 | AR | Argillite (<5% Greywacke) |
| 06-044 | MR-03-018 | 22075 East | Eastern Pit | 60 | 70 | AR | Argillite (<5% Greywacke) |
| 06-046 | MR-05-120 | 22075 East | Eastern Pit | 25 | 35 | AR | Argillite (<5% Greywacke) |
| 06-047 | MR-03-019 | 22075 East | Eastern Pit | 17 | 23 | AR | Argillite (<5% Greywacke) |
| 06-048 | MR-03-021 | 22075 East | Eastern Pit | 20 | 28 | AR | Argillite (<5% Greywacke) |
| 06-049 | MR-05-122 | 22075 East | Eastern Pit | 10 | 20 | AR | Argillite (<5% Greywacke) |
| 06-050 | MR-05-122 | 22075 East | Eastern Pit | 25 | 35 | AR | Argillite (<5% Greywacke) |
| 06-053 | MR-03-024 | 22075 East | Eastern Pit | 14 | 23 | AR | Argillite (<5% Greywacke) |
| 06-054 | MR-05-124 | 22075 East | Eastern Pit | 15 | 25 | AR | Argillite (<5% Greywacke) |
| 06-067 | MR-05-084 | 21650 East | Western Pit | 125 | 130 | AR | Argillite (<5% Greywacke) |
| 06-071 | MR-05-083 | 21675 East | Western Pit | 91 | 98 | AR | Argillite (<5% Greywacke) |
| 06-073 | MR-05-094 | 21625 East | Western Pit | 12 | 22 | AR | Argillite (<5% Greywacke) |
| 06-074 | MR-05-094 | 21625 East | Western Pit | 45 | 55 | AR | Argillite (<5% Greywacke) |
| 06-076 | MR-05-094 | 21625 East | Western Pit | 100 | 105 | AR | Argillite (<5% Greywacke) |
| 06-077 | MR-03-001 | 21650 East | Western Pit | 11 | 20 | AR | Argillite (<5% Greywacke) |
| 06-078 | MR-03-001 | 21650 East | Western Pit | 32 | 40 | AR | Argillite (<5% Greywacke) |
| 06-079 | MR-03-001 | 21650 East | Western Pit | 50 | 59 | AR | Argillite (<5% Greywacke) |
| 06-080 | MR-03-001 | 21650 East | Western Pit | 59 | 65 | AR | Argillite (<5% Greywacke) |
| 06-083 | MR-03-002 | 21650 East | Western Pit | 32 | 37 | AR | 39.08-40=GW |
| 06-084 | MR-03-002 | 21650 East | Western Pit | 59 | 65 | AR | Argillite (<5% Greywacke) |
| COMPOSITE | | | | | | | |
| 06-007 | MR-05-107 | 21975 East | Central Pit | 12 | 22 | composite | Composite of Greywacke and Argillite |
| 06-018 | MR-05-102 | 21900 East | Central Pit | 27 | 37 | composite | Composite of Greywacke and Argillite |
| 06-023 | MR-05-101 | 21900 East | Central Pit | 27 | 36 | composite | Composite of Greywacke and Argillite |
| 06-027 | MR-05-100 | 21900 East | Central Pit | 25 | 35 | composite | Composite of Greywacke and Argillite |
| 06-035 | MR-05-091 | 21900 East | Central Pit | 22 | 28 | composite | Composite of Greywacke and Argillite |
| 06-045 | MR-05-120 | 22075 East | Eastern Pit | 11 | 20 | composite | Composite of Greywacke and Argillite |
| 06-051 | MR-03-023 | 22075 East | Eastern Pit | 11 | 21 | composite | Composite of Greywacke and Argillite |
| 06-052 | MR-05-123 | 22075 East | Eastern Pit | 12 | 22 | composite | Composite of Greywacke and Argillite |
| 06-055 | MR-05-085 | 21650 East | Western Pit | 3 | 11 | composite | Composite of Greywacke and Argillite |
| 06-058 | MR-05-085 | 21650 East | Western Pit | 28 | 38 | composite | Composite of Greywacke and Argillite |
| 06-059 | MR-05-085 | 21650 East | Western Pit | 61 | 67 | composite | Composite of Greywacke and Argillite |
| 06-062 | MR-05-084 | 21650 East | Western Pit | 3 | 13 | composite | Composite of Greywacke and Argillite |
| 06-064 | MR-05-084 | 21650 East | Western Pit | 32 | 42 | composite | Composite of Greywacke and Argillite |
| 06-069 | MR-05-083 | 21675 East | Western Pit | 30 | 40 | composite | Composite of Greywacke and Argillite |
| 06-070 | MR-05-083 | 21675 East | Western Pit | 68 | 74.5 | composite | Composite of Greywacke and Argillite |

Table 2
Summary of Samples Collected for Geochemical Testing

| Sample # | Hole # | Section | Location | From (m) | To (m) | Lithology | Statistics |
|--|-----------|------------|--------------|----------|--------|-----------|--|
| GREYWACKE (20%-50% ARGILLITE INTERBEDS) | | | | | | | |
| 06-001 | MR-05-128 | 21975 East | Central Pit | 7 | 17 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-002 | MR-05-128 | 21975 East | Central Pit | 23 | 33 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-003 | MR-05-128 | 21975 East | Central Pit | 35 | 45 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-011 | MR-04-039 | 21900 East | Central Pit | 6 | 14 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-013 | MR-04-039 | 21900 East | Central Pit | 17 | 24 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-015 | MR-04-039 | 21900 East | Central Pit | 35 | 40 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-020 | MR-05-101 | 21900 East | Central Pit | 4 | 9 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-024 | MR-05-100 | 21900 East | Central Pit | 6 | 10 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-026 | MR-05-100 | 21900 East | Central Pit | 20 | 24 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-034 | MR-05-091 | 21900 East | Central Pit | 10 | 20 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-039 | MR-04-049 | 21850 East | Central Pit | 10 | 20 | G/A | Greywacke with 20-50% argillite interbeds |
| 06-057 | MR-05-085 | 21650 East | Western Pit | 20 | 28 | G/A | Greywacke with 20-50% argillite interbeds |
| GREYWACKE (<20% ARGILLITE INTERBEDS) | | | | | | | |
| 06-056 | MR-05-085 | 21650 East | Western Pit | 11 | 19 | GW | Greywacke with <20% argillite interbeds |
| 06-060 | MR-05-085 | 21650 East | Western Pit | 75 | 85 | GW | Greywacke with <20% argillite interbeds |
| 06-061 | MR-05-085 | 21650 East | Western Pit | 90 | 100 | GW | Greywacke with <20% argillite interbeds |
| 06-063 | MR-05-084 | 21650 East | Western Pit | 14 | 24 | GW | Greywacke with <20% argillite interbeds |
| 06-065 | MR-05-084 | 21650 East | Western Pit | 42 | 52 | GW | Greywacke with <20% argillite interbeds |
| 06-066 | MR-05-084 | 21650 East | Western Pit | 65 | 72 | GW | Greywacke with <20% argillite interbeds |
| 06-068 | MR-05-083 | 21675 East | Western Pit | 5 | 15 | GW | Greywacke with <20% argillite interbeds |
| 06-072 | MR-05-083 | 21675 East | Western Pit | 100 | 110 | GW | Greywacke with <20% argillite interbeds |
| 06-075 | MR-05-094 | 21625 East | Western Pit | 85 | 95 | GW | Greywacke with <20% argillite interbeds |
| 06-081 | MR-03-002 | 21650 East | Western Pit | 5 | 15 | GW | Greywacke with <20% argillite interbeds |
| MARGINAL ORE | | | | | | | |
| 06-008 | MR-05-071 | 21975 East | Marginal Ore | 3 | 13 | AR | Argillite (<5% Greywacke) - marginal ore |
| 06-085 | MR-05-107 | 21975 East | Marginal Ore | 45 | 50 | AR | Argillite (<5% Greywacke) |
| 06-086 | MR-05-118 | 22150 East | Marginal Ore | 32 | 36 | AR | Argillite (<5% Greywacke) |
| 06-087 | MR-05-092 | 21900 East | Marginal Ore | 9 | 13 | AR | Argillite (<5% Greywacke) |
| 06-088 | MR-05-080 | 21725 East | Marginal Ore | 34 | 42 | AR | Argillite (<5% Greywacke) |
| 06-089 | MR-04-054 | 21775 East | Marginal Ore | 12 | 16 | composite | Composite of Greywacke and Argillite |
| 06-090 | MR-03-019 | 22075 East | Marginal Ore | 42 | 45 | AR | Argillite (<5% Greywacke) |
| 06-091 | MR-05-121 | 22075 East | Marginal Ore | 17 | 19 | AR | Argillite (<5% Greywacke) |
| 06-092 | MR-05-116 | 22150 East | Marginal Ore | 39 | 48 | AR | Argillite (<5% Greywacke) |
| 06-093 | MR-05-083 | 21775 East | Marginal Ore | 111 | 115 | AR | Argillite (<5% Greywacke) |
| 06-094 | MR-04-058 | 21775 East | Marginal Ore | 13 | 17 | composite | Composite of Greywacke and Argillite |
| QUARTZ VEIN | | | | | | | |
| 06-037 | MR-05-091 | 21900 East | Central Pit | 44 | 47 | QV | Massive Quartz Vein (>50% of interval) |
| TAILINGS | | | | | | | |
| CND2 Treated Solids (Master Composite) | - | - | - | - | - | - | Generated by SGS Lakefield using TAM master composite provided by Atlantic Gold. (Composite of TWT, TWM, TWB, TET & TEB) - Lakefield ID "CND2 Treated Solids" |
| TWT | - | - | - | - | - | - | Argillite location composite - western section top. |
| TWM | - | - | - | - | - | - | Argillite location composite - western section middle. |
| TWB CN Feed | - | - | - | - | - | - | Argillite location composite - western section bottom. |
| TET | - | - | - | - | - | - | Argillite location composite - eastern section top. |
| TEB | - | - | - | - | - | - | Argillite location composite - eastern section bottom. |
| CN1 CND 1-7 Solids (TWB) | - | - | - | - | - | - | Generated by SGS Lakefield using 20kg sample of TWB (Argillite location composite - western section bottom) as provided by Metcon Labs - Lakefield ID "CN1 CND 1-7 Solids". "CND 1-7" indicates that this is a composite sample of the 7 different tests done. |

Notes:

TAM - Master Argillite Composite containing equal amounts of TWT, TWM, TWB, TET and TEB

AR - Argillite (<5% Greywacke)

A/G - Argillite with 5-49% greywacke interbeds

GW - Greywacke with <20% argillite interbeds

G/A - Greywacke with 20-50% argillite interbeds

QV - Massive Quartz Vein (>50% of interval)

Table 3
Summary of Whole Rock Results

| Sample # | Statistics | SiO ₂ (%) | Al ₂ O ₃ (%) | Fe ₂ O ₃ (%) | MgO (%) | CaO (%) | Na ₂ O (%) | K ₂ O (%) | TI0 ₂ (%) | P ₂ O ₅ (%) | MnO (%) | Cr ₂ O ₃ (%) | V ₂ O ₅ (%) | LOI (%) | Sum (%) |
|---|---|----------------------|------------------------------------|------------------------------------|---------|---------|-----------------------|----------------------|----------------------|-----------------------------------|---------|------------------------------------|-----------------------------------|---------|---------|
| ARGILLITE (5-49% GREYWACKE) | | | | | | | | | | | | | | | |
| | Minimum | 57.1 | 15.20 | 6.90 | 1.86 | 0.87 | 1.06 | 2.87 | 0.77 | 0.30 | 0.10 | 0.01 | 0.01 | 4.26 | 98.2 |
| | Maximum | 63.0 | 19.50 | 8.38 | 2.51 | 2.57 | 2.07 | 4.16 | 1.06 | 0.15 | 0.14 | 0.02 | 0.03 | 5.27 | 99.4 |
| | Average | 59.6 | 17.03 | 7.47 | 2.21 | 1.92 | 1.50 | 3.38 | 0.90 | 0.12 | 0.12 | 0.01 | 0.02 | 4.56 | 98.9 |
| | Standard Deviation | 2.4 | 1.67 | 0.53 | 0.23 | 0.64 | 0.37 | 0.53 | 0.11 | 0.02 | 0.01 | 0.00 | 0.01 | 0.40 | 0.47 |
| | Median | 59.1 | 17.15 | 7.33 | 2.23 | 2.01 | 1.51 | 3.22 | 0.88 | 0.12 | 0.11 | 0.01 | 0.01 | 4.38 | 99.0 |
| | Count | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| ARGILLITE (<5% GREYWACKE) | | | | | | | | | | | | | | | |
| | Minimum | 52.5 | 16.10 | 7.10 | 2.07 | 0.30 | 0.11 | 3.10 | 0.74 | 0.09 | 0.06 | 0.01 | 0.01 | 3.68 | 97.1 |
| | Maximum | 63.0 | 20.10 | 9.40 | 3.32 | 1.77 | 1.58 | 5.06 | 1.04 | 0.13 | 0.15 | 0.04 | 0.03 | 5.65 | 99.7 |
| | Average | 57.4 | 18.33 | 8.30 | 2.54 | 1.39 | 0.75 | 4.17 | 0.93 | 0.11 | 0.11 | 0.01 | 0.02 | 4.46 | 98.5 |
| | Standard Deviation | 2.2 | 0.99 | 0.58 | 0.26 | 0.48 | 0.28 | 0.56 | 0.06 | 0.01 | 0.02 | 0.01 | 0.01 | 0.41 | 0.58 |
| | Median | 57.4 | 18.40 | 8.21 | 2.49 | 1.33 | 0.79 | 4.12 | 0.93 | 0.11 | 0.10 | 0.01 | 0.02 | 4.43 | 98.6 |
| | Count | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 | 39 |
| COMPOSITE | | | | | | | | | | | | | | | |
| | Minimum | 56.9 | 14.40 | 5.08 | 1.91 | 0.50 | 1.00 | 2.57 | 0.72 | 0.09 | 0.09 | 0.01 | 0.01 | 3.62 | 98.3 |
| | Maximum | 65.1 | 18.30 | 8.17 | 2.48 | 6.68 | 2.32 | 3.97 | 1.00 | 0.16 | 0.21 | 0.03 | 0.03 | 7.29 | 100 |
| | Average | 59.8 | 17.09 | 7.10 | 2.16 | 2.19 | 1.52 | 3.46 | 0.92 | 0.12 | 0.12 | 0.01 | 0.02 | 4.53 | 99.0 |
| | Standard Deviation | 2.0 | 1.22 | 0.81 | 0.18 | 1.50 | 0.32 | 0.37 | 0.08 | 0.02 | 0.03 | 0.01 | 0.01 | 0.93 | 0.46 |
| | Median | 59.2 | 17.30 | 7.37 | 2.21 | 1.71 | 1.50 | 3.51 | 0.94 | 0.12 | 0.12 | 0.01 | 0.01 | 4.39 | 98.9 |
| | Count | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| GREYWACKE (20%-50% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | | |
| | Minimum | 55.5 | 11.70 | 3.85 | 0.95 | 1.18 | 0.87 | 1.68 | 0.74 | 0.08 | 0.09 | 0.01 | 0.01 | 3.41 | 96.4 |
| | Maximum | 70.8 | 19.60 | 9.08 | 2.57 | 3.89 | 2.77 | 4.23 | 0.99 | 0.14 | 0.15 | 0.02 | 0.03 | 4.92 | 99.7 |
| | Average | 63.4 | 15.26 | 6.17 | 1.79 | 2.19 | 1.93 | 2.86 | 0.87 | 0.11 | 0.11 | 0.01 | 0.02 | 4.09 | 98.9 |
| | Standard Deviation | 4.2 | 2.30 | 1.40 | 0.43 | 0.82 | 0.56 | 0.76 | 0.59 | 0.02 | 0.02 | 0.00 | 0.01 | 0.51 | 0.41 |
| | Median | 63.7 | 15.09 | 6.22 | 1.74 | 1.89 | 2.11 | 2.79 | 0.88 | 0.10 | 0.11 | 0.01 | 0.02 | 4.04 | 98.8 |
| | Count | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| GREYWACKE (<20% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | | |
| | Minimum | 63.1 | 11.60 | 3.87 | 1.08 | 1.21 | 0.05 | 1.31 | 0.58 | 0.07 | 0.08 | 0.01 | 0.01 | 2.63 | 97.2 |
| | Maximum | 71.0 | 15.30 | 5.88 | 2.33 | 4.06 | 3.14 | 3.38 | 0.89 | 0.15 | 0.13 | 0.02 | 0.02 | 4.51 | 100 |
| | Average | 67.8 | 13.29 | 4.67 | 1.56 | 2.33 | 2.42 | 2.16 | 0.74 | 0.11 | 0.10 | 0.01 | 0.01 | 3.65 | 98.9 |
| | Standard Deviation | 2.5 | 1.10 | 0.68 | 0.38 | 0.97 | 0.89 | 0.65 | 0.11 | 0.03 | 0.02 | 0.00 | 0.00 | 0.65 | 0.89 |
| | Median | 68.3 | 13.00 | 4.54 | 1.55 | 2.06 | 2.63 | 2.10 | 0.73 | 0.12 | 0.10 | 0.01 | 0.01 | 3.65 | 98.9 |
| | Count | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| MARGINAL ORE | | | | | | | | | | | | | | | |
| | Minimum | 55.8 | 15.70 | 5.41 | 1.46 | 0.68 | 0.18 | 3.14 | 0.80 | 0.09 | 0.08 | 0.01 | 0.01 | 3.58 | 97.7 |
| | Maximum | 65.3 | 18.70 | 9.06 | 2.85 | 2.24 | 1.94 | 4.51 | 0.92 | 0.13 | 0.11 | 0.03 | 0.03 | 4.58 | 99.8 |
| | Average | 59.8 | 17.81 | 7.76 | 2.39 | 1.56 | 0.79 | 4.06 | 0.89 | 0.11 | 0.10 | 0.01 | 0.02 | 4.18 | 98.5 |
| | Standard Deviation | 2.6 | 0.83 | 0.84 | 0.36 | 0.46 | 0.45 | 0.40 | 0.03 | 0.01 | 0.01 | 0.01 | 0.01 | 0.29 | 0.63 |
| | Median | 56.2 | 18.00 | 7.94 | 2.37 | 1.61 | 0.71 | 4.15 | 0.89 | 0.11 | 0.10 | 0.01 | 0.02 | 4.16 | 98.2 |
| | Count | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| QUARTZ VEIN | | | | | | | | | | | | | | | |
| OVERALL STATISTICS (WASTE ROCK AND MARGINAL ORE) | | | | | | | | | | | | | | | |
| | Overall Minimum | 52.50 | 0.53 | 1.46 | 0.13 | 0.30 | 0.05 | 0.12 | 0.02 | 0.02 | 0.05 | 0.01 | 0.01 | 1.23 | 97.00 |
| | Overall Maximum | 92.00 | 20.10 | 9.40 | 3.32 | 6.68 | 3.14 | 5.06 | 1.06 | 0.16 | 0.21 | 0.04 | 0.03 | 7.29 | 100.00 |
| | Overall Average | 60.36 | 16.87 | 7.26 | 2.21 | 1.77 | 1.24 | 3.57 | 0.88 | 0.11 | 0.11 | 0.01 | 0.02 | 4.28 | 98.70 |
| | Overall Standard Deviation | 5.31 | 2.68 | 1.53 | 0.50 | 0.90 | 0.75 | 0.90 | 0.13 | 0.02 | 0.02 | 0.01 | 0.01 | 0.68 | 0.63 |
| | Overall Median | 58.9 | 17.75 | 7.65 | 2.33 | 1.63 | 0.99 | 3.81 | 0.91 | 0.11 | 0.11 | 0.01 | 0.01 | 4.36 | 98.8 |
| | Overall Count | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |
| TAILINGS | | | | | | | | | | | | | | | |
| | CNO 2 Treated Solids (Master Composite) | 56.9 | 19.70 | 7.70 | 2.60 | 1.16 | 0.57 | 4.80 | 0.54 | 0.11 | 0.08 | 0.03 | 0.02 | 4.47 | 98.7 |
| | TWT | 66.9 | 18.20 | 8.11 | 2.52 | 1.28 | 0.64 | 4.32 | 0.97 | 0.10 | 0.10 | 0.03 | 0.02 | 4.42 | 97.5 |
| | TWM | 66.9 | 18.50 | 8.22 | 2.64 | 1.46 | 0.58 | 4.43 | 0.94 | 0.11 | 0.11 | 0.02 | 0.02 | 4.21 | 98.1 |
| | TET | 57.8 | 18.90 | 8.20 | 2.57 | 1.33 | 0.66 | 4.21 | 0.92 | 0.11 | 0.10 | 0.03 | 0.02 | 4.30 | 98.6 |
| | TEB | 57.0 | 18.70 | 8.15 | 2.59 | 1.41 | 0.66 | 4.31 | 0.85 | 0.11 | 0.10 | 0.02 | 0.02 | 4.85 | 98.8 |
| | TWB CN Feed | 57.7 | 18.40 | 8.32 | 2.58 | 1.17 | 0.38 | 4.49 | 0.96 | 0.10 | 0.11 | 0.02 | 0.02 | 4.28 | 98.6 |
| | GN1 CNO 1-7 Solids (TWB) | 57.0 | 19.60 | 7.65 | 2.61 | 0.97 | 0.40 | 4.86 | 0.66 | 0.11 | 0.09 | 0.02 | 0.02 | 4.42 | 98.4 |
| | Minimum | 56.9 | 18.20 | 7.65 | 2.52 | 0.97 | 0.38 | 4.21 | 0.54 | 0.10 | 0.08 | 0.02 | 0.02 | 4.21 | 97.5 |
| | Maximum | 57.8 | 19.70 | 8.32 | 2.64 | 1.46 | 0.66 | 4.86 | 0.96 | 0.11 | 0.11 | 0.03 | 0.02 | 4.85 | 98.8 |
| | Count | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |

Note:
A value equal to the instrument detection limit was used in statistical calculations when a non-detect value was encountered.

Table 4 Summary of ICP Results

| Sample # | Ag | Al | As | Ba | Be | Bi | Cd | Co | Cr | Cu | Pb | K | Li | Mg | Min | Mo | Ni | Pb | Sb | Se | Sn | Sr | Ti | Ti | U | V | Y | Zn | Hg | | |
|--|-------|----------|---------|--------|-------|-------|-------|-------|-------|-------|-------|------|------|-------|--------|------|-------|-------|-------|-------|-------|-------|--------|-------|-------|--------|-------|-------|-------|------|-----|
| | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (%) | (%) | (ppb) | (ppb) | (%) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | (ppb) | | |
| ARGILLITE (8-9%) GREYWACHE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.13 | 65000 | 15 | 360 | 0.02 | 0.17 | 0.04 | 14 | 54 | 27 | 4.90 | 2.2 | 38 | 1.10 | 820 | 1.70 | 1.10 | 36 | 9.30 | 0.10 | 2.0 | 1.60 | 98 | 1000 | 0.40 | 1.40 | 81.0 | 6.30 | 26.0 | 0.1 | |
| Average | 0.18 | 100000 | 3800 | 750 | 2.60 | 0.72 | 0.31 | 19 | 85 | 59 | 6.10 | 2.30 | 43 | 1.80 | 1100 | 3.70 | 2.10 | 31 | 22.4 | 0.25 | 2.2 | 2.15 | 140 | 2000 | 2.70 | 1.40 | 140 | 140 | 140 | 1.0 | |
| Standard Deviation | 0.23 | 14662 | 5565 | 141 | 0.43 | 0.19 | 0.46 | 1.0 | 2 | 4 | 2.4 | 0.65 | 3 | 0.27 | 97 | 0.37 | 1.04 | 4 | 12.3 | 0.88 | 0.41 | 0.37 | 16 | 415 | 0.53 | 0.15 | 21.3 | 7.24 | 17.9 | 0.0 | |
| Median | 0.21 | 78500 | 101.5 | 530 | 1.90 | 0.36 | 1.25 | 0.09 | 16 | 61 | 6.0 | 5.75 | 3 | 1.16 | 980 | 2.25 | 1.85 | 3 | 18.3 | 0.15 | 2.0 | 2.06 | 178 | 1830 | 0.80 | 1.20 | 115 | 20 | 10 | 0 | |
| Count | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | |
| ARGILLITE (5-6%) GREYWACHE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.12 | 85000 | 25 | 480 | 1.50 | 0.10 | 0.18 | 0.03 | 13 | 45 | 27 | 3.90 | 2.7 | 27 | 120 | 410 | 0.05 | 1.10 | 2.0 | 1.70 | 35 | 1000 | 0.50 | 1.40 | 86.0 | 4.30 | 68.0 | 0.0 | 0.1 | | |
| Average | 0.16 | 110000 | 10000 | 870 | 3.10 | 0.80 | 0.44 | 22 | 72 | 72 | 7.30 | 4.5 | 49 | 2.10 | 1100 | 4.10 | 2.30 | 42 | 48.0 | 0.20 | 2.0 | 1.50 | 140 | 3000 | 2.20 | 2.00 | 190 | 140 | 140 | 1.0 | |
| Standard Deviation | 0.26 | 85000 | 6223 | 650 | 0.75 | 0.49 | 0.95 | 0.14 | 17 | 60 | 5.6 | 5.72 | 3.5 | 1.57 | 823 | 1.11 | 1.11 | 33 | 18.4 | 1.6 | 2.2 | 2.60 | 35 | 2058 | 0.75 | 1.63 | 116 | 7.45 | 11.1 | 0.1 | |
| Median | 0.21 | 85000 | 3034 | 87 | 2.19 | 0.43 | 0.08 | 3 | 6 | 23 | 3.80 | 3.1 | 5 | 0.23 | 811 | 0.68 | 0.76 | 3 | 10.0 | 0.45 | 1.7 | 1.60 | 65 | 1600 | 0.70 | 1.16 | 110 | 160 | 110 | 0.1 | |
| Count | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | |
| COMPOSITE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.11 | 85000 | 25 | 360 | 1.40 | 0.09 | 0.33 | 0.03 | 11 | 40 | 20 | 3.40 | 2.2 | 19 | 110 | 600 | 0.70 | 0.89 | 2.1 | 1.50 | 20 | 70 | 1000 | 0.50 | 1.40 | 80.0 | 6.70 | 64.0 | 0.1 | | |
| Average | 0.16 | 110000 | 10000 | 870 | 3.10 | 0.80 | 0.44 | 22 | 72 | 72 | 7.30 | 4.5 | 49 | 2.10 | 1100 | 4.10 | 2.30 | 42 | 48.0 | 0.20 | 2.0 | 1.50 | 140 | 3000 | 2.20 | 2.00 | 190 | 140 | 140 | 1.0 | |
| Standard Deviation | 0.26 | 85000 | 6223 | 650 | 0.75 | 0.49 | 0.95 | 0.14 | 17 | 60 | 5.6 | 5.72 | 3.5 | 1.57 | 823 | 1.11 | 1.11 | 33 | 18.4 | 1.6 | 2.2 | 2.60 | 35 | 2058 | 0.75 | 1.63 | 116 | 7.45 | 11.1 | 0.1 | |
| Median | 0.21 | 85000 | 3034 | 87 | 2.19 | 0.43 | 0.08 | 3 | 6 | 23 | 3.80 | 3.1 | 5 | 0.23 | 811 | 0.68 | 0.76 | 3 | 10.0 | 0.45 | 1.7 | 1.60 | 65 | 1600 | 0.70 | 1.16 | 110 | 160 | 110 | 0.1 | |
| Count | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | 28 | |
| GREYWACHE (20%-50% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.12 | 95000 | 32 | 270 | 1.10 | 0.13 | 0.61 | 0.03 | 9 | 41 | 18 | 2.80 | 1.5 | 12 | 650 | 700 | 1.10 | 0.65 | 1.5 | 1.5 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| Average | 0.16 | 110000 | 10000 | 870 | 3.10 | 0.80 | 0.44 | 22 | 72 | 72 | 7.30 | 4.5 | 49 | 2.10 | 1100 | 4.10 | 2.30 | 42 | 48.0 | 0.20 | 2.0 | 1.50 | 140 | 3000 | 2.20 | 2.00 | 190 | 140 | 140 | 1.0 | |
| Standard Deviation | 0.26 | 85000 | 6223 | 650 | 0.75 | 0.49 | 0.95 | 0.14 | 17 | 60 | 5.6 | 5.72 | 3.5 | 1.57 | 823 | 1.11 | 1.11 | 33 | 18.4 | 1.6 | 2.2 | 2.60 | 35 | 2058 | 0.75 | 1.63 | 116 | 7.45 | 11.1 | 0.1 | |
| Median | 0.21 | 85000 | 3034 | 87 | 2.19 | 0.43 | 0.08 | 3 | 6 | 23 | 3.80 | 3.1 | 5 | 0.23 | 811 | 0.68 | 0.76 | 3 | 10.0 | 0.45 | 1.7 | 1.60 | 65 | 1600 | 0.70 | 1.16 | 110 | 160 | 110 | 0.1 | |
| Count | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | |
| GREYWACHE (50%-90% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.13 | 95000 | 19 | 270 | 0.92 | 0.09 | 0.70 | 0.03 | 7 | 24 | 9.9 | 2.60 | 1.3 | 12 | 650 | 700 | 1.10 | 0.65 | 1.5 | 1.5 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| Average | 0.16 | 110000 | 10000 | 870 | 3.10 | 0.80 | 0.44 | 22 | 72 | 72 | 7.30 | 4.5 | 49 | 2.10 | 1100 | 4.10 | 2.30 | 42 | 48.0 | 0.20 | 2.0 | 1.50 | 140 | 3000 | 2.20 | 2.00 | 190 | 140 | 140 | 1.0 | |
| Standard Deviation | 0.26 | 85000 | 6223 | 650 | 0.75 | 0.49 | 0.95 | 0.14 | 17 | 60 | 5.6 | 5.72 | 3.5 | 1.57 | 823 | 1.11 | 1.11 | 33 | 18.4 | 1.6 | 2.2 | 2.60 | 35 | 2058 | 0.75 | 1.63 | 116 | 7.45 | 11.1 | 0.1 | |
| Median | 0.21 | 85000 | 3034 | 87 | 2.19 | 0.43 | 0.08 | 3 | 6 | 23 | 3.80 | 3.1 | 5 | 0.23 | 811 | 0.68 | 0.76 | 3 | 10.0 | 0.45 | 1.7 | 1.60 | 65 | 1600 | 0.70 | 1.16 | 110 | 160 | 110 | 0.1 | |
| Count | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
| MARGINAL ORE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.01 | 67000 | 8 | 430 | 1.60 | 0.35 | 0.43 | 0.03 | 9 | 50 | 18 | 3.90 | 2.6 | 19 | 930 | 930 | 0.31 | 0.18 | 22 | 6.10 | 0.10 | 2.0 | 1.80 | 46 | 1400 | 0.80 | 1.50 | 92.0 | 60.0 | 60.0 | 0.1 |
| Average | 0.02 | 67000 | 8 | 430 | 1.60 | 0.35 | 0.43 | 0.03 | 9 | 50 | 18 | 3.90 | 2.6 | 19 | 930 | 930 | 0.31 | 0.18 | 22 | 6.10 | 0.10 | 2.0 | 1.80 | 46 | 1400 | 0.80 | 1.50 | 92.0 | 60.0 | 60.0 | 0.1 |
| Standard Deviation | 0.15 | 6950 | 743 | 64 | 0.20 | 0.10 | 0.28 | 0.07 | 3 | 6 | 17 | 0.82 | 0.34 | 5 | 0.22 | 82 | 0.39 | 0.30 | 5 | 4.86 | 0.72 | 0.65 | 0.98 | 15 | 274 | 0.68 | 0.74 | 6.17 | 1.09 | 15.3 | 0.0 |
| Median | 0.18 | 64000 | 300 | 590 | 2.00 | 0.17 | 0.96 | 0.12 | 15 | 62 | 17 | 5.20 | 3.1 | 30 | 34 | 74 | 0.65 | 0.15 | 32 | 17.0 | 0.8 | 2.0 | 2.10 | 11 | 110 | 0.10 | 1.0 | 10 | 10 | 10 | 0.0 |
| Count | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | |
| SQUARES (10% MARGINAL ORE) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.21 | 13000 | 250 | 35 | 0.14 | 2.30 | 1.10 | 0.03 | 4 | 32 | 39 | 1.10 | 0.2 | 3 | 0.10 | 500 | 11000 | 2.80 | 15 | 70.0 | 0.10 | 2.0 | 0.20 | 15 | 94 | 0.60 | 0.18 | 2.60 | 2.20 | 11 | 0.1 |
| Average | 0.05 | 13000 | 8.00 | 33.00 | 0.14 | 0.05 | 0.16 | 0.03 | 3.60 | 24.00 | 9.80 | 1.10 | 0.20 | 3.00 | 410.00 | 0.05 | 0.05 | 14.00 | 4.30 | 0.10 | 2.0 | 0.20 | 15.00 | 94.00 | 0.70 | 0.15 | 2.60 | 2.20 | 11.00 | 0.10 | |
| Standard Deviation | 0.18 | 11114.50 | 2410.46 | 148.72 | 0.46 | 0.36 | 0.66 | 0.06 | 3.79 | 9.47 | 22.83 | 1.17 | 0.54 | 0.38 | 114.88 | 1.42 | 26.97 | 17.46 | 0.86 | 2.2 | 2.14 | 30.00 | 100.00 | 0.68 | 0.13 | 104.97 | 31.00 | 24.84 | 0.10 | | |
| Median | 0.23 | 65000 | 150.00 | 375.00 | 2.30 | 0.24 | 1.05 | 0.10 | 15 | 59 | 42 | 5.15 | 3.20 | 31 | 440 | 800 | 1.45 | 1.20 | 31 | 14.0 | 0.40 | 2.0 | 7.40 | 92 | 1650 | 0.70 | 1.60 | 110 | 7.80 | 100 | 0.1 |
| Count | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | 54 | |
| TALIBIGS | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Minimum | 0.35 | 70000 | 160 | 400 | 0.34 | 0.40 | 0.85 | 0.10 | 9 | 126 | 109 | 5.00 | 3.20 | 60 | 145 | 3500 | 5.20 | 0.25 | 44 | 10.0 | 3.10 | 1.0 | 3.20 | 63 | 2500 | 0.80 | 1.70 | 130 | 7.20 | 34.0 | 0.1 |
| Average | 0.37 | 66000 | 640 | 520 | 2.00 | 0.44 | 0.83 | 1.00 | 18 | 110 | 44 | 5.40 | 3.40 | 32 | 1450 | 600 | 6.30 | 0.30 | 63 | 25.0 | 0.80 | 1.0 | 2.60 | 75 | 1400 | 0.70 | 1.50 | 65.0 | 62.0 | 120 | 0.1 |
| Standard Deviation | 0.36 | 91000 | 1300 | 580 | 2.20 | 0.38 | 0.78 | 1.80 | 19 | 83 | 46 | 5.40 | 3.40 | 33 | 150 | 680 | 6.30 | 0.30 | 63 | 24.0 | 1.80 | 1.0 | 2.70 | 75 | 1000 | 0.60 | 1.40 | 88.0 | 82.0 | 110 | 0.1 |
| Median | 0.43 | 95000 | 1000 | 600 | 2.20 | 0.39 | 0.85 | 1.60 | 16 | 120 | 43 | 5.20 | 3.40 | 36 | 140 | 660 | 6.30 | 0.30 | 60 | 18.0 | 1.40 | 1.0 | 2.40 | 85 | 1300 | 0.60 | 1.50 | 54.0 | 54.0 | 110 | 0.1 |
| Count | 0.80 | 80000 | 3000 | 100 | 0.75 | 0.3 | 0.65 | 0.10 | 7 | 30 | 32 | 4.80 | 1.50 | 32 | 140 | 500 | 5.00 | 0.35 | 44 | 14.0 | 0.80 | 1.0 | | | | | | | | | |

Table 5
Summary of Acid-Base Accounting Results

| Sample # | Statistics | NP CaCO ₃ /1000 | AP CaCO ₃ /1000 | Net NP CaCO ₃ /1000 | NP:AP ratio | S % | Acid Leachable SO ₄ S % | Sulphide-S % | C % | Carbonate % | TIC % | Carb-NP CaCO ₃ /1000 | Carb-NP/ATP ratio |
|---|---|-------------------------------|-------------------------------|-----------------------------------|----------------|--------|---------------------------------------|-----------------|--------|----------------|----------|------------------------------------|----------------------|
| ARGILLITE (4-8%) GREYWACKE | | | | | | | | | | | | | |
| Minimum | | 212 | 0.9 | 18.0 | 3.50 | 0.05 | 0.01 | 0.03 | 0.41 | 1.31 | 0.26 | 21.6 | 4.1 |
| Maximum | | 115 | 12 | 112 | 49.6 | 0.66 | 0.28 | 0.36 | 6.11 | 2.92 | 0.58 | 102 | 40 |
| Average | | 45.1 | 4.7 | 40.4 | 10.7 | 0.23 | 0.09 | 0.15 | 1.39 | 2.10 | 0.42 | 44.6 | 9.6 |
| Standard Deviation | | 30.0 | 3.7 | 26.3 | 17.2 | 0.21 | 0.11 | 0.12 | 2.08 | 0.53 | 0.11 | 26.6 | 14 |
| Median | | 41.9 | 3.5 | 38.2 | 9.90 | 0.13 | 0.03 | 0.10 | 0.91 | 2.65 | 0.41 | 39.0 | 8.7 |
| Count | | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| ARGILLITE (4-8%) GREYWACKE | | | | | | | | | | | | | |
| Minimum | | 71.0 | 0.9 | 13.3 | 0.40 | 0.03 | 0.00 | 0.03 | 0.10 | 0.30 | 0.08 | 5.0 | 0.2 |
| Maximum | | 73.4 | 2.6 | 68.8 | 24.6 | 1.62 | 0.78 | 0.84 | 2.43 | 3.75 | 0.75 | 62.5 | 26 |
| Average | | 30.1 | 6.8 | 23.3 | 4.4 | 0.37 | 0.16 | 0.22 | 0.54 | 1.58 | 0.32 | 26.6 | 3.9 |
| Standard Deviation | | 11.7 | 6.1 | 5.6 | 6.36 | 0.38 | 0.20 | 0.20 | 0.46 | 0.68 | 0.14 | 11.2 | 5.3 |
| Median | | 30.1 | 4.7 | 24.7 | 5.30 | 0.25 | 0.07 | 0.15 | 0.42 | 1.51 | 0.30 | 25.4 | 4.6 |
| Count | | 43 | 43 | 43 | 43 | 43 | 43 | 43 | 43 | 39 | 39 | 43 | 43 |
| COMPOSITE | | | | | | | | | | | | | |
| Minimum | | 8.60 | 1.2 | 3 | 2.40 | 0.06 | 0.01 | 0.04 | 0.13 | 0.45 | 0.09 | 7.5 | 1.8 |
| Maximum | | 15 | 11 | 4 | 6.57 | 0.05 | 0.21 | 0.37 | 1.44 | 6.64 | 1.33 | 111 | 58 |
| Average | | 39.9 | 4.4 | 35.5 | 9.08 | 0.19 | 0.06 | 0.14 | 0.51 | 2.01 | 0.40 | 33.6 | 7.6 |
| Standard Deviation | | 26.8 | 2.6 | 24.2 | 14.8 | 0.11 | 0.06 | 0.08 | 0.33 | 1.53 | 0.31 | 25.5 | 14 |
| Median | | 30.6 | 4.1 | 27.8 | 7.0 | 0.17 | 0.03 | 0.13 | 0.41 | 1.49 | 0.30 | 24.9 | 6.6 |
| Count | | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| GREYWACKE (20%-50% ARGILLITE INTERBEDS) | | | | | | | | | | | | | |
| Minimum | | 28.2 | 0.5 | 17.4 | 2.10 | 0.07 | 0.01 | 0.02 | 0.44 | 1.69 | 0.34 | 16.4 | 2.7 |
| Maximum | | 15 | 15 | 65.0 | 61.4 | 0.58 | 0.14 | 0.49 | 0.99 | 3.69 | 0.73 | 50.4 | 5.7 |
| Average | | 43.1 | 4.8 | 38.3 | 8.99 | 0.20 | 0.05 | 0.13 | 0.63 | 2.32 | 0.45 | 31.0 | 7.0 |
| Standard Deviation | | 41.8 | 4.0 | 36.8 | 21.9 | 0.16 | 0.04 | 0.09 | 0.59 | 2.04 | 0.42 | 34.5 | 15 |
| Median | | 41.8 | 3.3 | 36.2 | 13 | 0.16 | 0.04 | 0.09 | 0.59 | 2.04 | 0.42 | 34.5 | 15 |
| Count | | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 12 | 12 | 13 | 13 |
| GREYWACKE (50% ARGILLITE INTERBEDS) | | | | | | | | | | | | | |
| Minimum | | 21.8 | 0.9 | 16.4 | 5.00 | 0.04 | 0.00 | 0.03 | 0.31 | 1.05 | 0.21 | 17.5 | 4.1 |
| Maximum | | 133 | 19 | 114 | 67.4 | 0.62 | 0.24 | 0.61 | 2.33 | 3.77 | 0.75 | 122 | 63 |
| Average | | 51.0 | 3.7 | 47.2 | 13.7 | 0.16 | 0.04 | 0.12 | 1.35 | 2.22 | 0.44 | 41.3 | 11 |
| Standard Deviation | | 27.0 | 4.7 | 22.3 | 19.3 | 0.17 | 0.06 | 0.15 | 1.79 | 0.93 | 0.19 | 25.9 | 17 |
| Median | | 44.8 | 2.4 | 41.1 | 22.6 | 0.08 | 0.02 | 0.07 | 0.69 | 1.86 | 0.39 | 34.5 | 17 |
| Count | | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 15 | 10 | 10 | 15 | 15 |
| MARGINAL ORE | | | | | | | | | | | | | |
| Minimum | | 18.3 | 2.5 | 13.3 | 2.40 | 0.12 | 0.04 | 0.08 | 0.21 | 0.73 | 0.15 | 12.2 | 1.7 |
| Maximum | | 39.4 | 13 | 28.8 | 12.3 | 0.57 | 0.36 | 0.42 | 0.59 | 2.30 | 0.46 | 38.4 | 11 |
| Average | | 28.0 | 6.1 | 21.8 | 4.56 | 0.39 | 0.19 | 0.20 | 0.30 | 1.51 | 0.30 | 25.2 | 4.1 |
| Standard Deviation | | 8.42 | 3.4 | 5.2 | 2.76 | 0.17 | 0.12 | 0.11 | 0.11 | 0.45 | 0.09 | 7.5 | 3.0 |
| Median | | 28.6 | 5.0 | 21.8 | 6.30 | 0.48 | 0.20 | 0.18 | 0.37 | 1.58 | 0.32 | 26.4 | 4.9 |
| Count | | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 11 |
| QUARTZ VEIN | | | | | | | | | | | | | |
| DA-037 | Reserve Quartz Vein (5-50% of Interval) | 27.5 | 10 | 17.5 | 2.80 | 0.42 | 0.10 | 0.32 | 0.33 | 1.11 | 0.22 | 18.5 | 1.8 |
| OVERALL STATISTICS (WASTE ROCK AND MARGINAL ORE) | | | | | | | | | | | | | |
| Minimum | | 7.10 | 0.60 | 13.30 | 0.40 | 0.03 | 0.00 | 0.02 | 0.10 | 0.30 | 0.06 | 5.00 | 0.2 |
| Maximum | | 133.12 | 28.20 | 118.00 | 67.40 | 1.62 | 0.78 | 0.84 | 2.33 | 6.64 | 1.33 | 122.51 | 62.64 |
| Average | | 37.2 | 5.6 | 31.6 | 12.3 | 0.3 | 0.1 | 0.2 | 0.7 | 1.8 | 0.4 | 32.0 | 10.5 |
| Standard Deviation | | 19.9 | 4.9 | 20.4 | 13.2 | 0.3 | 0.2 | 0.2 | 1.0 | 0.9 | 0.2 | 18.3 | 11.6 |
| Median | | 32.0 | 3.8 | 26.3 | 6.91 | 0.19 | 0.05 | 0.12 | 0.48 | 1.62 | 0.34 | 27.4 | 8.4 |
| Count | | 105 | 105 | 105 | 105 | 105 | 105 | 105 | 105 | 94 | 94 | 105 | 105 |
| TAILINGS (1) | | | | | | | | | | | | | |
| DA 0067 | CND-2 Treated Solids (Mixer Composite) | 21.5 | 3.4 | 18.1 | 6.25 | 0.17 | 0.40 | 0.11 | 0.38 | 1.22 | - | 20.3 | 5.9 |
| TWT | | 29.2 | 4 | 17.8 | 2.52 | 0.46 | 0.37 | 0.11 | 0.59 | 1.90 | - | 23.0 | 7.4 |
| TWM | | 32.4 | 2 | 30.2 | 3.07 | 0.40 | 0.14 | 0.06 | 0.42 | 1.36 | - | 27.0 | 11.4 |
| DET | | 28.1 | 2.2 | 20.3 | 3.71 | 0.33 | 0.25 | 0.09 | 0.46 | 1.49 | - | 21.9 | 6.5 |
| TEB | CN1 Feed | 29.6 | 2.7 | 27.9 | 3.74 | 0.33 | 0.25 | 0.09 | 0.40 | 1.49 | - | 24.9 | 9.4 |
| CN1 CND-1 Solids (TAR) | | 20.6 | 0.9 | 14.3 | 3.30 | 0.23 | 0.20 | 0.03 | 0.32 | 0.73 | - | 12.1 | 13.4 |
| Minimum | | 32.4 | 3.7 | 21.8 | 6.25 | 0.81 | 0.49 | 0.12 | 0.59 | 1.58 | - | 26.4 | 13.4 |
| Maximum | | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 0 | 7 | 7 |
| Count | | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 0 | 7 | 7 |
| ORE | | | | | | | | | | | | | |
| DA 0067 | | 46.1 | 17 | 28.8 | 2.66 | 0.55 | 0.01 | 0.55 | 1.21 | - | - | 20.2 | 1.2 |
| DA 0351 | | 50.7 | 17 | 33.9 | 3.01 | 0.54 | 0.01 | 0.54 | 1.39 | - | - | 23.2 | 1.4 |
| DA 0368 | | 13.9 | 12 | 2.07 | 1.18 | 0.36 | 0.02 | 0.36 | 1.03 | - | - | 17.2 | 3.8 |
| DA 0402 | | 62.7 | 14 | 36.6 | 3.09 | 0.48 | 0.01 | 0.48 | 1.49 | - | - | 28.9 | 1.9 |
| DA 0521 | | 45.3 | 17 | 28.0 | 2.63 | 0.55 | 0.01 | 0.54 | 1.57 | - | - | 26.2 | 1.9 |
| DA 0528 | | 83.5 | 17 | 66.3 | 4.86 | 0.61 | 0.01 | 0.61 | 3.27 | - | - | 54.5 | 3.2 |
| DA 0638 | | 65.4 | 4.3 | 61.1 | 15.4 | 0.14 | 0.01 | 0.13 | 2.33 | - | - | 36.8 | 9.1 |
| DA 8157 | | 30.5 | 7.2 | 23.3 | 3.23 | 0.23 | 0.01 | 0.23 | 0.81 | - | - | 13.4 | 1.8 |
| Minimum | | 13.9 | 4.3 | 2.07 | 1.18 | 0.14 | 0.01 | 0.13 | 0.81 | - | - | 13.4 | 1.8 |
| Maximum | | 83.5 | 31 | 66.3 | 15.4 | 0.85 | 0.02 | 0.85 | 3.27 | - | - | 54.5 | 9.1 |
| Count | | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 0 | 0 | 9 | 9 |

Note:
A table used to the instrument detection limit was used in statistical calculations when a non-detect value was encountered.
1) The percent sulphide concentrations for TWT, TWM, TET, TEB, TMB, CNFEED, and CN1 CND-1 Solids were calculated based on the difference between total sulphur and acid leachable sulphur.

Summary of CND 2 Treated Solids (Master Composite) Tailings Supernatant Water Aging Results

| Parameter | Units | MMER Guidelines (mg/L) | CCME | Day 0 | Day 3 | Day 7 | Day 14 | Day 45 |
|----------------------------------|---------------------------|------------------------|----------|------------|------------|---------------|---------------|-----------|
| General Parameters | | | | | | | | |
| Temperature Upon Receipt | °C | - | - | 21 | 20.5 | 18.5 | 18 | 20.5 |
| Total Suspended Solids | mg/L | 15.00 | - | 116 | 136 | 29 UAL | 32 UAL | 42 |
| Conductivity | uS/cm | - | - | 2200 | 2520 | 2440 | 2480 | 2620 |
| pH | units | - | 6.5-9 | 7.97 | 7.76 | 7.79 | 7.92 | 8.03 |
| Alkalinity | mg/L as CaCO ₃ | - | - | 65 | 56 | 63 | 73 | 118 |
| Cl | mg/L | - | - | 13 | 13 | 13 | 13 | 14 |
| SO ₄ | mg/L | - | - | 970 | 1100 | 1100 | 1200 | 1100 |
| Nutrients | | | | | | | | |
| NO ₂ | as N mg/L | - | 0.06 | < 0.06 | < 0.06 | < 0.06 | < 0.06 | < 0.6 |
| NO ₃ | as N mg/L | - | - | 0.05 | 0.06 | 0.06 | < 0.05 | < 0.5 |
| NH ₃ +NH ₄ | as N mg/L | - | - | 29.3 | 45.8 | 3.1 | 26.5 | 37.3 |
| Total Metals | | | | | | | | |
| Hg | mg/L | - | 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | 0.0001 | 0.0002 |
| Ag | mg/L | - | 0.0001 | 0.00032 | < 0.00003 | < 0.00003 | < 0.00003 | 0.00005 |
| Al | mg/L | - | 0.1 | 2.14 | 1.68 | 0.496 | 0.63 | 0.758 |
| As | mg/L | 0.50 | 0.005 | 0.469 | 0.448 | 0.353 | 0.242 | 0.219 |
| B | mg/L | - | - | 0.026 | 0.029 | 0.051 | 0.035 | < 0.05 |
| Ba | mg/L | - | - | 0.0268 | 0.0409 | 0.0339 | 0.0362 | 0.0376 |
| Be | mg/L | - | - | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 |
| Bi | mg/L | - | - | 0.00006 | < 0.00002 | < 0.00002 | < 0.00002 | 0.00003 |
| Ca | mg/L | - | - | 136 | 183 | 185 | 187 | 159 |
| Cd | mg/L | - | 0.000017 | < 0.00006 | < 0.00006 | < 0.00006 | 0.00006 | < 0.00006 |
| Co | mg/L | - | - | 0.2 | 0.216 | 0.25 | 0.22 | 0.186 |
| Cr | mg/L | - | 0.001 | 0.0059 | 0.0062 | 0.0055 | 0.0026 | 0.0021 |
| Cu | mg/L | 0.30 | 0.004 | 0.0474 | 0.0522 | 0.0397 | 0.0253 | 0.0249 |
| Fe | mg/L | - | 0.3 | 3.66 | 3.52 | 0.84 | 1.24 | 1.66 |
| K | mg/L | - | - | 22.5 | 22.3 | 21.3 | 21.3 | 27.1 |
| Li | mg/L | - | - | 0.0057 | 0.0062 | 0.0137 | 0.0062 | 0.0089 |
| Mg | mg/L | - | - | 5.05 | 6.22 | 6.92 | 7.68 | 13.4 |
| Mn | mg/L | - | - | 0.0773 | 0.0924 | 0.104 | 0.109 | 0.0739 |
| Mo | mg/L | - | 0.073 | 0.0231 | 0.024 | 0.0301 | 0.0262 | 0.0292 |
| Na | mg/L | - | - | 337 | 402 | 405 | 401 | 412 |
| Ni | mg/L | 0.50 | 0.025 | 0.0079 | 0.0087 | 0.0047 | 0.0047 | 0.0045 |
| Pb | mg/L | 0.20 | 0.001 | 0.00165 | 0.00184 | 0.00185 | 0.00104 | 0.00088 |
| Sb | mg/L | - | - | 0.016 | 0.0162 | 0.013 | 0.0133 | 0.0104 |
| Se | mg/L | - | 0.001 | 0.004 | < 0.003 | < 0.003 | < 0.003 | < 0.003 |
| Sn | mg/L | - | - | < 0.0003 | 0.0017 | 0.002 | < 0.002 | 0.0041 |
| Sr | mg/L | - | - | 0.279 | 0.343 | 0.366 | 0.373 | 0.41 |
| Ti | mg/L | - | - | 0.0088 | 0.0085 | 0.0027 | 0.0041 | 0.0044 |
| Tl | mg/L | - | 0.0008 | < 0.01 | < 0.01 | < 0.01 | < 0.01 | < 0.01 |
| U | mg/L | - | - | 0.00486 | 0.00479 | 0.0053 | 0.00496 | 0.00605 |
| V | mg/L | - | - | 0.00258 | 0.00212 | 0.00142 | 0.00061 | 0.0012 |
| W | mg/L | - | - | 0.0346 | 0.031 | 0.0337 | 0.0335 | 0.0286 |
| Y | mg/L | - | - | 0.000547 | 0.000428 | 0.00014 | 0.000203 | 0.000186 |
| Zn | mg/L | 0.50 | 0.03 | 0.0077 | 0.0156 | 0.0146 | 0.0092 | 0.0053 |

Summary of CND 2 Treated Solids (Master Composite) Tailings Supernatant Water Aging Results

| Parameter | Units | MMER Guidelines (mg/L) | CCME | Day 0 | Day 3 | Day 7 | Day 14 | Day 45 |
|-------------------------|---------------------------------------|------------------------|----------|--------------|-----------|-----------|-----------|-----------|
| Dissolved Metals | | | | | | | | |
| Hg | mg/L | - | 0.0001 | < 0.0001 | < 0.0001 | 0.0003 | < 0.0001 | 0.0001 |
| Ag | mg/L | - | 0.0001 | 0.00015 | 0.00015 | < 0.00003 | < 0.00003 | < 0.00003 |
| Al | mg/L | - | 0.1 | 0.158 | 0.0788 | 0.0847 | 0.0725 | 0.0982 |
| As | mg/L | 0.50 | 0.005 | 0.532 | 0.366 | 0.335 | 0.307 | 0.227 |
| B | mg/L | - | - | 0.03 | 0.032 | 0.027 | 0.027 | < 0.05 |
| Ba | mg/L | - | - | 0.0259 | 0.036 | 0.0332 | 0.0347 | 0.0359 |
| Be | mg/L | - | - | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 |
| Bi | mg/L | - | - | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 |
| Ca | mg/L | - | - | 135 | 163 | 144 | 196 | 144 |
| Cd | mg/L | - | 0.000017 | < 0.00006 | < 0.00006 | < 0.00006 | < 0.00006 | < 0.00006 |
| Co | mg/L | - | - | 0.183 | 0.186 | 0.218 | 0.205 | 0.182 |
| Cr | mg/L | - | 0.001 | 0.0031 | 0.0032 | 0.003 | 0.0025 | 0.0012 |
| Cu | mg/L | 0.30 | 0.004 | 0.0337 | 0.0335 | 0.0293 | 0.0252 | 0.0194 |
| Fe | mg/L | - | 0.3 | 0.08 | 0.11 | 0.08 | 0.07 | 0.11 |
| K | mg/L | - | - | 17.7 | 22 | 18.6 | 21.6 | 23.7 |
| Li | mg/L | - | - | 0.0038 | 0.0058 | 0.0054 | 0.0051 | 0.0049 |
| Mg | mg/L | - | - | 4.16 | 5.25 | 5.93 | 7.76 | 11.6 |
| Mn | mg/L | - | - | 0.0238 | 0.046 | 0.0615 | 0.105 | 0.0567 |
| Mo | mg/L | - | 0.073 | 0.0222 | 0.0237 | 0.0224 | 0.0234 | 0.0277 |
| Na | mg/L | - | - | 378 | 368 | 376 | 401 | 377 |
| Ni | mg/L | 0.50 | 0.025 | 0.0063 | 0.0038 | 0.0037 | 0.0048 | 0.0035 |
| Pb | mg/L | 0.20 | 0.001 | 0.00003 | 0.00015 | 0.00025 | 0.00011 | 0.00022 |
| Sb | mg/L | - | - | 0.0178 | 0.0163 | 0.014 | 0.014 | 0.0103 |
| Se | mg/L | - | 0.001 | 0.004 | 0.003 | 0.003 | < 0.003 | < 0.003 |
| Sn | mg/L | - | - | < 0.0003 | 0.0017 | 0.0068 | < 0.002 | 0.0037 |
| Sr | mg/L | - | - | 0.301 | 0.319 | 0.331 | 0.372 | 0.379 |
| Ti | mg/L | - | - | 0.0008 | < 0.0002 | 0.0007 | 0.0005 | 0.0099 |
| Tl | mg/L | - | 0.0008 | < 0.01 | < 0.01 | < 0.01 | < 0.01 | < 0.01 |
| U | mg/L | - | - | 0.00437 | 0.0045 | 0.00481 | 0.00487 | 0.00549 |
| V | mg/L | - | - | 0.00114 | 0.00084 | 0.00065 | 0.00072 | 0.0007 |
| W | mg/L | - | - | 0.0303 | 0.0306 | 0.0322 | 0.0264 | 0.0253 |
| Y | mg/L | - | - | 0.00001 | 0.000018 | 0.000013 | 0.000033 | 0.000028 |
| Zn | mg/L | 0.50 | 0.03 | 0.0041 | 0.0052 | 0.0062 | 0.0079 | 0.0023 |
| Other Parameters | | | | | | | | |
| Thiosalts | as S ₂ O ₃ mg/L | - | - | < 10 | < 10 | < 10 | < 20 | < 10 |
| CN(T) | mg/L | 1.00 | - | 0.32 | 0.32 | 0.2 | 0.18 | 0.17 |
| CN(F) | mg/L | - | 0.005 | < 0.03 | < 0.05 | < 0.04 | < 0.04 | < 0.04 |
| CN(WAD) | mg/L | - | - | 0.03 | 0.04 | 0.03 | 0.04 | 0.04 |

Notes:

- 1.0** Indicates a value that is elevated relative to the CCME guideline.
 - 1.0** Indicates a value that is elevated relative to the MMER and CCME (if present) guideline values.
- CCME and MMER values provided only as basis of comparison, values above guidelines require further evaluation.

Table 9
Summary of CN1 CND 1-7 Solids (TWB) Tailings Supernatant Water Aging Results

| Parameter | Units | MMER Guidelines (mg/L) | CCME | Day 0 | Day 1 | Day 3 | Day 7 | Day 15 | Day 30 | Day 44 |
|----------------------------------|---------------------------|------------------------|----------|-------------|--------------|-------------|--------------|-----------|-----------|-----------|
| General Parameters | | | | | | | | | | |
| Temperature Upon Receipt | °C | - | - | 17.5 | - | 4.5 | 5 | 19 | 20 | 21 |
| Total Suspended Solids | mg/L | 15.00 | - | 241 | 5 | < 3 | 4 | 6 | 4 | < 2 |
| Conductivity | uS/cm | - | - | 2570 | 2660 | 2620 | 2540 | 2590 | 2610 | 2460 |
| pH | units | - | 6.5-9 | 7.9 | 8.12 | 8.04 | 8.07 | 8.02 | 8.36 | 8.06 |
| Alkalinity | mg/L as CaCO ₃ | - | - | 86 | 94 | 97 | 97 | 105 | 267 | 115 |
| Cl | mg/L | - | - | 20 | 120 | 20 | 21 | 21 | 20 | 20 |
| SO ₄ | mg/L | - | - | 1000 | 1000 | 920 | 900 | 1000 | 980 | 940 |
| Nutrients | | | | | | | | | | |
| NO ₂ | as N mg/L | - | 0.06 | < 0.6 | < 0.6 | < 0.6 | < 0.6 | < 0.6 | < 0.60 | < 0.06 |
| NO ₃ | as N mg/L | - | - | < 0.5 | 0.5 | < 0.5 | < 0.5 | 0.3 | 0.34 | 1.03 |
| NH ₃ +NH ₄ | as N mg/L | - | - | 64.1 | 3.9 | 4.2 | 5 | 5.5 | 8.4 | 10.8 |
| Total Metals | | | | | | | | | | |
| Hg | mg/L | - | 0.0001 | 0.0009 | 0.001 | 0.0011 | 0.0015 | 0.0006 | 0.0004 | 0.0002 |
| Ag | mg/L | - | 0.0001 | 0.00034 | 0.00521 | 0.00052 | 0.00069 | 0.00019 | 0.00006 | < 0.002 |
| Al | mg/L | - | 0.1 | 4.85 | 0.214 | 0.0884 | 0.0998 | 0.115 | 0.12 | 0.0569 |
| As | mg/L | 0.50 | 0.005 | 0.381 | 0.872 | 0.337 | 0.325 | 0.317 | 0.26 | 0.283 |
| B | mg/L | - | - | 0.057 | 0.065 | 0.047 | 0.046 | 0.046 | 0.046 | 0.048 |
| Ba | mg/L | - | - | 0.0381 | 0.0395 | 0.0394 | 0.0393 | 0.0379 | 0.0388 | 0.0332 |
| Be | mg/L | - | - | 6E-05 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 |
| Bi | mg/L | - | - | 0.00007 | < 0.00002 | 0.00002 | < 0.00002 | 0.00013 | < 0.00002 | 0.00003 |
| Ca | mg/L | - | - | 166 | 160 | 160 | 160 | 156 | 157 | 138 |
| Cd | mg/L | - | 0.000017 | < 0.00001 | 0.0001 | 0.0001 | 0.0001 | 0.00023 | < 0.00001 | < 0.00001 |
| Co | mg/L | - | - | 0.226 | 0.227 | 0.196 | 0.202 | 0.22 | 0.202 | 0.212 |
| Cr | mg/L | - | 0.001 | 0.0081 | 0.002 | < 0.004 | 0.0012 | 0.0018 | 0.0008 | < 0.002 |
| Cu | mg/L | 0.30 | 0.004 | 1.42 | 1.37 | 1.22 | 0.896 | 0.215 | 0.0872 | 0.0555 |
| Fe | mg/L | - | 0.3 | 10.1 | 0.3 | 0.08 | 0.13 | 0.2 | 22.7 | 0.02 |
| K | mg/L | - | - | 31.5 | 32.5 | 32.4 | 25.5 | 21.7 | 28.7 | 28.4 |
| Li | mg/L | - | - | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 |
| Mg | mg/L | - | - | 10.90 | 7.89 | 7.95 | 8.18 | 8.60 | 9.73 | 9.45 |
| Mn | mg/L | - | - | 0.1810 | 0.0940 | 0.0892 | 0.0955 | 0.1130 | 0.0965 | 0.0708 |
| Mo | mg/L | - | 0.073 | 0.0589 | 0.0541 | 0.0573 | 0.0548 | 0.0528 | 0.0563 | 0.34 |
| Na | mg/L | - | - | 400 | 561 | 552 | 399 | 500 | 393 | 375 |
| Ni | mg/L | 0.50 | 0.025 | 0.0187 | 0.1390 | 0.0111 | 0.0116 | 0.0067 | 0.0034 | 0.0487 |
| Pb | mg/L | 0.20 | 0.001 | 0.00321 | 0.00242 | 0.00295 | 0.00137 | 0.00139 | 0.00074 | < 0.00007 |
| P | mg/L | - | - | 0.1 | 0.2 | 0.02 | 0.01 | < 0.01 | 0.01 | < 0.01 |
| Sb | mg/L | - | - | 0.0278 | 0.026 | 0.0287 | 0.0313 | 0.0253 | 0.0245 | 0.0368 |
| Se | mg/L | - | 0.001 | 0.005 | 0.005 | 0.003 | 0.004 | 0.003 | 0.007 | 0.004 |
| Sn | mg/L | - | - | 0.0021 | 0.0022 | 0.0015 | 0.0036 | 0.0033 | 0.0021 | 0.0026 |
| Sr | mg/L | - | - | 0.516 | 0.565 | 0.548 | 0.573 | 0.533 | 0.526 | 0.456 |
| Ti | mg/L | - | - | 0.0305 | 0.0017 | 0.0009 | 0.0011 | 0.0008 | 0.0021 | 0.0004 |
| Tl | mg/L | - | 0.0008 | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | 0.0002 | 0.0001 | < 0.0001 |
| U | mg/L | - | - | 0.00632 | 0.00669 | 0.00698 | 0.00659 | 0.00736 | 0.00726 | 0.0111 |
| V | mg/L | - | - | 0.00426 | 0.00095 | 0.00072 | 0.00071 | 0.001 | 0.00077 | < 0.001 |
| W | mg/L | - | - | 0.00208 | 0.00292 | 0.00217 | 0.00253 | 0.00246 | 0.00200 | 0.00456 |
| Y | mg/L | - | - | 0.000977 | 0.000067 | 0.000037 | 0.000035 | 0.000185 | 0.000035 | 0.000022 |
| Zn | mg/L | 0.50 | 0.03 | 0.0272 | 0.0054 | 0.0101 | 0.011 | 0.0091 | 0.0038 | 0.0057 |

Table 9
Summary of CN1 CND 1-7 Solids (TWB) Tailings Supernatant Water Aging Results

| Parameter | Units | MMER Guidelines (mg/L) | CCME | Day 0 | Day 1 | Day 3 | Day 7 | Day 15 | Day 30 | Day 44 |
|-------------------------|---------------------------------------|------------------------|----------|------------|-------------|-------------|--------------|-----------|-----------|-----------|
| Dissolved Metals | | | | | | | | | | |
| Hg | mg/L | - | 0.0001 | 0.0008 | 0.0009 | 0.0011 | 0.0014 | 0.0001 | < 0.0001 | < 0.0001 |
| Ag | mg/L | - | 0.0001 | < 0.00003 | 0.00031 | 0.00064 | 0.00018 | 0.00005 | < 0.00003 | < 0.0002 |
| Al | mg/L | - | 0.1 | 0.05 | 0.0485 | 0.0516 | 0.0368 | 0.0344 | 0.0407 | 0.0468 |
| As | mg/L | 0.50 | 0.005 | 0.334 | 0.343 | 0.318 | 0.32 | 0.293 | 0.269 | 0.283 |
| B | mg/L | - | - | 0.044 | 0.043 | 0.045 | 0.046 | 0.046 | 0.042 | 0.051 |
| Ba | mg/L | - | - | 0.037 | 0.0376 | 0.0373 | 0.0386 | 0.0356 | 0.0374 | 0.0328 |
| Be | mg/L | - | - | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 | < 0.00004 |
| Bi | mg/L | - | - | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 | < 0.00002 |
| Ca | mg/L | - | - | 159 | 160 | 153 | 151 | 156 | 152 | 136 |
| Cd | mg/L | - | 0.000017 | 0.00004 | 0.00005 | < 0.00001 | < 0.00001 | 0.00007 | 0.00004 | < 0.00001 |
| Co | mg/L | - | - | 0.206 | 0.215 | 0.205 | 0.204 | 0.194 | 0.204 | 0.204 |
| Cr | mg/L | - | 0.001 | 0.001 | 0.001 | < 0.004 | 0.0015 | 0.0015 | 0.0012 | < 0.002 |
| Cu | mg/L | 0.30 | 0.004 | 1.2 | 1.23 | 1.23 | 0.839 | 0.191 | 0.0741 | 0.0512 |
| Fe | mg/L | - | 0.3 | 0.06 | < 0.01 | 0.02 | < 0.01 | < 0.01 | < 0.05 | 0.02 |
| K | mg/L | - | - | 28.3 | 22.5 | 24.6 | 24.0 | 21.4 | 24.1 | 27.8 |
| Li | mg/L | - | - | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 | < 0.002 |
| Mg | mg/L | - | - | 7.90 | 7.86 | 7.51 | 7.77 | 8.18 | 9.07 | 9.75 |
| Mn | mg/L | - | - | 0.0826 | 0.0850 | 0.0799 | 0.0922 | 0.0965 | 0.0926 | 0.0770 |
| Mo | mg/L | - | 0.073 | 0.0498 | 0.0514 | 0.0554 | 0.0512 | 0.048 | 0.0526 | 0.0457 |
| Na | mg/L | - | - | 389 | 398 | 383 | 375 | 378 | 384 | 387 |
| Ni | mg/L | 0.50 | 0.025 | 0.0121 | 0.0123 | 0.0114 | 0.0158 | 0.0050 | 0.0053 | 0.0027 |
| Pb | mg/L | 0.20 | 0.001 | < 0.00002 | 0.00087 | 0.00263 | 0.00098 | 0.00058 | 0.00026 | < 0.00007 |
| P | mg/L | - | - | 0.03 | 0.02 | 0.02 | 0.02 | 0.01 | < 0.01 | 0.02 |
| Sb | mg/L | - | - | 0.0271 | 0.0269 | 0.0288 | 0.0323 | 0.0240 | 0.0300 | 0.0369 |
| Se | mg/L | - | 0.001 | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.002 | 0.002 |
| Sn | mg/L | - | - | 0.0015 | 0.0022 | 0.0016 | 0.0024 | 0.002 | 0.002 | 0.0013 |
| Sr | mg/L | - | - | 0.479 | 0.510 | 0.495 | 0.536 | 0.517 | 0.530 | 0.467 |
| Ti | mg/L | - | - | 0.0005 | 0.0004 | 0.0006 | 0.0005 | 0.0003 | 0.0002 | 0.0003 |
| Tl | mg/L | - | 0.0008 | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 | < 0.0001 |
| U | mg/L | - | - | 0.00583 | 0.00575 | 0.00607 | 0.00587 | 0.00603 | 0.0073 | 0.00462 |
| V | mg/L | - | - | 0.00081 | 0.00087 | 0.0007 | 0.00123 | 0.00091 | 0.00103 | 0.001 |
| W | mg/L | - | - | 0.00195 | 0.00186 | 0.00197 | 0.00195 | 0.00193 | 0.00203 | 0.00164 |
| Y | mg/L | - | - | 0.000005 | < 0.000005 | 0.000013 | 0.000017 | 0.000014 | 0.000014 | 0.000009 |
| Zn | mg/L | 0.50 | 0.03 | 0.003 | 0.0038 | 0.0098 | 0.0105 | 0.0052 | 0.0032 | 0.0015 |
| Other Parameters | | | | | | | | | | |
| Thiosalts | as S ₂ O ₃ mg/L | - | - | 171 | - | - | - | - | - | - |
| S2O3 | mg/L | - | - | - | 1.4 | 2.3 | 0.9 | 0.2 | < 2 | 1.2 |
| S3O6 | mg/L | - | - | - | 6 | 2 | < 2 | < 2 | < 2 | < 2 |
| S4O6 | mg/L | - | - | - | 1.8 | 2.3 | 4.8 | 6.1 | 8.0 | 8.9 |
| CN(T) | mg/L | 1.00 | - | 0.663 | 0.638 | 0.752 | 0.408 | 0.510 | 0.560 | 0.430 |
| CN(F) | mg/L | - | 0.005 | < 0.2 | < 0.2 | < 0.2 | < 0.2 | < 0.2 | < 0.2 | < 0.2 |
| CNWAD | mg/L | - | - | 0.588 | 0.494 | 0.793 | 0.313 | 0.044 | 0.160 | 0.170 |

Notes:

- 1.0** Indicates a value that is elevated relative to the CCME guideline.
 - 1.0** Indicates a value that is elevated relative to the MMER and CCME (if present) guideline values.
- CCME and MMER values provided only as basis of comparison, values above guidelines require further evaluation.

FIGURES

Figure 1a. Summary of Major Element Distribution (ICP) for Argillite Samples Torquay Site Halifax

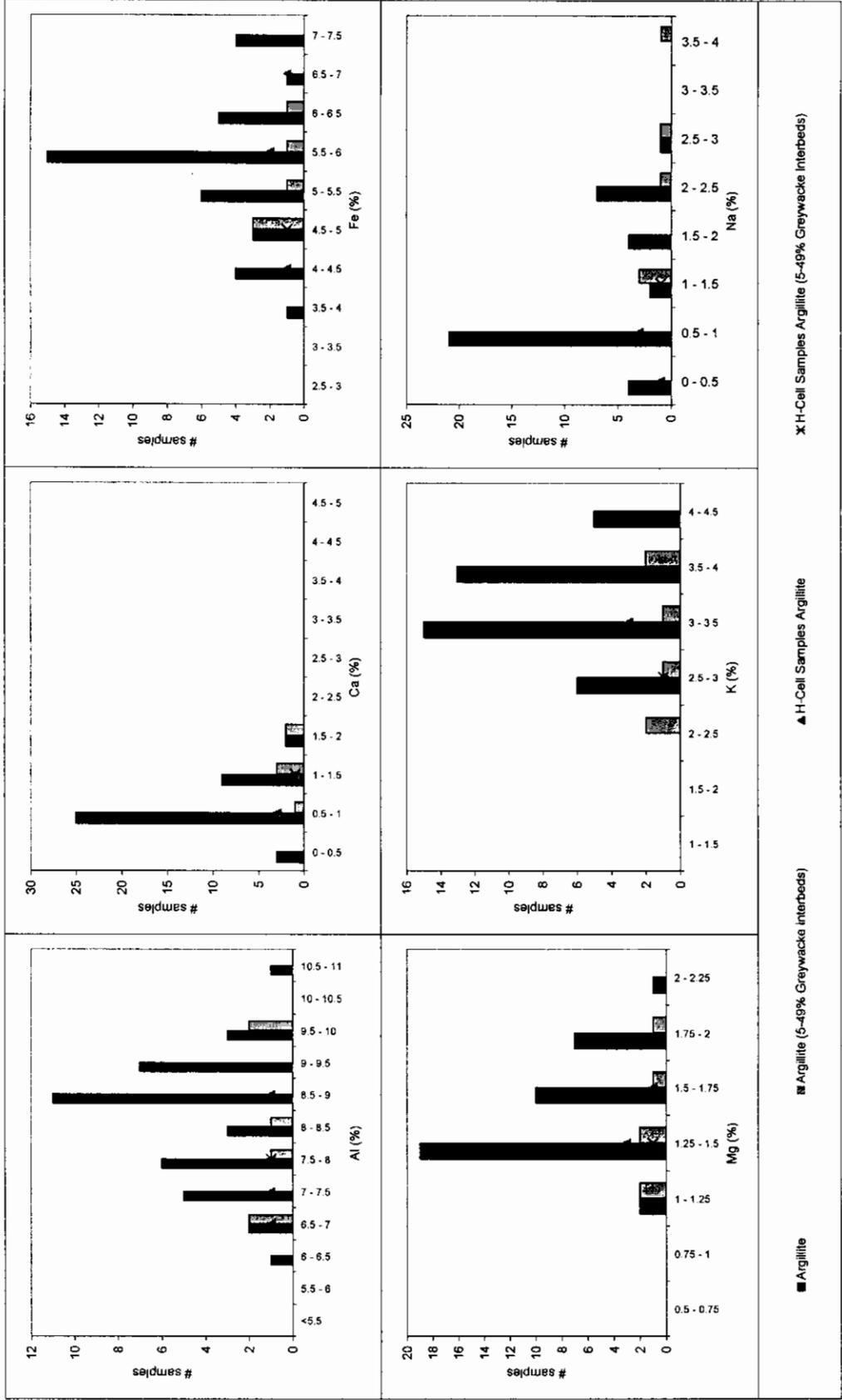


Figure 1b.
Summary of Major Element Distribution (ICP) for Greywacke Samples
Torquay Site
Halifax

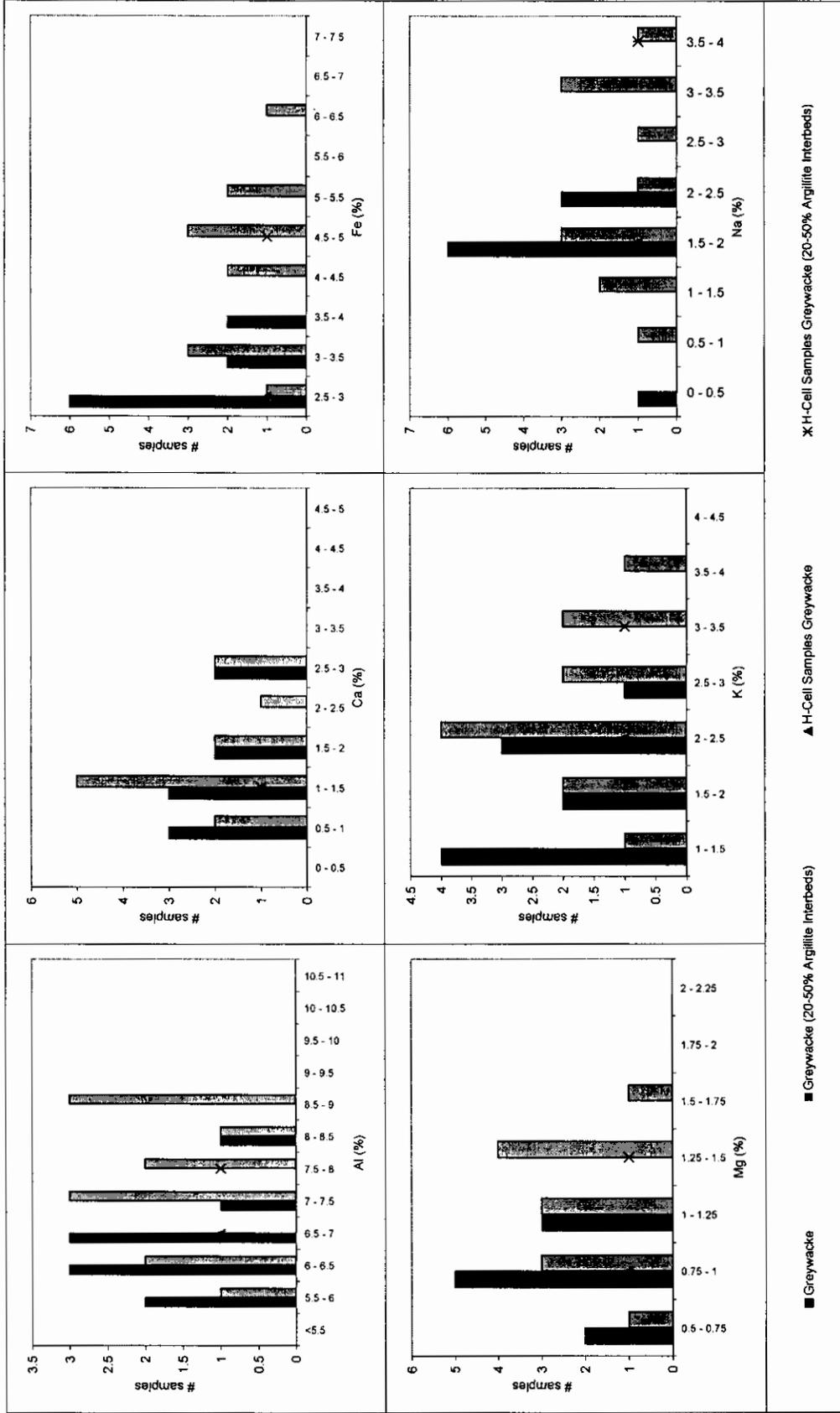


Figure 1c.
Summary of Major Element Distribution (ICP) for Composite and Marginal Ore Samples
Touquoy Site
Halifax

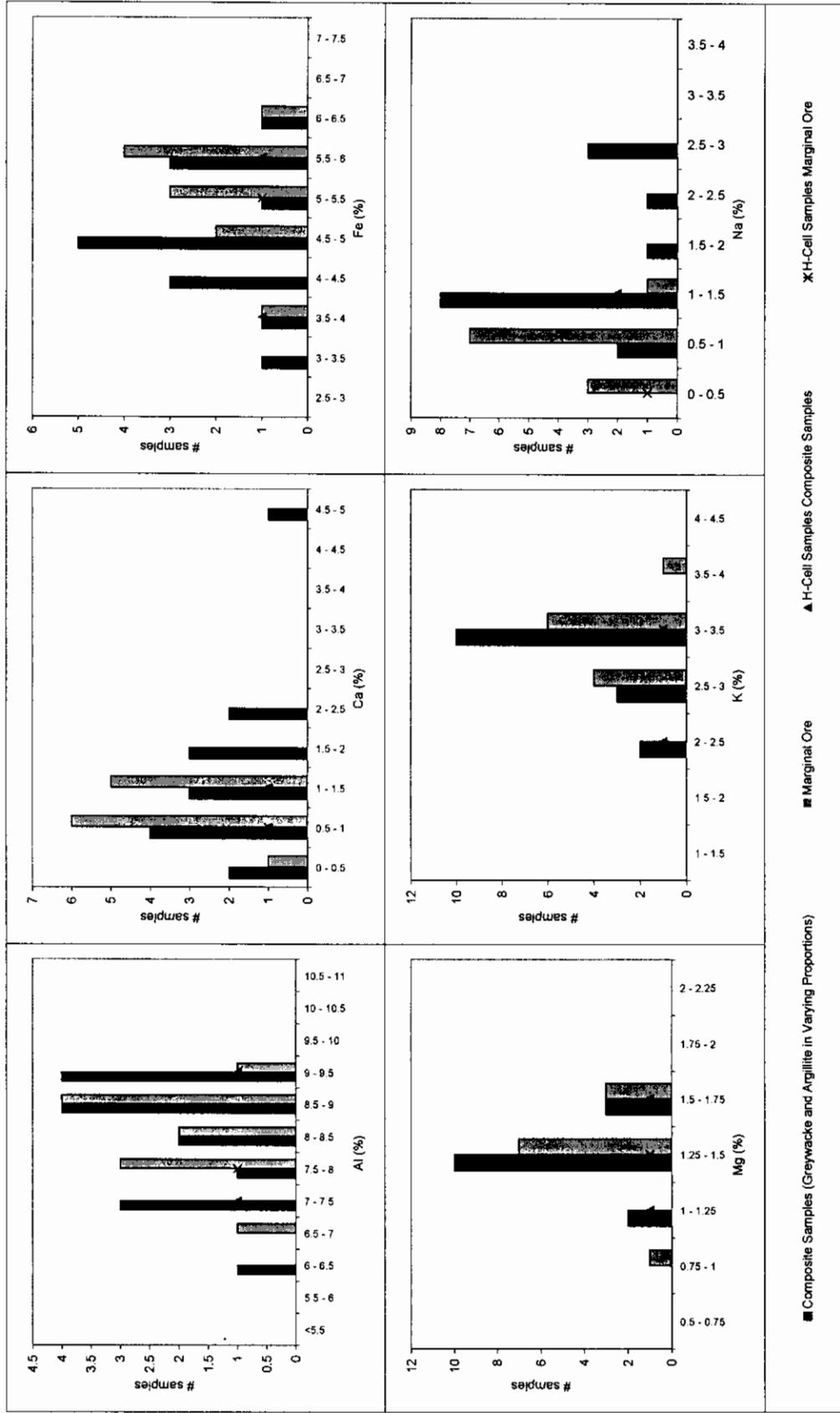


Figure 2a.
 Summary of Sulphide and ICP Trace Metal Distributions for Argillite Samples
 Touquoy Site
 Halifax

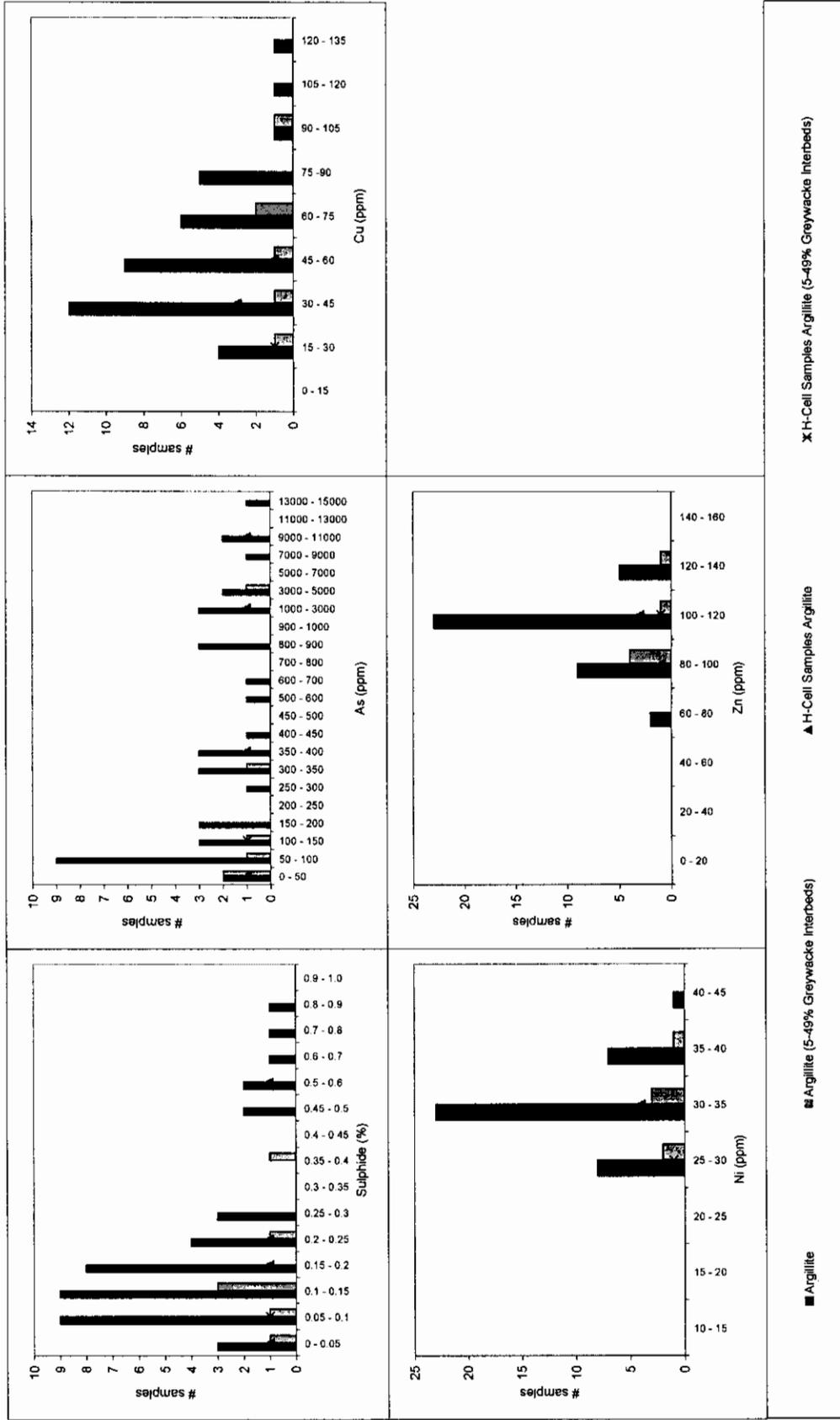


Figure 2b. Summary of Sulphide and Trace Metal Distributions for Greywacke Samples Touquoy Site Halifax

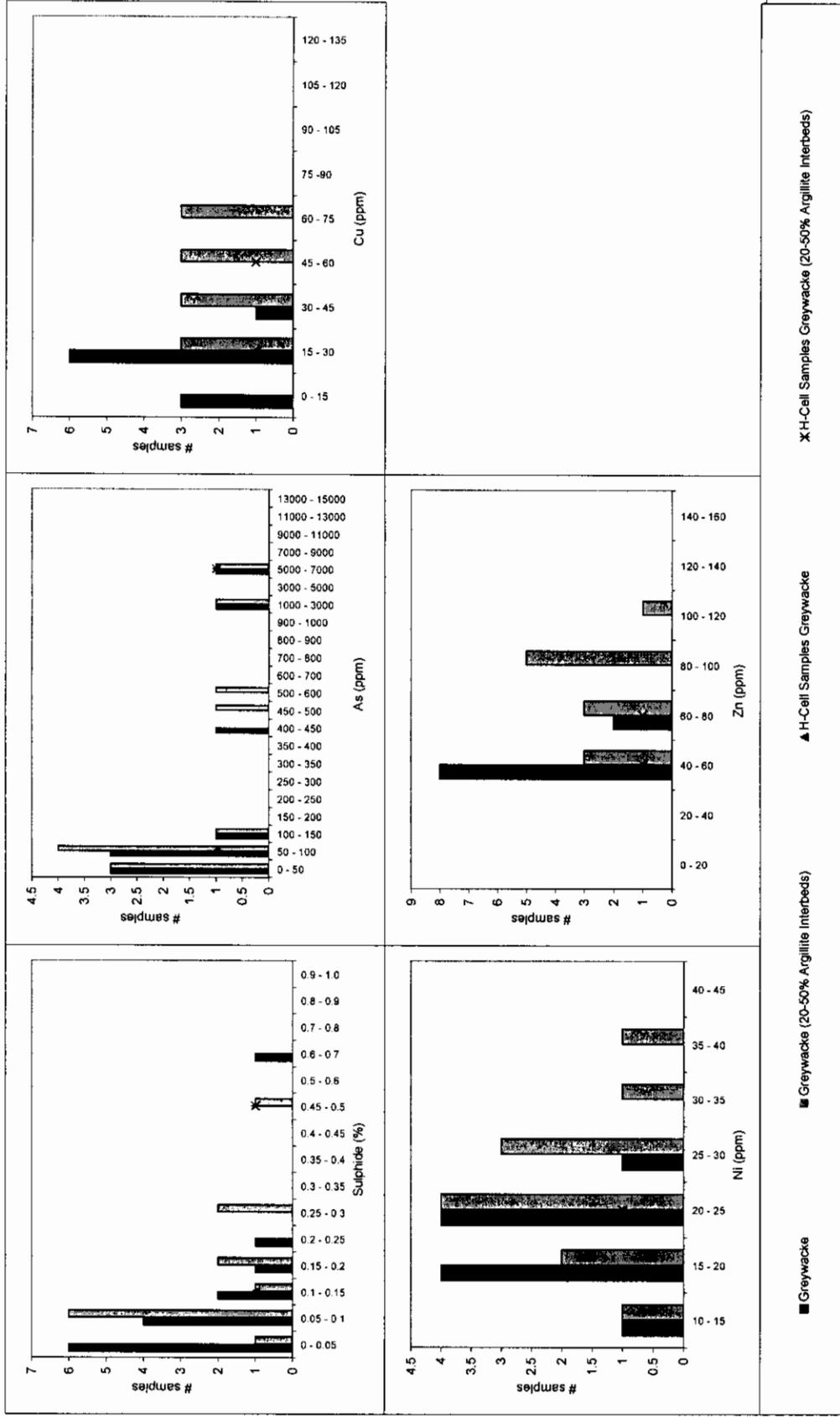


Figure 2c. Summary of Sulphide and ICP Trace Metal Distributions for Composite and Marginal Ore Samples Touquoy Site Halifax

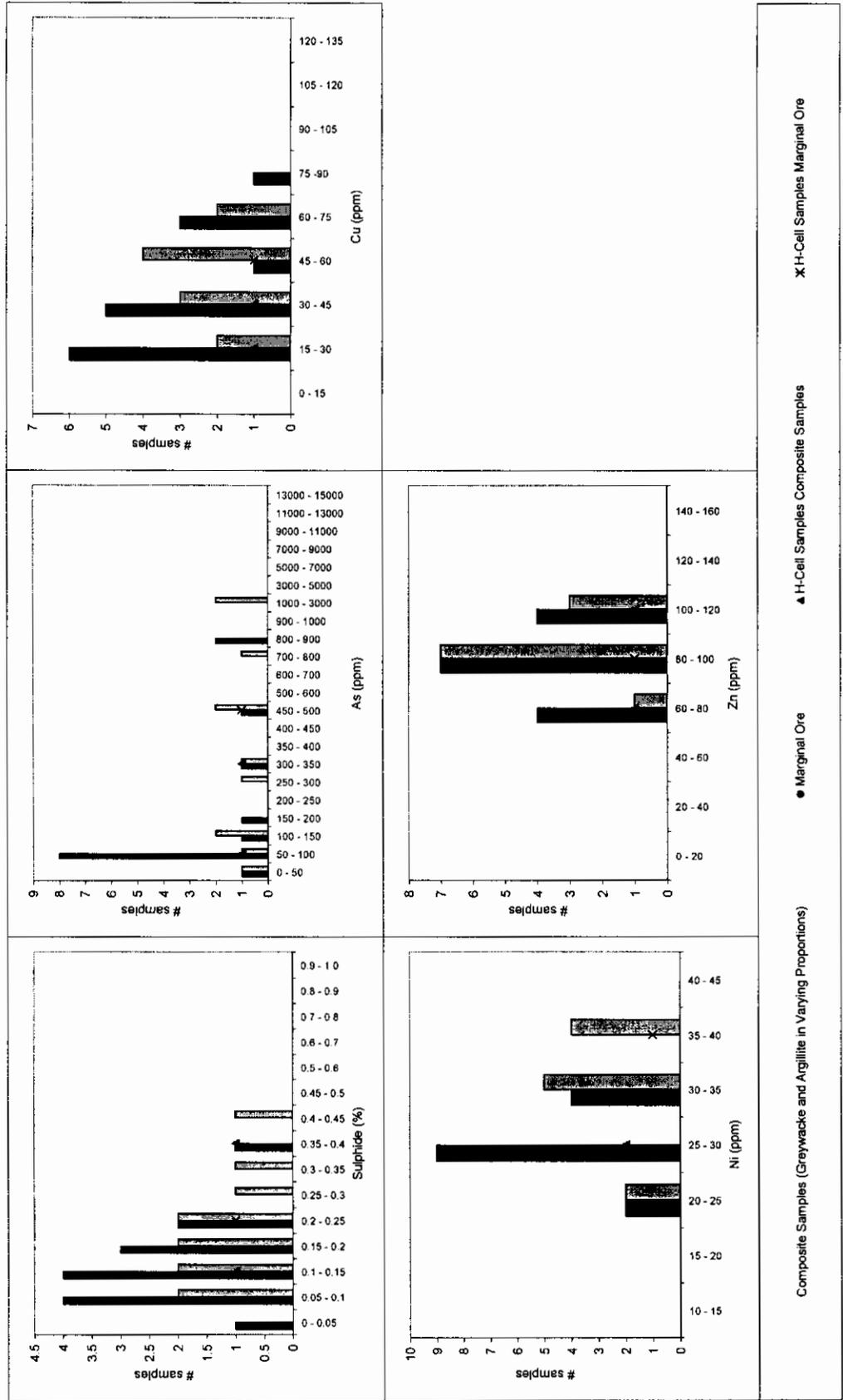
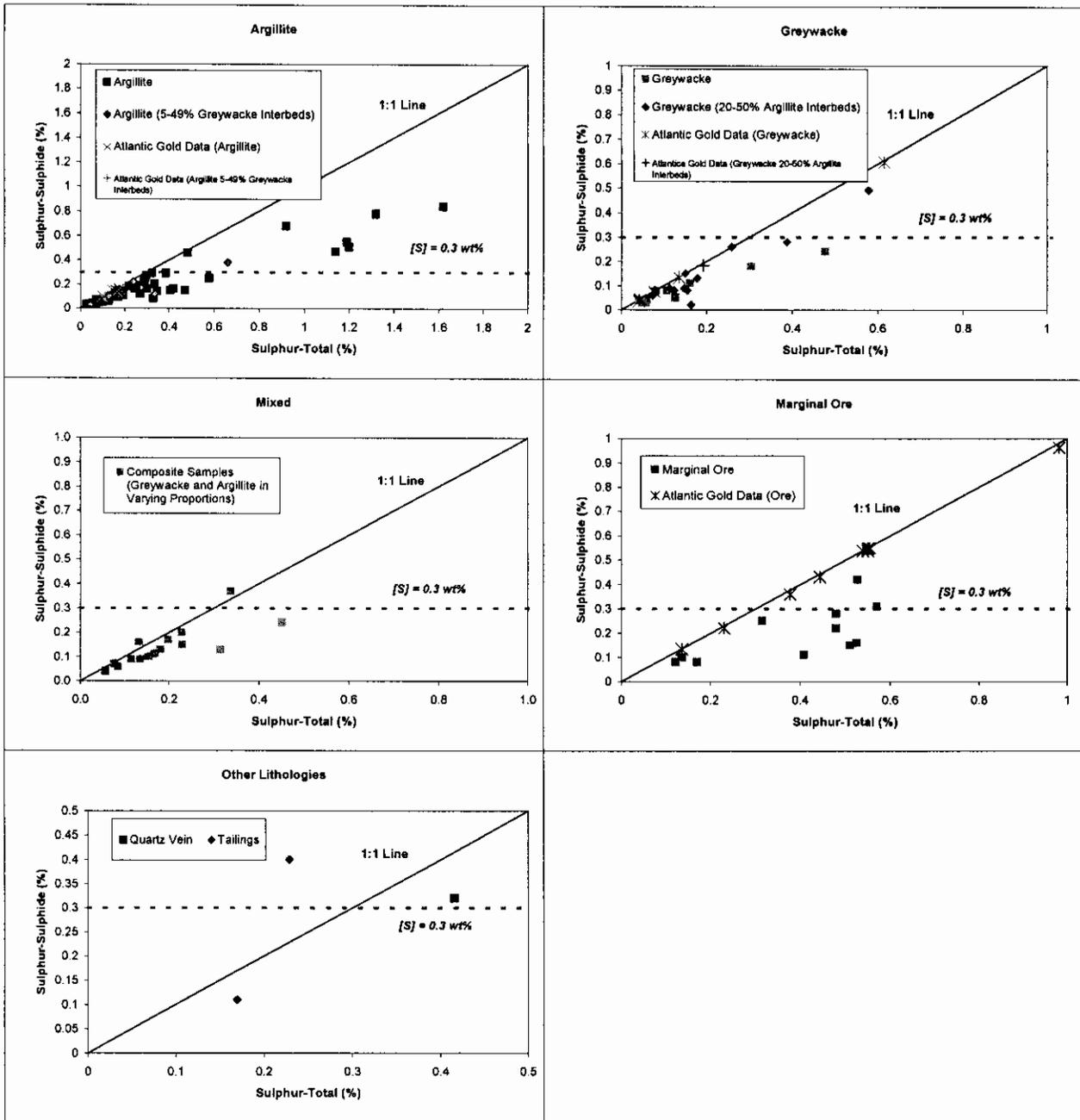


Figure 3.
Sulphide Sulphur vs. Total Sulphur by Lithology



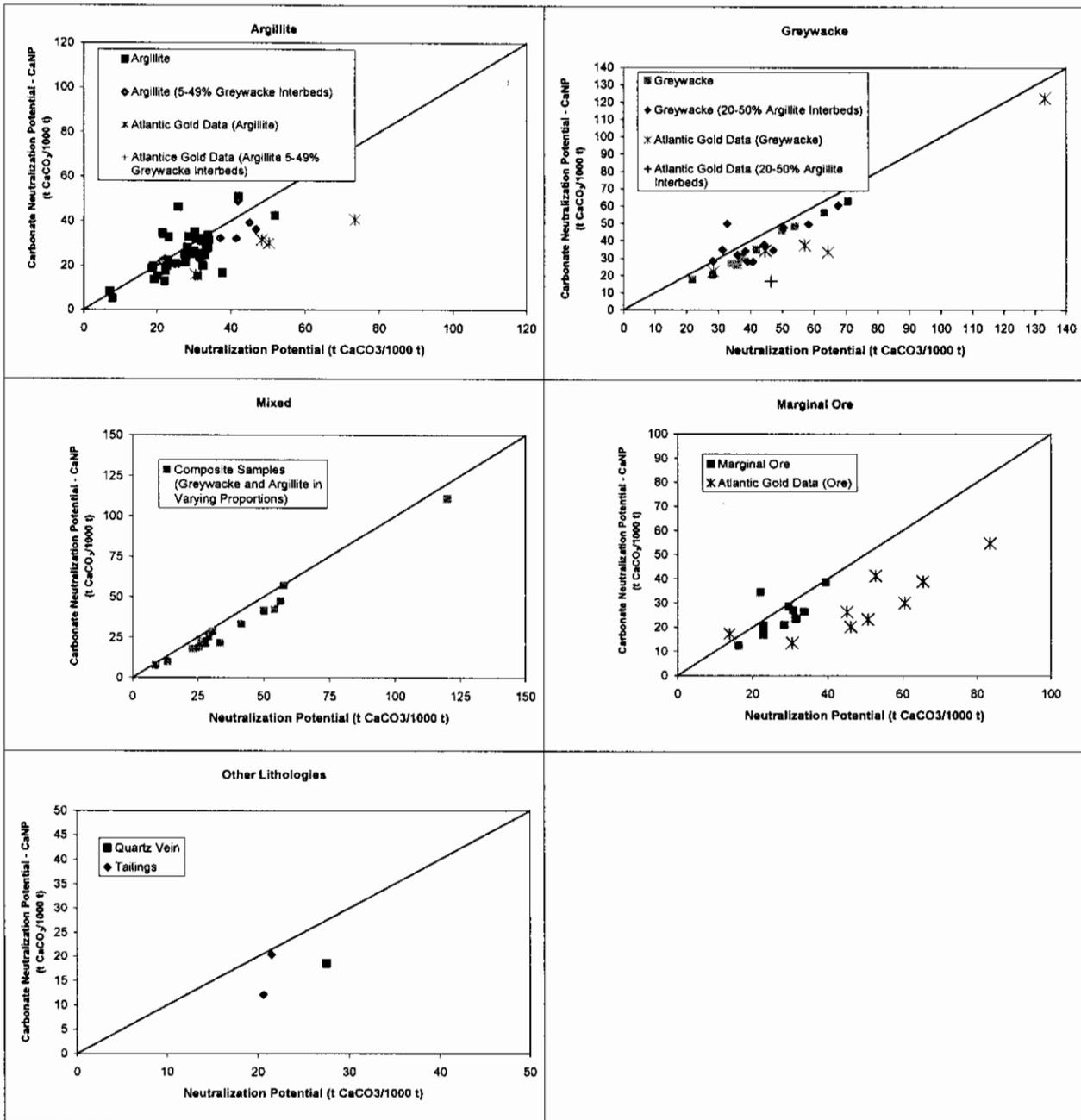
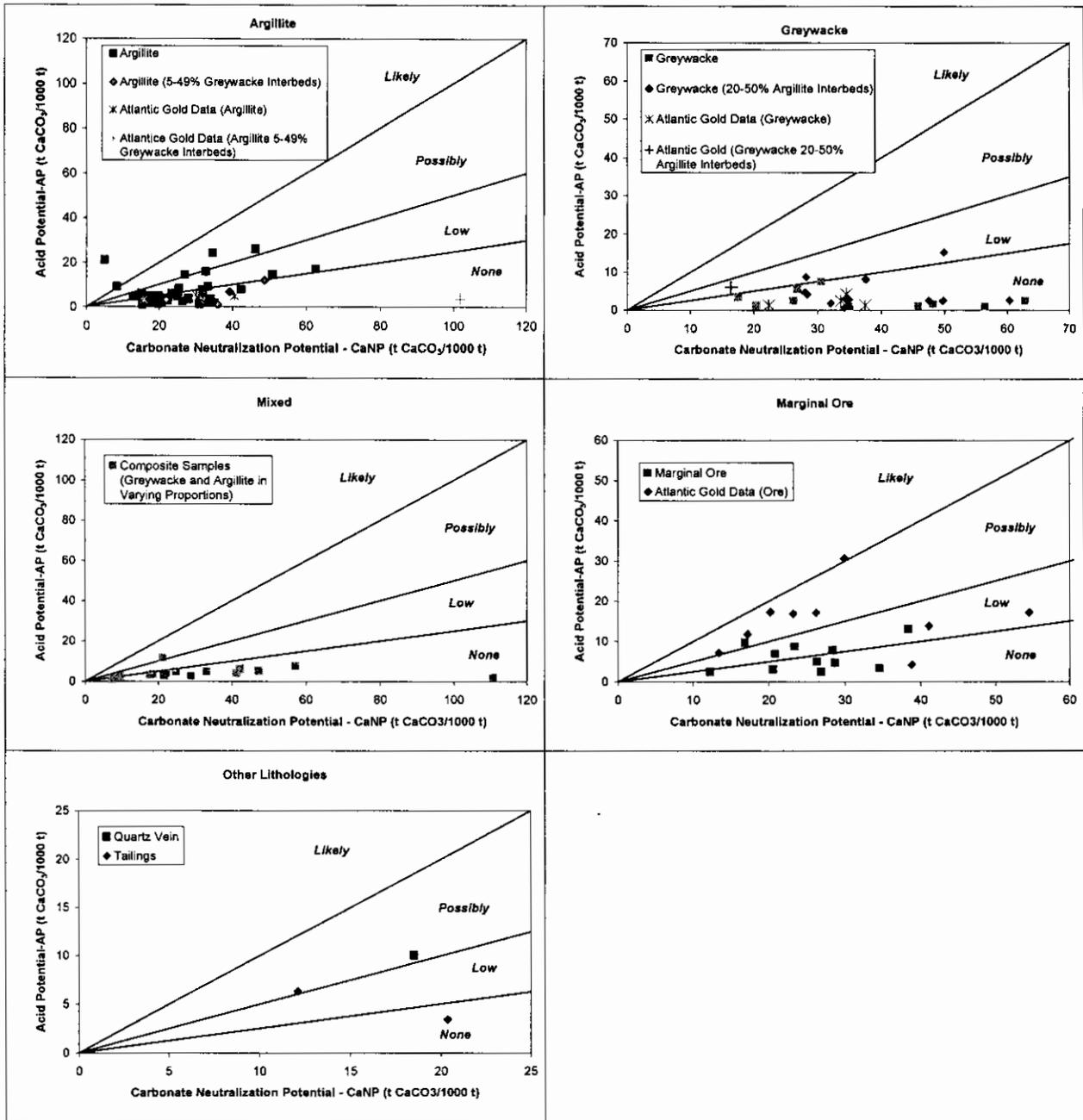


Figure 5. Potential for Acid Rock Drainage (Acid Potential vs. Carbonate Neutralization Potential) by Lithology



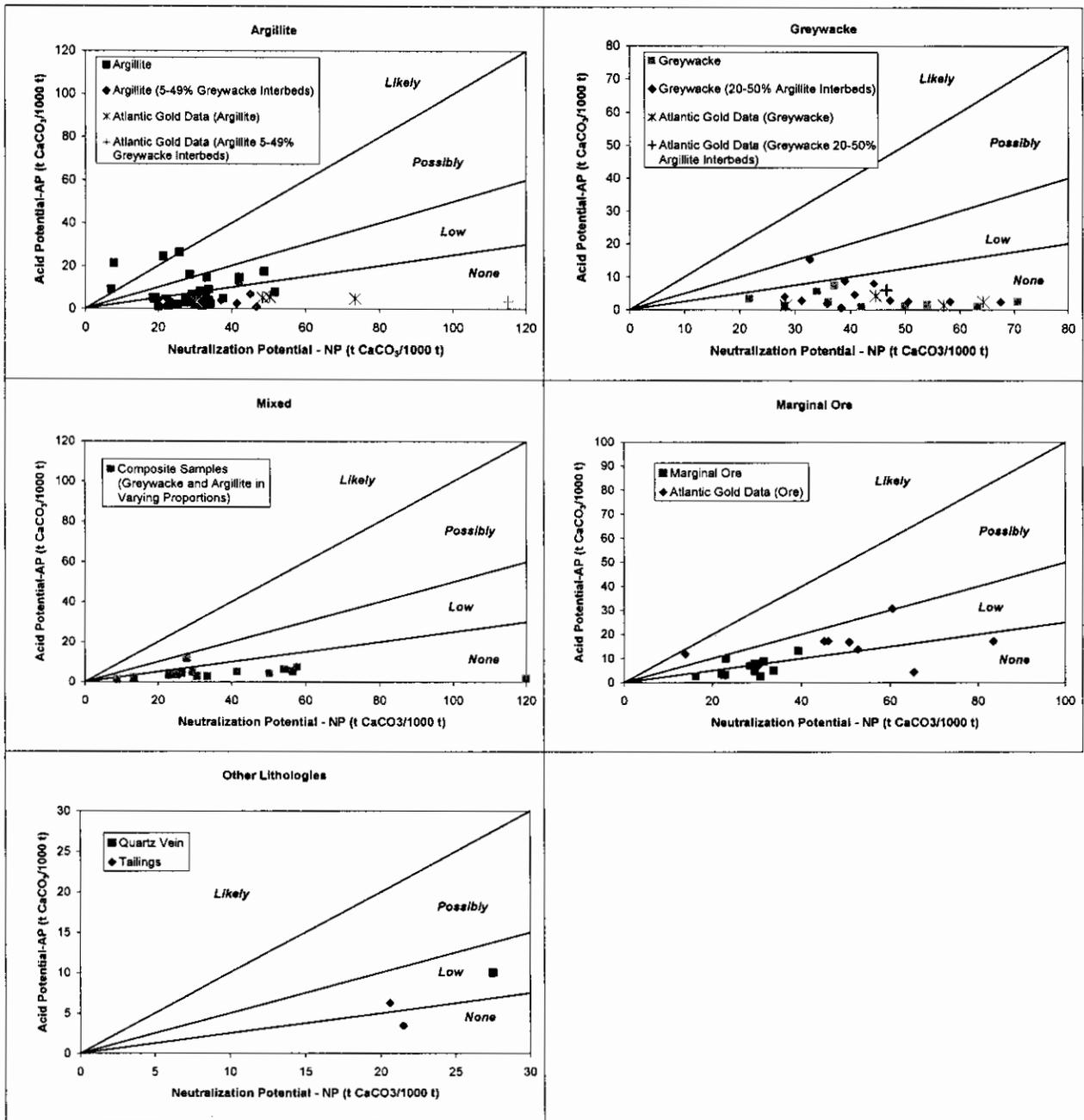


Figure 7a. Summary of Short Term Leach Results for Argillite Samples Torquay Site Halifax.

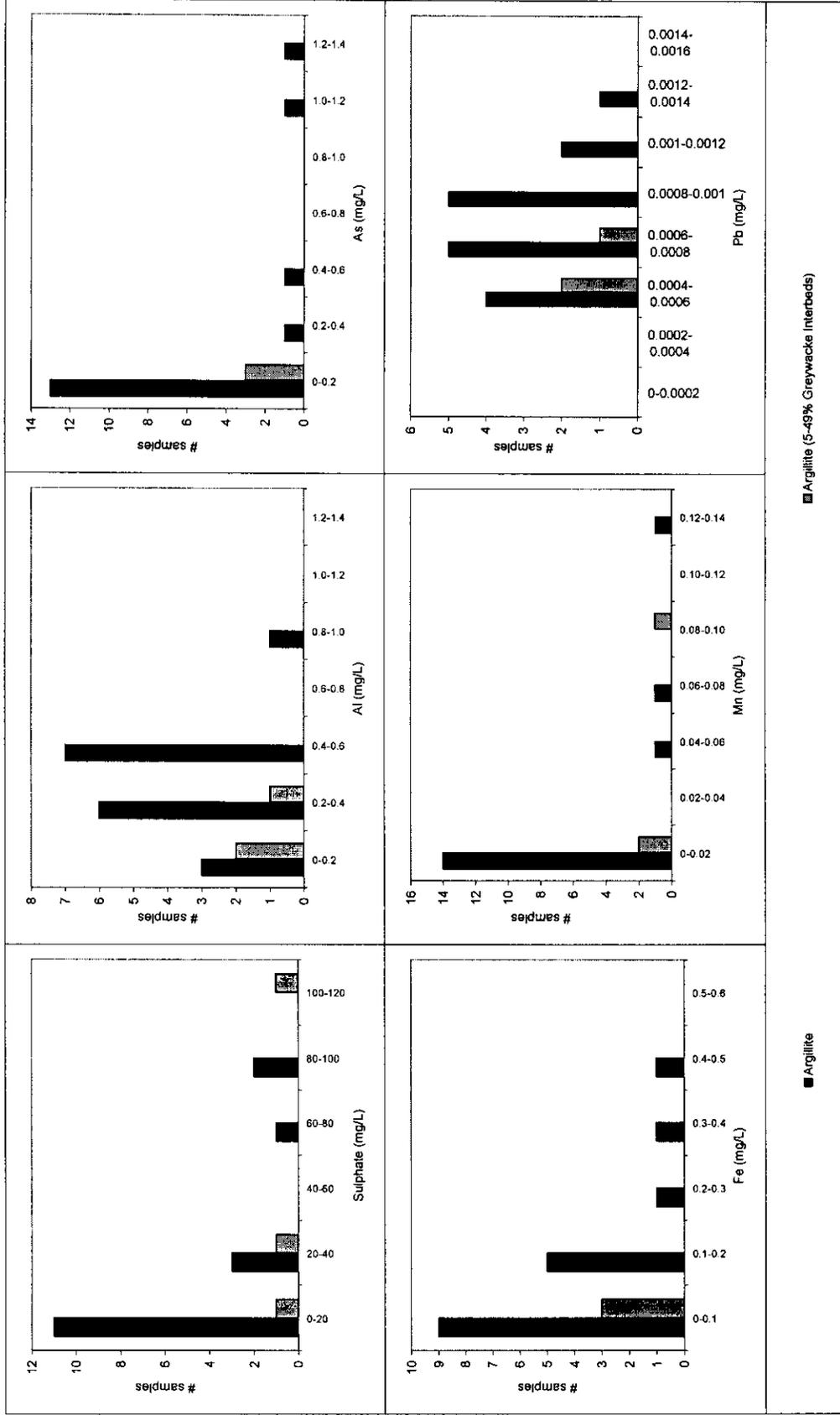


Figure 7b. Summary of Short Term Leach Results for Greywacke Samples Touquoy Site Halifax

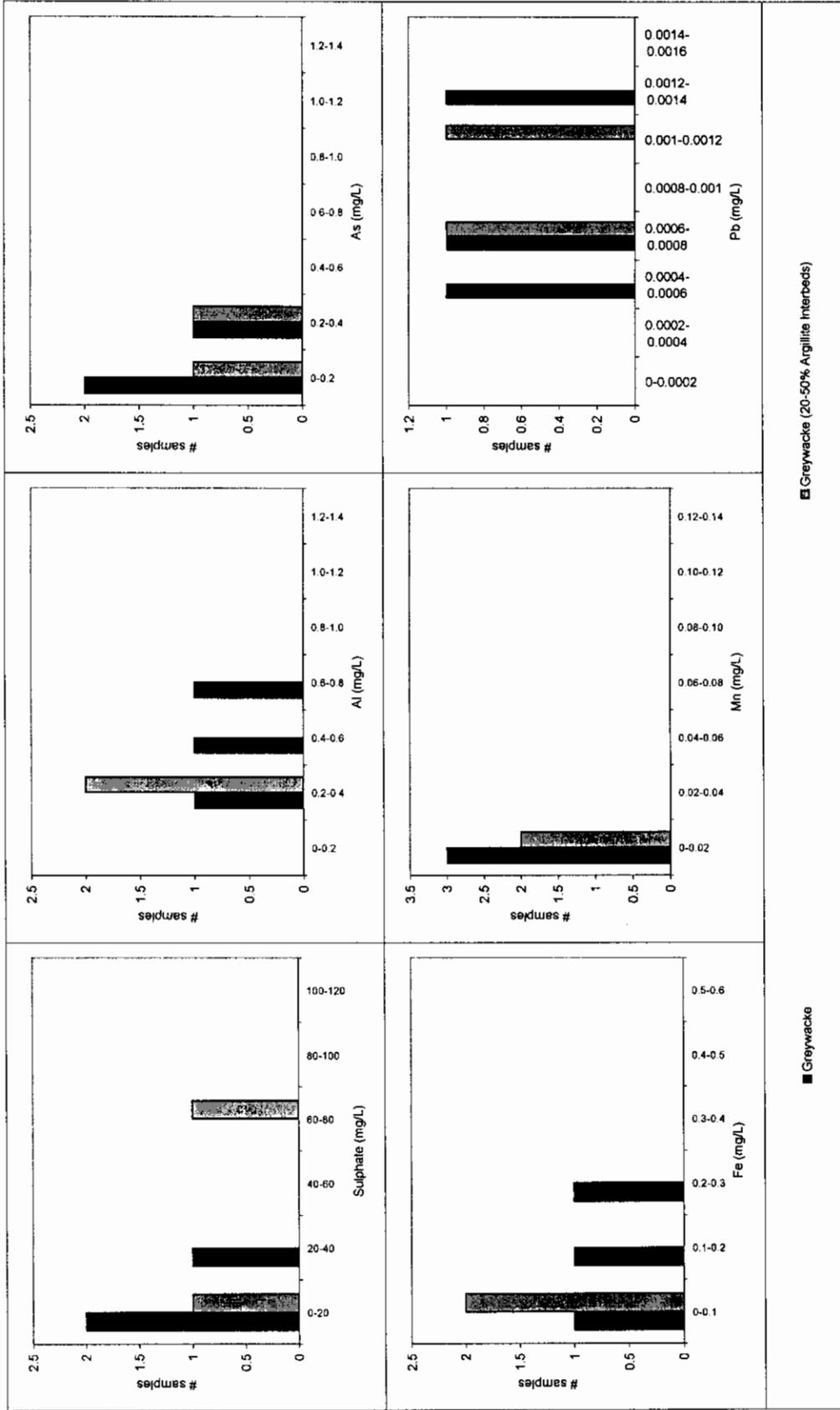


Figure 7c.
Summary of Short Term Leach Results for Composite and Marginal Ore Samples
Touquoy Site
Halifax

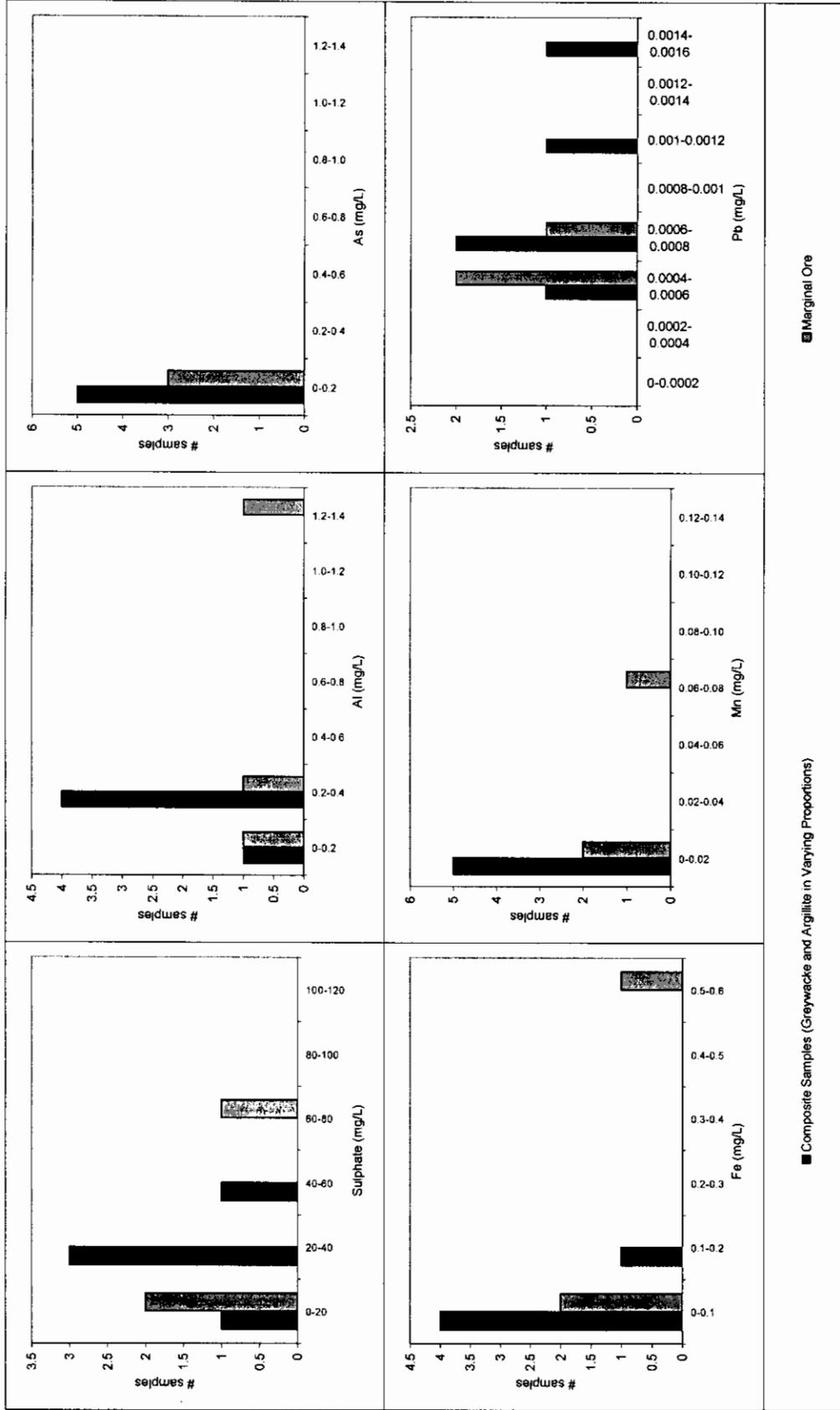
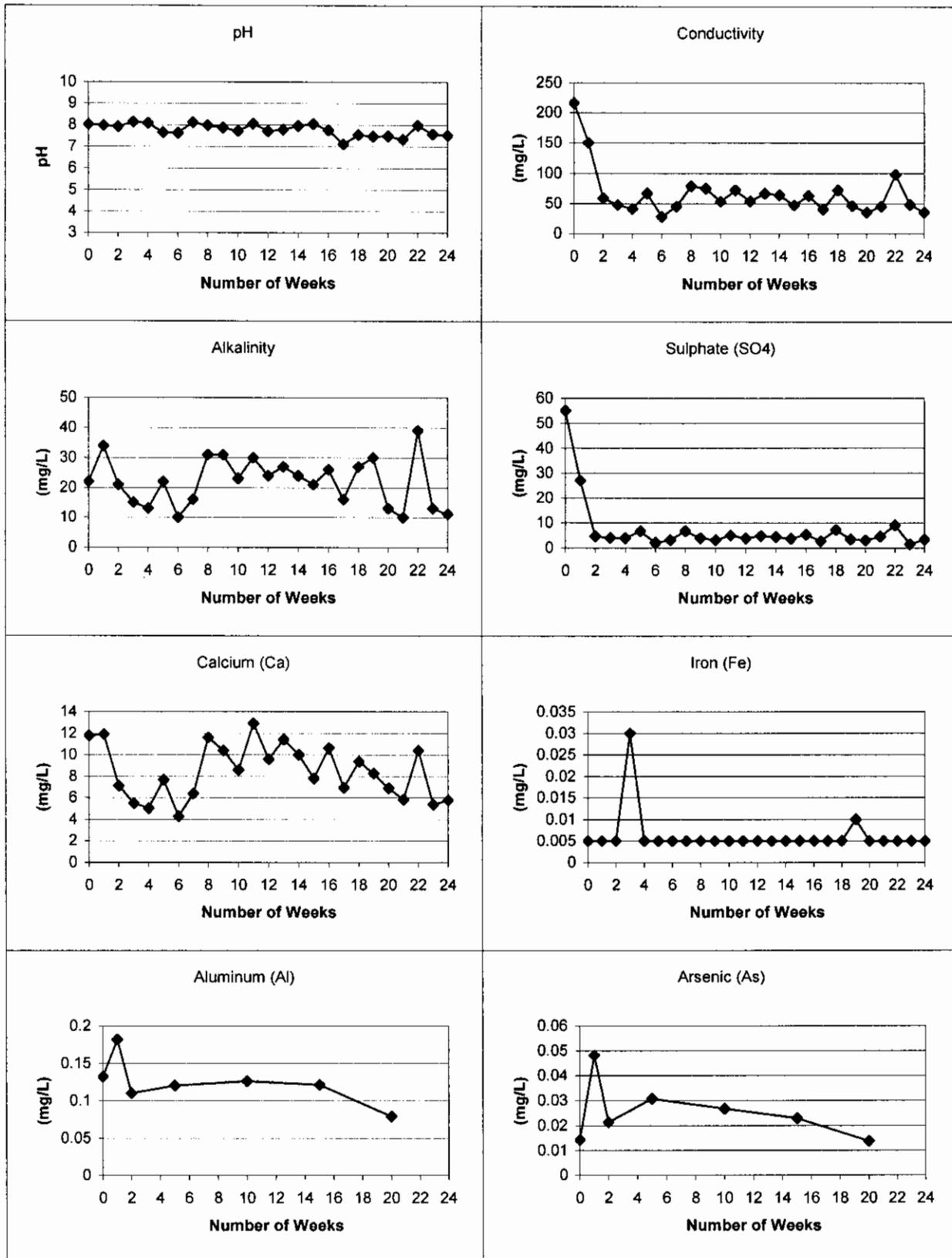


FIGURE 8a
 HUMIDITY CELL RESULTS FOR HC 06-006
 Argillite (<5% Greywacke)



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FIGURE 8a
HUMIDITY CELL RESULTS FOR HC 06-006
Argillite (<5% Greywacke)

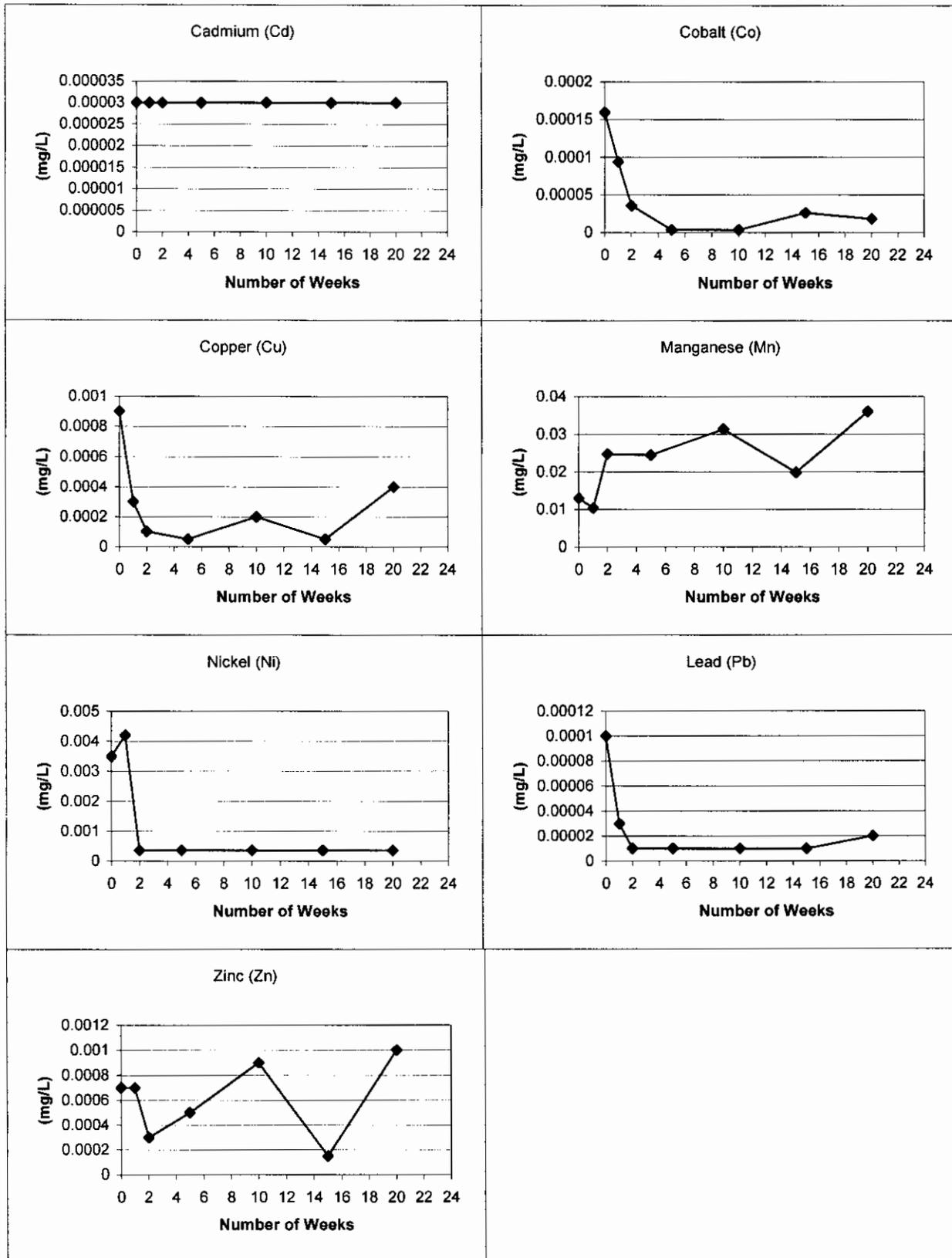
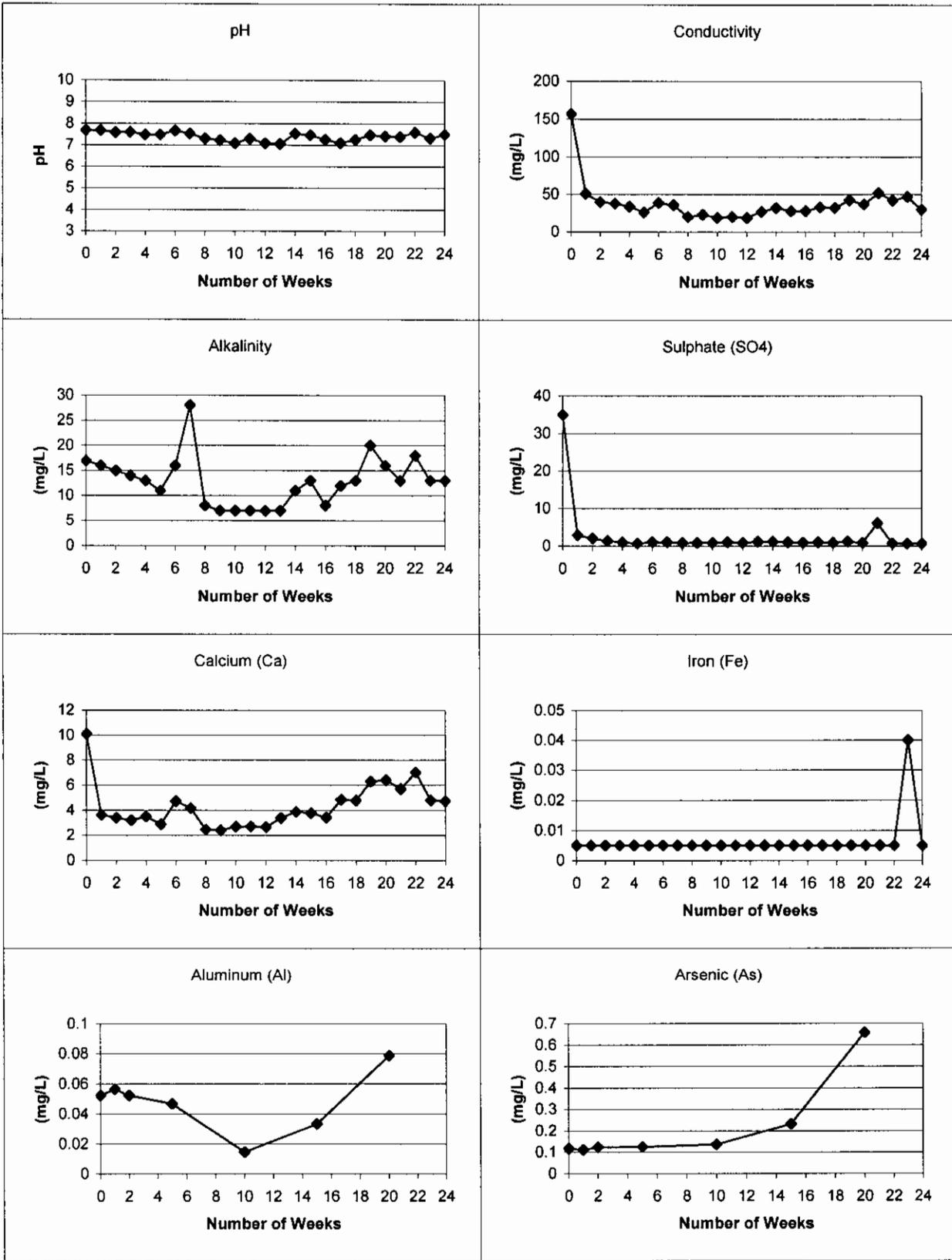
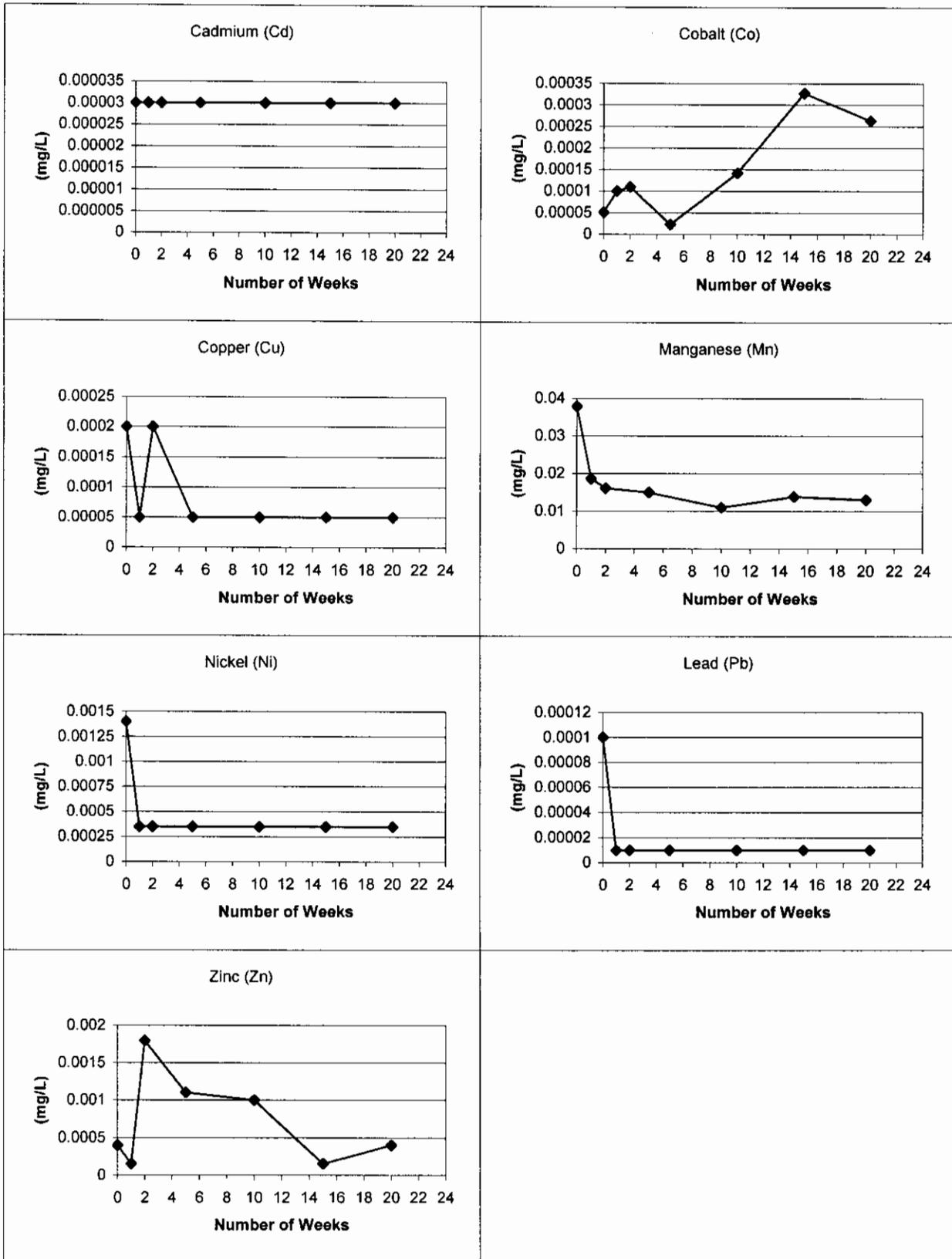


FIGURE 8b
 HUMIDITY CELL RESULTS FOR HC 06-017
 Argillite (<5% Greywacke)



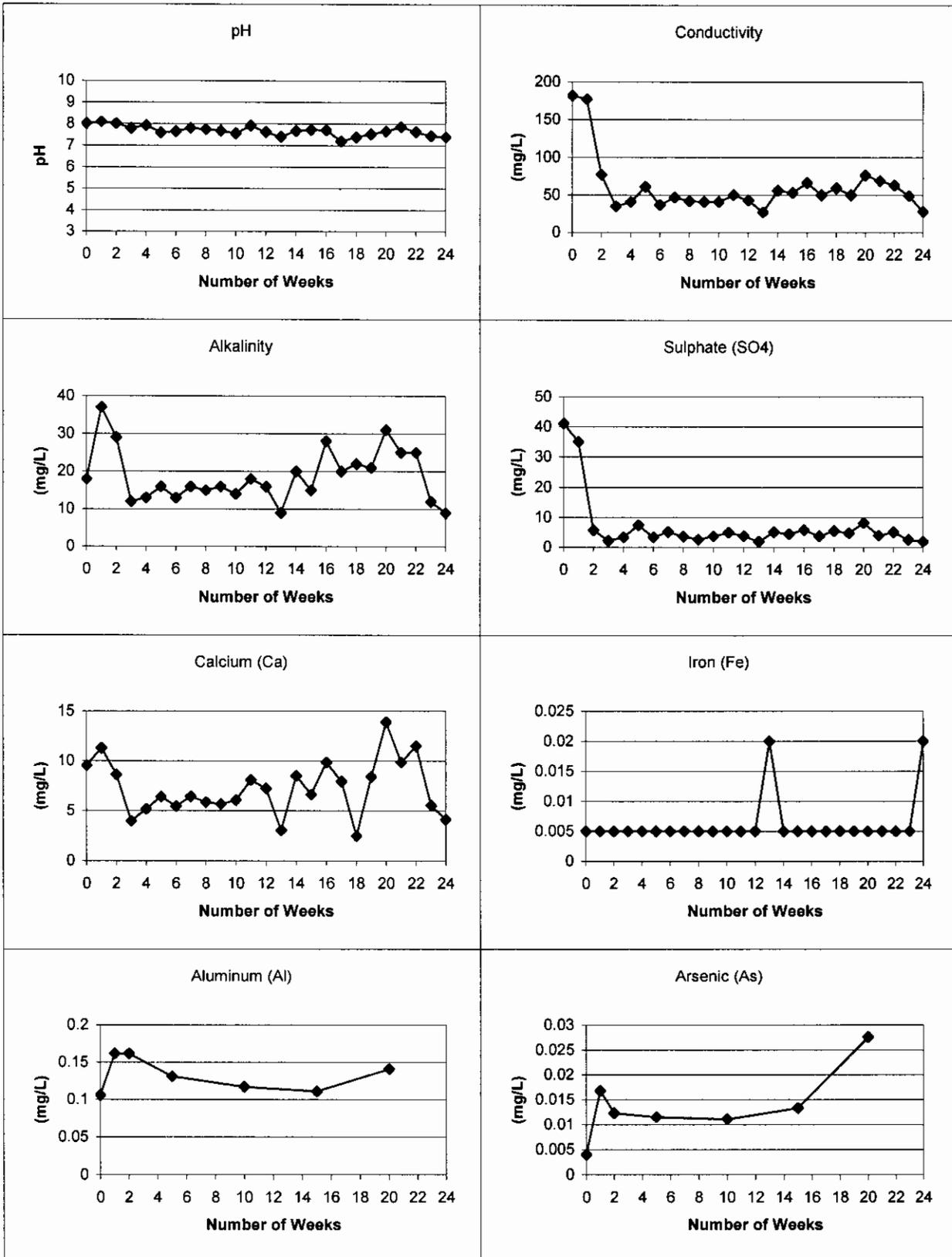
Golder Associates

FIGURE 8b
HUMIDITY CELL RESULTS FOR HC 06-017
Argillite (<5% Greywacke)



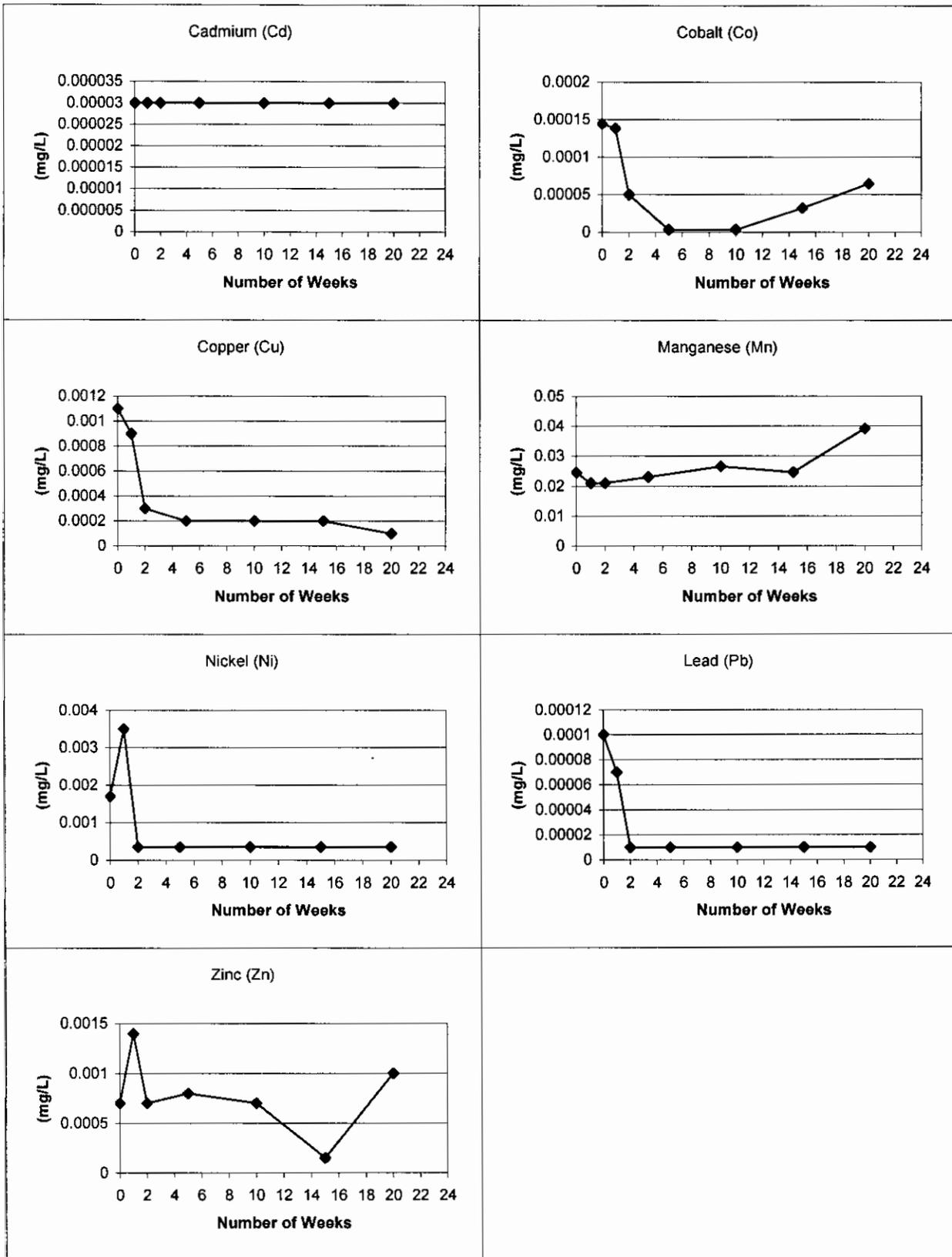
Golder Associates

FIGURE 8c
HUMIDITY CELL RESULTS FOR HC 06-049
 Argillite (<5% Greywacke)



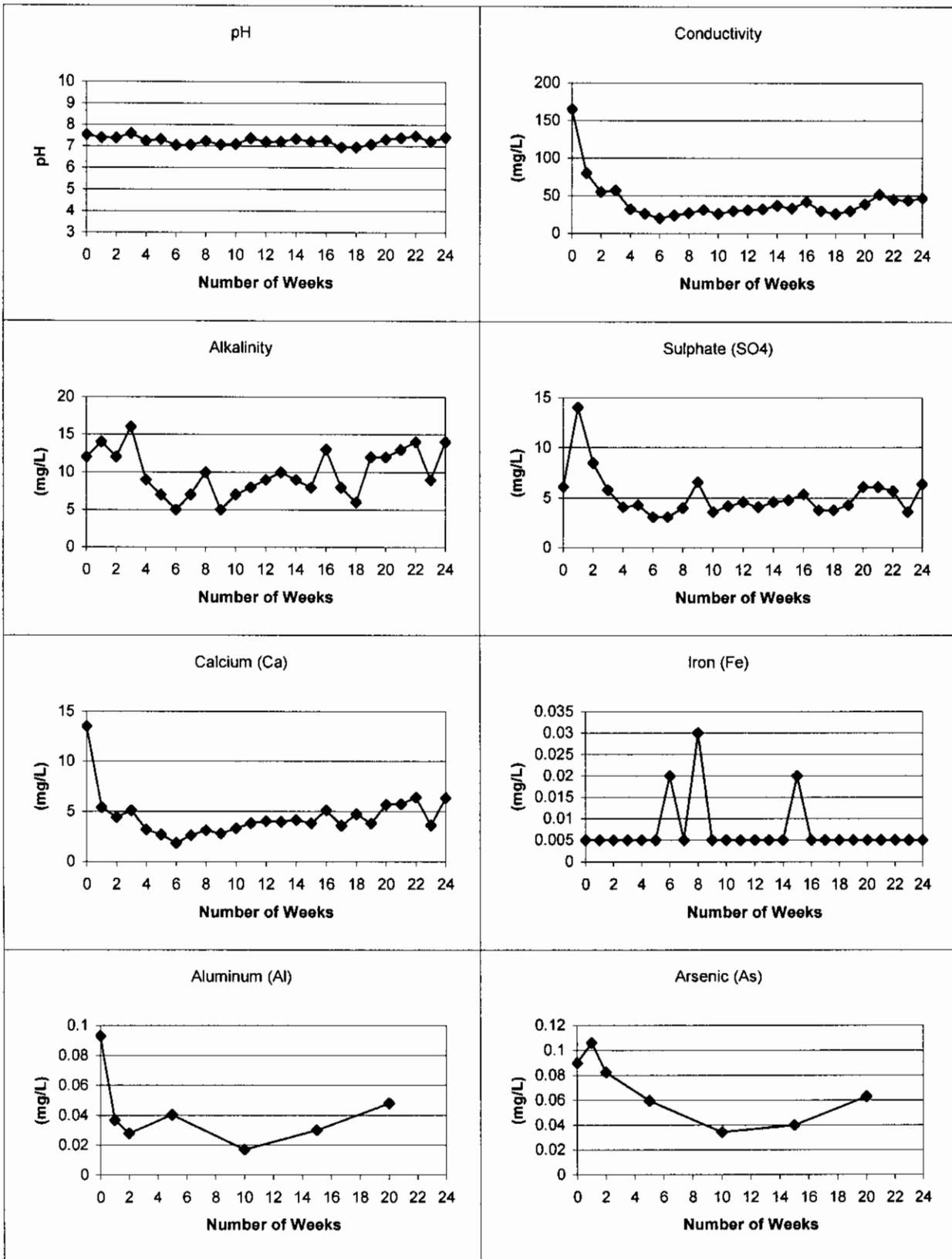
Golder Associates

FIGURE 8c
HUMIDITY CELL RESULTS FOR HC 06-049
Argillite (<5% Greywacke)



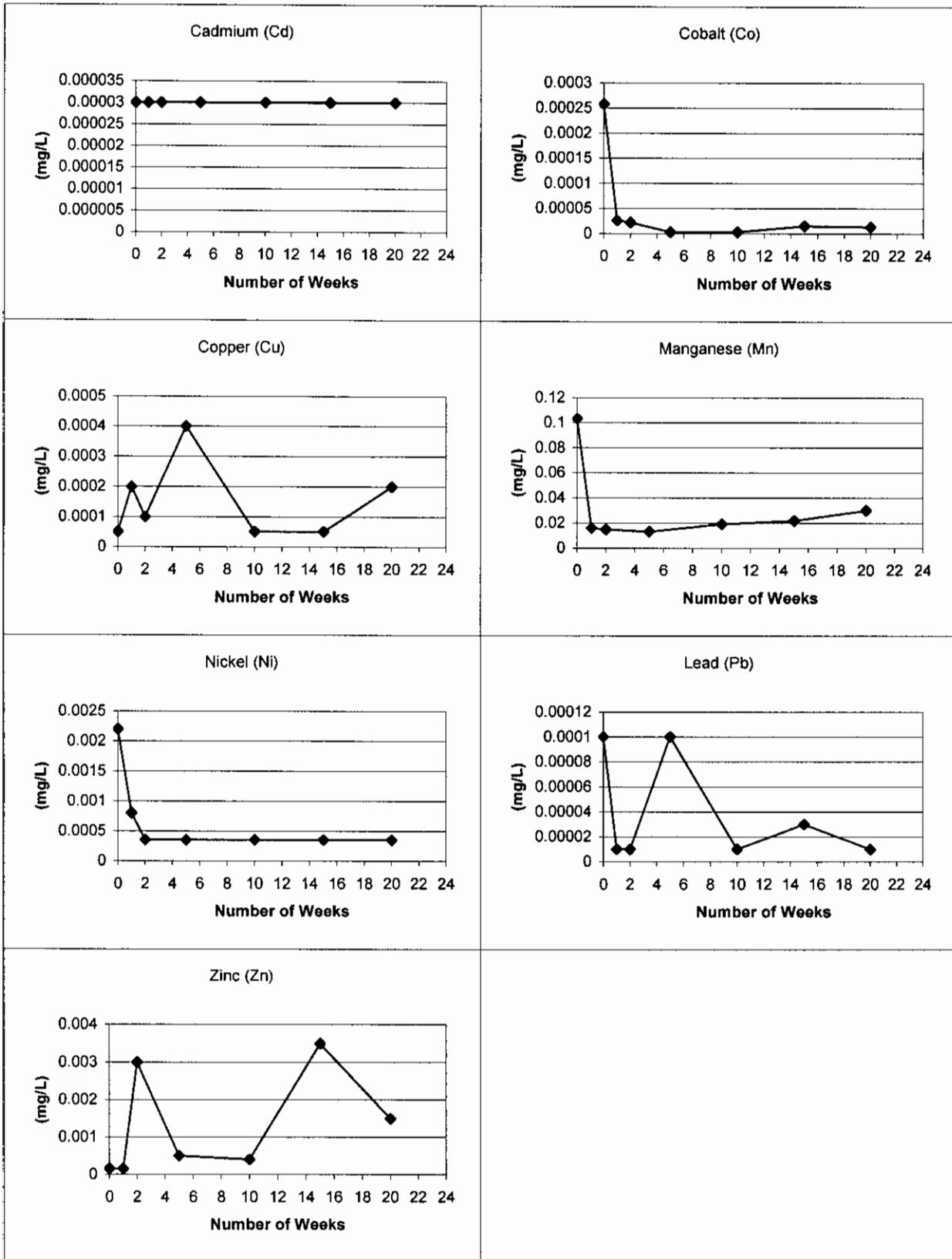
Golder Associates

FIGURE 8d
 HUMIDITY CELL RESULTS FOR HC 06-079
 Argillite (<5% Greywacke)



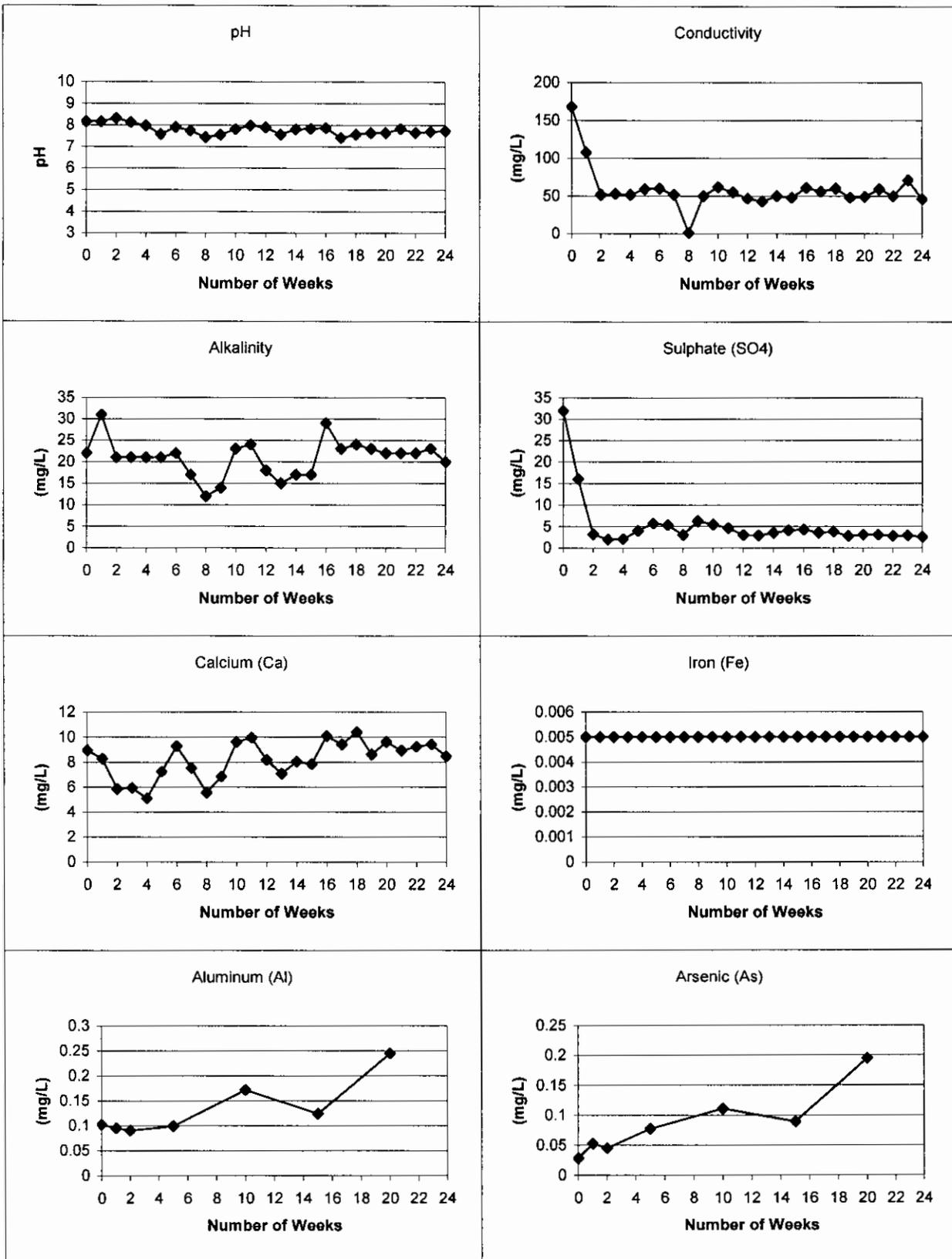
Golder Associates

FIGURE 8d
HUMIDITY CELL RESULTS FOR HC 06-079
Argillite (<5% Greywacke)



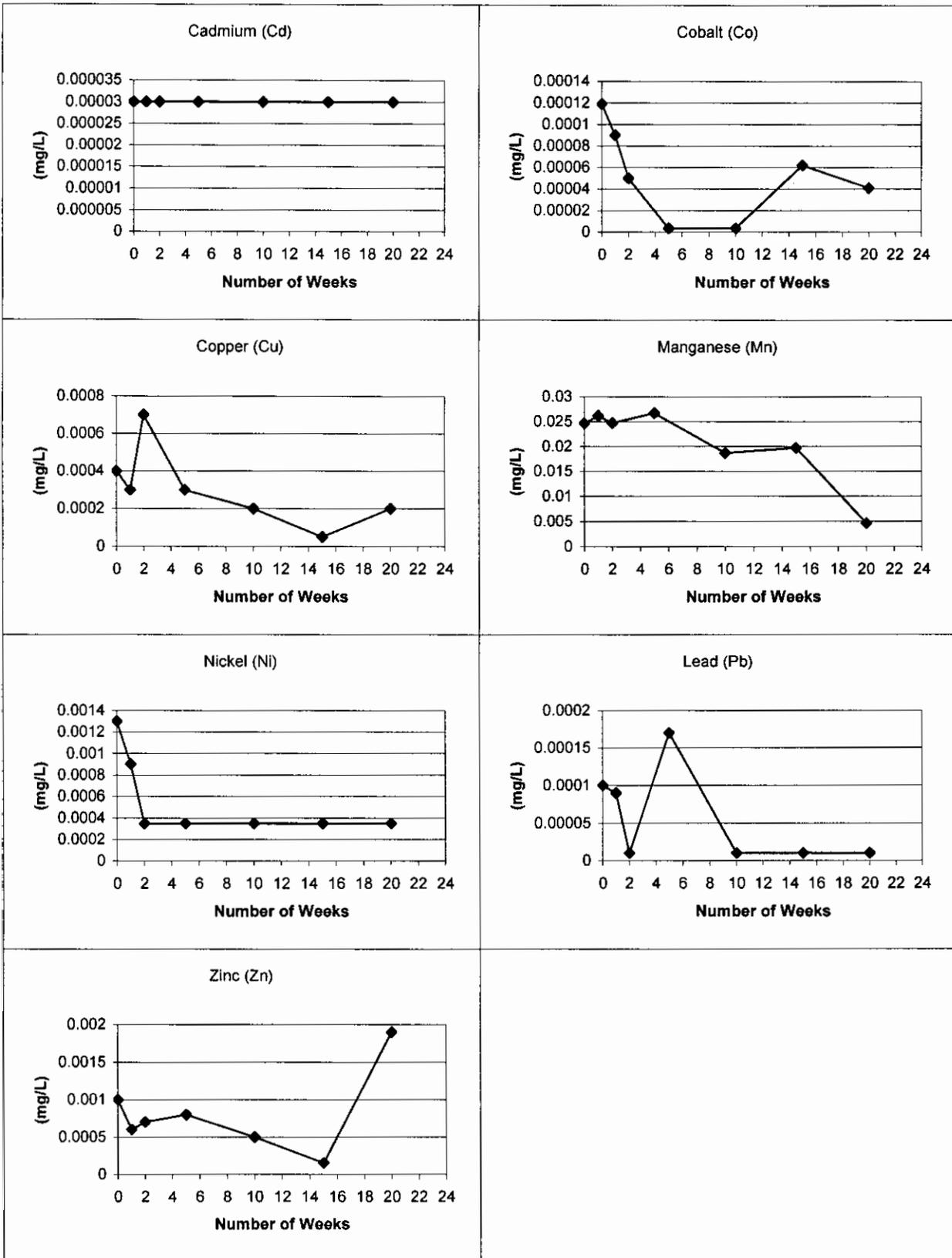
Golder Associates

FIGURE 9
HUMIDITY CELL RESULTS FOR HC 06-068
Greywacke (<20% Argillite Interbeds)



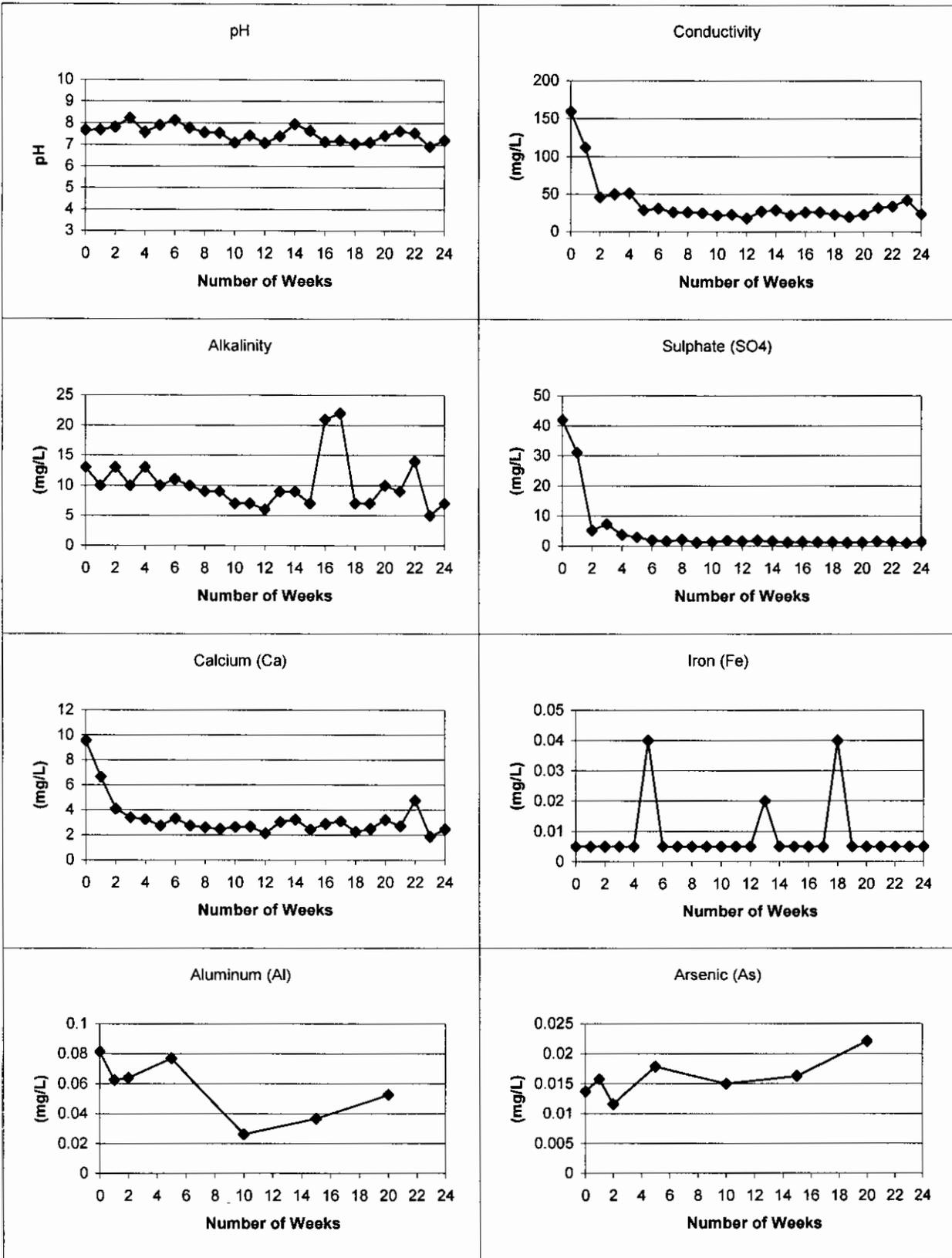
Golder Associates

FIGURE 9
HUMIDITY CELL RESULTS FOR HC 06-068
Greywacke (<20% Argillite Interbeds)



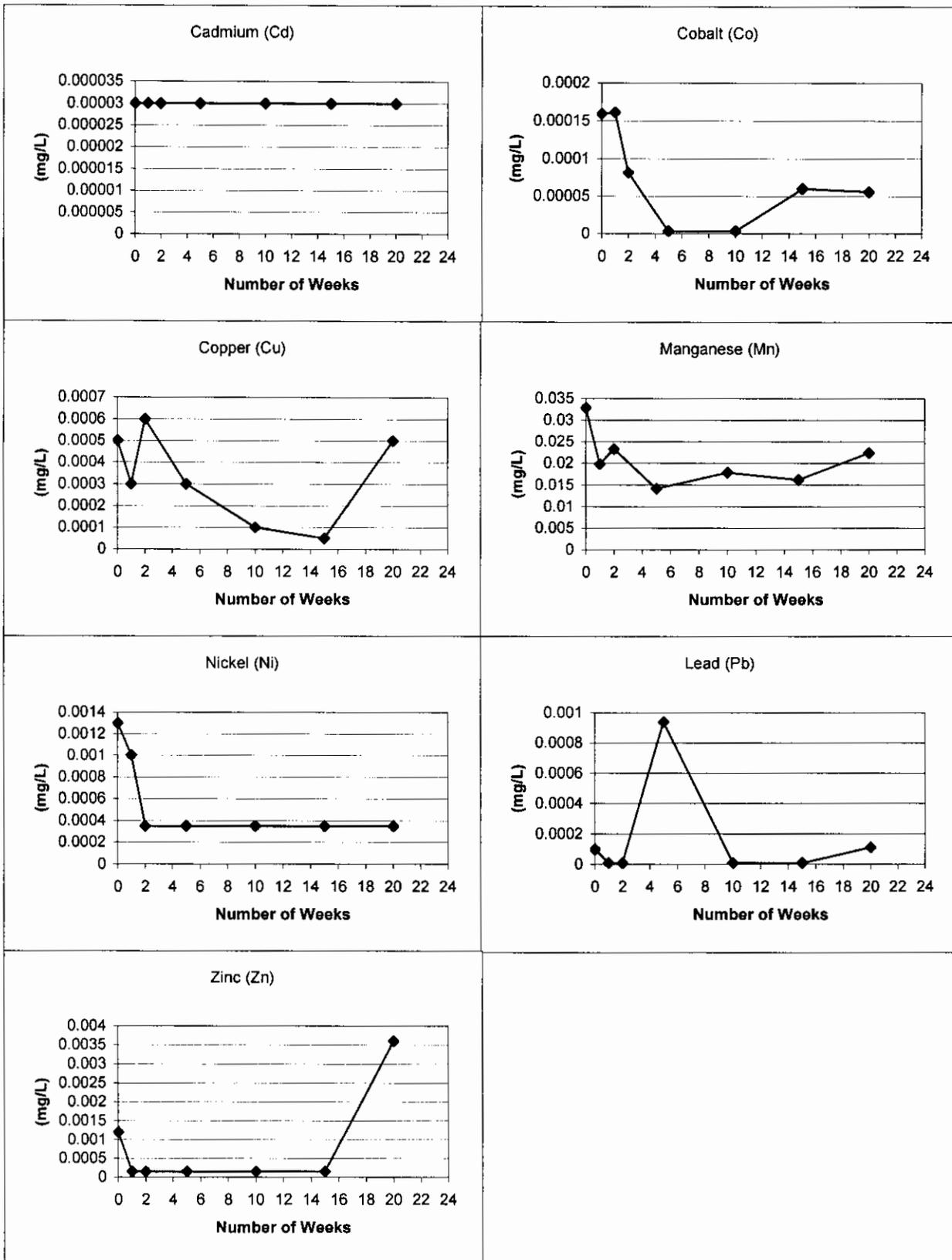
Golder Associates

FIGURE 10
 HUMIDITY CELL RESULTS FOR HC 06-012
 Argillite (5-49% Greywacke Interbeds)



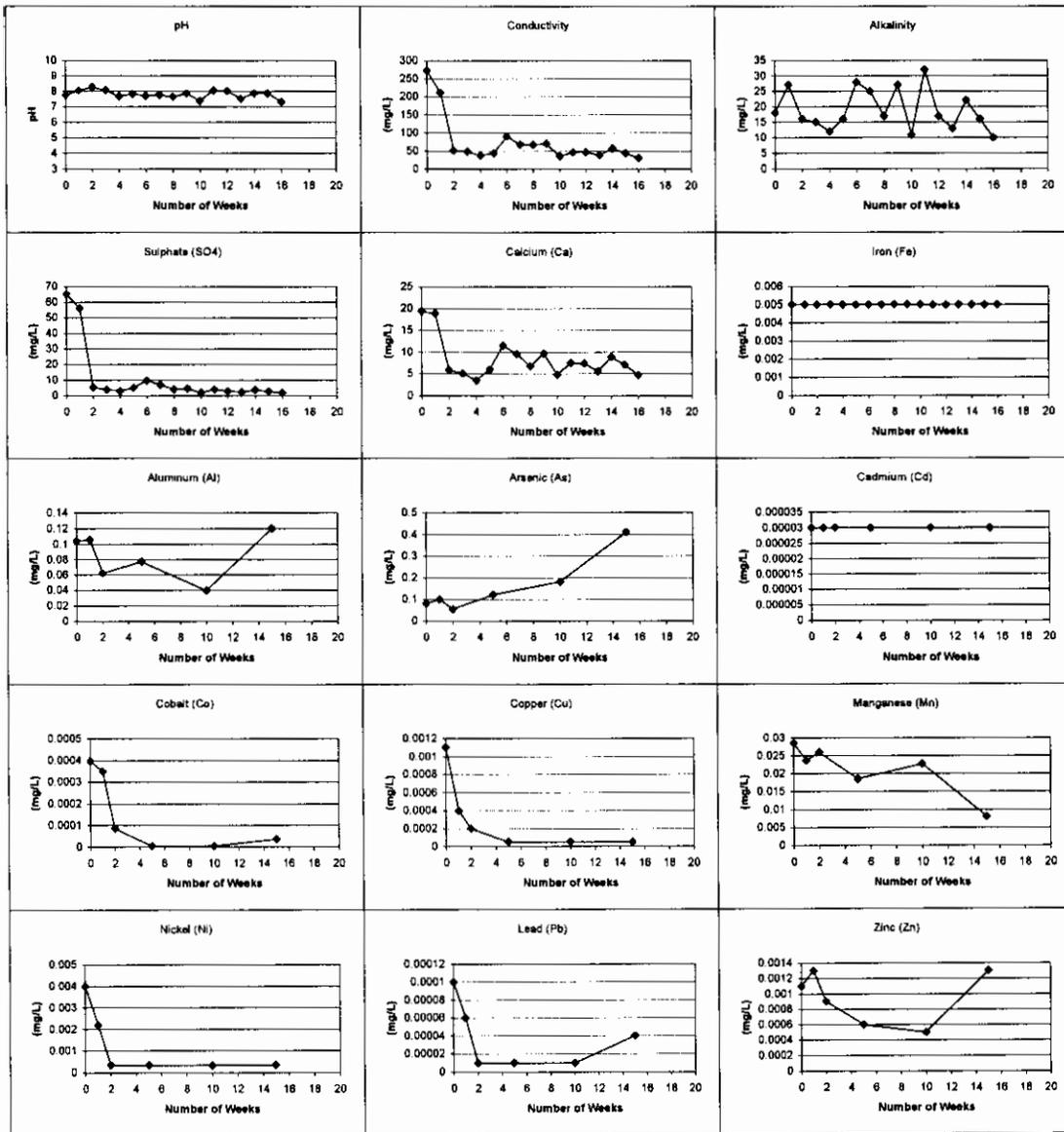
Golder Associates

FIGURE 10
 HUMIDITY CELL RESULTS FOR HC 06-012
 Argillite (5-49% Greywacke Interbeds)



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FIGURE 11
 HUMIDITY CELL RESULTS FOR HC 06-039
 Greywacke (20 - 50% Argillite interbeds)



Summary of Depletion Calculations from Humidity Cell Data

| Sample | Depletion Rate (mg/kg/wk) | | | Time to Depletion (years) | | |
|-----------|---------------------------|------|------|---------------------------|------|------|
| | Sulphide | NP | CaNP | Sulphide | NP | CaNP |
| CND2 | 6.1 | 27.9 | 20.7 | 2.9 | 14.3 | 18.4 |
| HC 06-006 | 1.2 | 17.6 | 14.8 | 27.7 | 35.4 | 31.4 |
| HC 06-012 | 0.4 | 8.0 | 6.4 | 39.9 | 99.1 | 95.3 |
| HC 06-017 | 0.6 | 14.8 | 13.8 | 9.8 | 25.7 | 21.1 |
| HC 06-039 | 0.9 | 22.6 | 21.7 | 102.3 | 27.3 | 43.8 |
| HC 06-049 | 1.3 | 20.9 | 19.6 | 32.5 | 26.3 | 24.3 |
| HC 06-051 | 2.3 | 24.0 | 23.1 | 11.5 | 23.0 | 20.2 |
| HC 06-068 | 0.9 | 22.8 | 21.8 | 15.8 | 29.9 | 22.6 |
| HC 06-070 | 0.9 | 8.0 | 7.5 | 76.7 | 66.5 | 53.6 |
| HC 06-079 | 1.8 | 16.4 | 13.2 | 54.8 | 33.1 | 47.1 |
| HC 06-085 | 2.6 | 12.4 | 11.5 | 15.8 | 43.5 | 34.3 |

Note: These values are for indicational purposes as they reflect laboratory conditions which differ greatly from field conditions.

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APPENDIX C
SAMPLE DISTRIBUTION ON
GEOLOGICAL SECTIONS

APPENDIX D
SGS LAKEFIELD (2006) WASTE ROCK
MINERALOGICAL REPORT

An Investigation into
**MINERALOGICAL CHARACTERIZATION OF FIVE WASTE
ROCK SAMPLES, TOUQUOY GEOCHEMISTRY PROGRAM**

prepared for
DDV GOLD

LR 11373-001 – M15020-AUG06
October 30, 2006

NOTE:

This report refers to the samples as received.

The practice of this Company in issuing reports of this nature is to require the recipient not to publish the report or any part thereof without the written consent of SGS Minerals Services.

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Introduction

Five waste rock samples (listed in Table 1 below) were submitted to Mineral Technologies for mineralogical examination. The purpose of the investigation was to determine the bulk mineral assemblage and textural characteristics of the mineral species within the sample. The sample was also investigated for its acid generation (AG) and/or neutralization potential (NP) based on the proportion of sulphide and carbonate minerals and their respective textural associations in each sample. The mineralogical examinations included X-ray diffraction analysis (XRD), optical microscopy, and scanning electron microscopy (SEM) equipped with an energy dispersive X-ray spectrometer (EDS).

Table 1. List of Samples

| | | Hole | From | To | Lithology | Lithology Description |
|--|--------|-----------|------|----|-----------|---|
| | 06-034 | MR-05-091 | 10 | 20 | G/A | Greywacke with 20-50% argillite |
| | | MR-05-122 | 10 | 20 | AR | Argillite (< 5% greywacke) |
| | 06-066 | MR-05-084 | 65 | 72 | GW | Greywacke with <20% argillite |
| | 06-070 | MR-05-083 | 68 | 75 | Comp | Composite GW/AR Argillite (< 5% greywacke) |

Stephanie Downing, M.Sc.
Project Mineralogist

Jou Zhou, M.Sc., P.Geo.
Group Leader, Mineral Technologies

Experimental work by: Krista Henderson, Section Preparator
Huxun Zhou, Ph.D., XRD Mineralogist
Report preparation by: Stephanie Downing, M.Sc., Project Mineralogist

Summary

Procedures

To ensure sample homogeneity, each as-received sample was initially screened at 16 mesh (1.2 mm), and the retained 16 mesh material was stage-crushed to passing 16 mesh and re-combined. A representative sub-sample of material was pulverized and submitted for X-ray diffraction (XRD) analysis, in order to determine the bulk crystalline mineral assemblage. XRD results are presented in Appendix 2.

One polished section and one polished thin section per sample were prepared from a representative sub-sample of -16 mesh material, as well as the original as-received material. Each polished section was examined optically with a petrographic microscope under incident (reflected) and transmitted light at 50x to 500x magnifications. The mineral assemblage and modal abundance of the sample were determined by compiling both optical data from manual point counting with a bulk mineral analysis (BMA) generated by Q_{unt}SCAN technology (results are presented in Table 2). Weight percentages of minerals were calculated from volume percentage using standard grain densities and documented mineral chemistries. A summary of the major calculated elemental oxides for each sample by mineralogical analysis is compared to the whole rock analysis (WRA) of each sample in assay reconciliation tables (presented in Appendix 1). The liberation characteristics of sulphide and carbonate minerals were determined by Q_{unt}SCAN analysis, where >95% of the target mineral from a line segment was considered liberated. For each sample, photomicrographs were taken to illustrate relevant textural and association data of the sulphide/carbonate minerals. Individual sample summaries including modal analysis, grain size, assay reconciliation, and photomicrographs are presented in Appendix

2. Mineralogical Results

2.1 Modal Analyses

Combined microscopic and SEM examination of the five waste rock samples indicate that they are composed primarily of silicates (varying between 85 and 92 wt. % amongst the samples). Minor amounts of carbonates (4.1 to 7.6 wt. %), sulphides (1.7 to 4.6 wt. %) and Fe-Ti oxides (1.0 to 1.9 wt. %) are also present, as well as trace amounts of sulphates (<0.2 wt. %) and phosphates (<0.3 wt. %). A summary of the bulk mineralogy of the five waste rock samples is presented below in Table 2.

Table 2. Summary modal analyses by optical/Q⁺SCAN analysis

| Mineral | Chemical composition | Sample | | | | |
|----------------------|--|--------------|--------------|--------------|--------------|--------------|
| | | WR1 | WR2 | WR3 | WR4 | WR5 |
| Quartz | SiO ₂ | 85.2 | 88.1 | 91.5 | 89.8 | 92.1 |
| Plagioclase feldspar | Al ₂ Si ₂ O ₇ (OH) ₄ | 1.2 | 1.5 | 1.8 | 1.4 | 1.6 |
| Microcline | KAlSi ₃ O ₈ | 0.5 | 0.6 | 0.7 | 0.5 | 0.6 |
| Orthoclase | KAlSi ₃ O ₈ | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Amphibole | (Ca,Mg,Fe)Si ₇ O ₂₂ (OH) ₂ | 0.3 | 0.4 | 0.5 | 0.3 | 0.4 |
| Pyrite | FeS ₂ | 1.7 | 2.1 | 2.5 | 1.8 | 2.2 |
| Chalcopyrite | CuFeS ₂ | 0.2 | 0.3 | 0.4 | 0.2 | 0.3 |
| Pyrrhotite | Fe ₇ S ₈ | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Carbonate | Ca(Mg,Fe)(CO ₃) ₂ | 4.1 | 5.2 | 6.3 | 4.5 | 5.6 |
| Iron oxide | Fe ₂ O ₃ | 1.0 | 1.2 | 1.4 | 1.1 | 1.3 |
| Titanium oxide | TiO ₂ | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Sulphate | CaSO ₄ | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| Phosphate | Ca ₃ (PO ₄) ₂ | 0.05 | 0.05 | 0.05 | 0.05 | 0.05 |
| Other | | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| Total | | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 |

Assay Reconciliation

In general, reconciliation of calculated mineralogical assay versus direct chemical assay is good, demonstrating confidence in mineralogical results (see reconciliation Tables in Appendix 1). Due to the coarse-grained nature of the sulphide minerals (200 µm up to 1 mm), a slight over-estimation of elemental sulphur by calculated mineralogical assay occurs due to this sulphide “nugget” effect. Similarly, carbonate minerals occur as large, coarse-grained clasts thus may be over-estimated due to a nugget particle effect. Documented mineral chemistries are used for mineralogical assay reconciliation tables for all minerals; therefore actual mineral chemistries will vary slightly from calculated ‘book’ values.

Quartz is the main silicate mineral present in all samples, ranging from 28 to 40 wt. % of sample, with the exception of samples 06-049 and 06-073, in which muscovite is either fairly equivalent in abundance to quartz (06-049) or predominates over quartz (06-073). Quartz appears to have a bi-modal distribution in grain size, occurring as both coarse blocky grains interstitial to fine-grained foliated particles (see Appendix 1, Figs. 8 and 19), and as fine grains, interstitial to foliated phyllosilicates consisting of muscovite and chlorite (A1, Fig.12).

Plagioclase feldspar predominates over K-feldspar, with the exception of samples 06-049 and 06-073, in which K-feldspar is predominant. SEM-EDS analysis of plagioclase shows a Na-rich end-member composition of albite for all samples. Feldspar grains typically occur together with quartz interstitial to phyllosilicates. K-feldspar commonly shows alteration to sericite and clay minerals among the samples.

Muscovite is the main phyllosilicate mineral present in all samples, followed by chlorite, both defining the foliation in the waste rock clasts (A1, Figs. 11 and 12). Muscovite commonly shows alteration to illite.

Other silicates that are present in trace proportions (typically < 0.2 wt. % of sample) include garnet, epidote, amphibole, pyroxene, talc and accessory zircon.

Magnetite, ilmenite and rutile are the main Fe- and Ti-oxide minerals present in all samples. The oxide minerals typically occur interstitial to silicate minerals within laminated particles (A1, Fig. 1).

Gypsum is the main sulphate mineral and occurs in trace amounts as attachments to silicate mineral particles. Rare Fe-sulphate is also present.

Phosphates

Trace amounts of apatite typically occur as fine inclusions within feldspar.

Carbonate minerals occur in minor amounts in all samples. Calcite is the main carbonate mineral among the five waste rock samples (ranging from 68% to 99% of total carbonate). Lesser amounts of dolomite and ankerite were also detected, as well as rare siderite. A complete breakdown of the carbonate mineral species, per sample basis, is presented in Table 3 below.

Table 3. Carbonate mineral species distribution

| Sample | Mineral | Sample 1 | | Sample 2 | | Sample 3 | | Sample 4 | | Sample 5 | |
|----------|---|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| | | Weight % | Volume % |
| Sample 1 | Ca(Fe,Mg,Mn)(CO ₃) _n | 68 | 78 | 72 | 82 | 75 | 85 | 78 | 88 | 82 | 92 |
| Sample 2 | Dolomite | 15 | 18 | 12 | 15 | 10 | 12 | 8 | 10 | 5 | 6 |
| Sample 3 | Ankerite | 5 | 6 | 3 | 4 | 2 | 3 | 1 | 2 | 1 | 1 |
| Sample 4 | Siderite | 1 | 1 | 0.5 | 0.5 | 0.2 | 0.2 | 0.1 | 0.1 | 0.1 | 0.1 |
| Sample 5 | Other | 11 | 13 | 16 | 19 | 18 | 21 | 20 | 24 | 10 | 12 |

Although the chemistry will dictate the carbonate neutralization potential (NP), its association will also have an impact on its availability for neutralization. In all samples, the majority of carbonates in the sample are typically liberated or exposed (ranging from 53% to 78%), and thus, are amenable to dissolution and neutralization. A lesser amount (22 to 47% among the samples

occur as locked inclusions, unavailable for neutralization. A graphical representation for those neutralizing minerals (calcite, dolomite and ankerite) is presented in Figure 1 below.

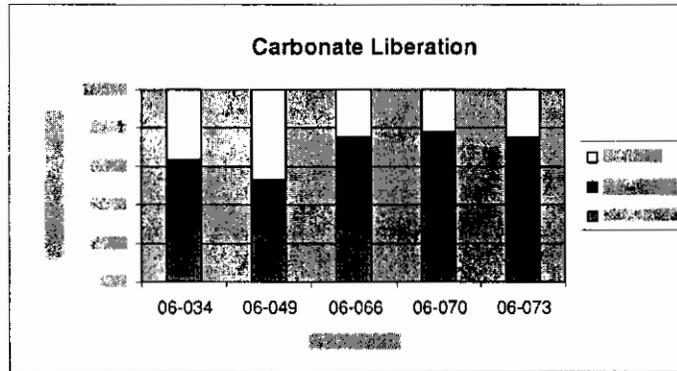


Figure 1. Carbonate association graph

Sulphides occur in minor proportions in all samples. The distribution of sulphide minerals varies across all samples. Pyrite is the most abundant sulphide mineral present in sample 06-070 (98% of total sulphides). Arsenopyrite is the most abundant sulphide mineral in samples 06-034 (87% of total sulphides) and 06-066 (58% of total sulphides). In sample 06-049, pyrrhotite is the predominant sulphide (40% of total sulphides) followed by arsenopyrite (36% of total sulphides) and pyrite (24% of total sulphides). In sample 06-073, pyrite and arsenopyrite are the predominant sulphides showing 44% and 42% distribution of the sulphides among the samples, respectively. A complete breakdown of the sulphide mineral speciation is presented in Table 4

Table 4. Sulphide mineral species distribution

| Sample | Total Sulphide (%) | Pyrite | | Arsenopyrite | | Pyrrhotite | | Chalcopyrite | | Other | |
|--------|--------------------|--------|------------|--------------|------------|------------|------------|--------------|------------|-------|------------|
| | | wt% | % of Total | wt% | % of Total | wt% | % of Total | wt% | % of Total | wt% | % of Total |
| 06-034 | 100 | 87 | 87 | 13 | 13 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06-049 | 100 | 24 | 24 | 36 | 36 | 40 | 40 | 0 | 0 | 0 | 0 |
| 06-066 | 100 | 0 | 0 | 58 | 58 | 42 | 42 | 0 | 0 | 0 | 0 |
| 06-070 | 100 | 98 | 98 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06-073 | 100 | 44 | 44 | 42 | 42 | 14 | 14 | 0 | 0 | 0 | 0 |

As pyrite, pyrrhotite and arsenopyrite minerals may all contribute to acidity under oxidizing conditions, their textural associations were examined in detail. Pyrite typically shows high degrees of locking, with over half (50% to 80%) among all samples locked within silicate particles. Figure 2 shows a summary association graph for pyrite among the samples.

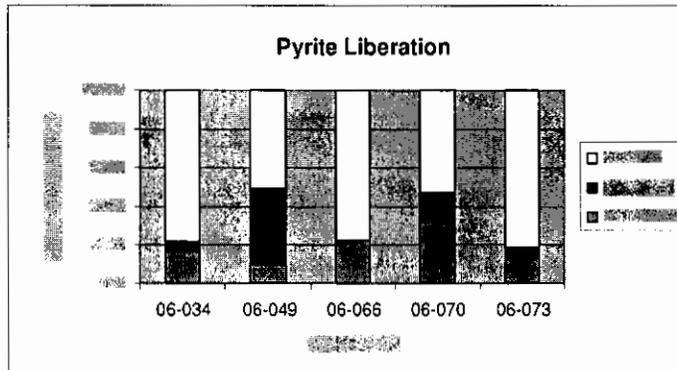


Figure 2. Pyrite association graph

Pyrrhotite typically occurs as locked (50 to 100% of total pyrrhotite) or exposed grains (01 to 50% of total pyrrhotite), with only trace amounts as liberated grains (< 1% of total pyrrhotite). Figure 3 shows the association of pyrrhotite among the samples.

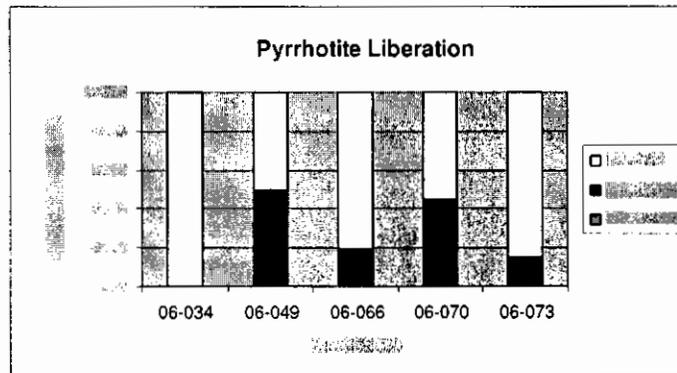


Figure 3. Pyrrhotite association graph

In comparison, arsenopyrite commonly occurs as large liberated grains (46% to 100% liberated). Only minor proportions occur locked (0% to 26%). Figure 4 shows the association of arsenopyrite among the samples.

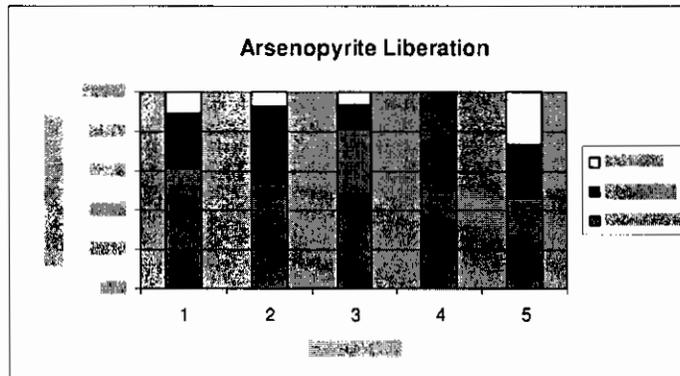


Figure 4. Arsenopyrite association graph

Summary of Sulphide and Carbonate Minerals

A summary of the sulphide and carbonate mineral species is presented in Table 5 below.

Table 5. Summary of carbonate and sulphide minerals by sample

| Sample | Mineral | Sample 1 | | Sample 2 | | Sample 3 | | Sample 4 | | Sample 5 | |
|----------|----------|----------|-------|----------|-------|----------|-------|----------|-------|----------|-------|
| | | wt. % | wt. % |
| Sample 1 | Calcite | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 |
| | Dolomite | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 |
| | Ankerite | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 |
| Sample 2 | Calcite | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 |
| | Dolomite | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 |
| | Ankerite | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 |
| Sample 3 | Calcite | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 |
| | Dolomite | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 |
| | Ankerite | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 |
| Sample 4 | Calcite | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 |
| | Dolomite | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 |
| | Ankerite | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 |
| Sample 5 | Calcite | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 | ~80 |
| | Dolomite | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 | ~15 |
| | Ankerite | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 | ~5 |

The carbonate mineralogy consists mainly of Ca-rich carbonates (calcite, dolomite, and ankerite) which provide the highest degree of neutralization among the carbonate minerals. These carbonate minerals also show a high degree of availability, suggesting a large neutralizing source. Only a minor amount of siderite or Fe-carbonate (< 0.5 wt. % distribution) is found among the samples.

Among the samples, a high proportion of pyrite and pyrrhotite show locking characteristics, typically occurring as inclusions or attachments to silicate mineral particles. This textural association suggests they will not contribute to any significant AG due to their encapsulation. Alternatively, arsenopyrite (the only As-bearing mineral among the samples) shows a high degree of liberation (> 50% up to 99%) among the samples.

4. Conclusions

- Among each waste rock sample examined, there is a higher proportion of carbonate minerals to sulphide minerals. The carbonate to sulphide ratio varies from 1.2 to 2.4 among the waste rocks (see Table 6 below). The carbonate associations as mainly exposed or liberated grains (53% to 78% of total carbonates) suggest there may be sufficient NP among these samples to react with any acidity generated by the oxidation of Fe-bearing sulphides.

Table 6. Summary of carbonate/sulphide mineral content and mineralogical NP

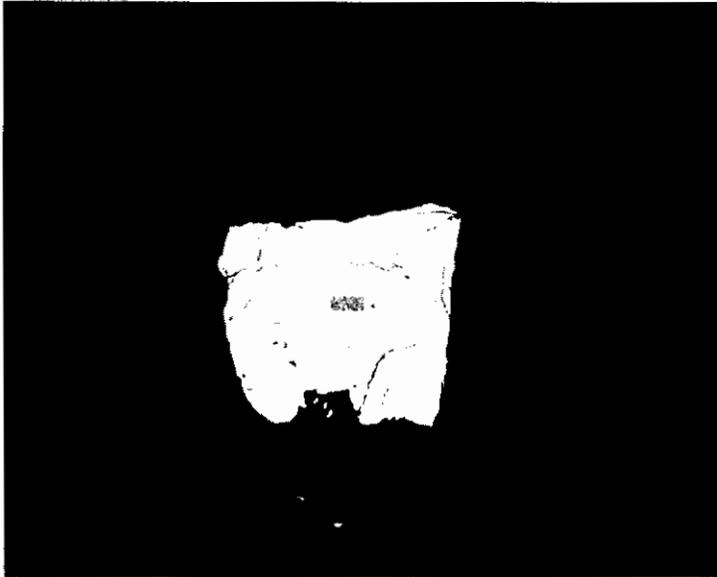
| Sample | 06-034 | 06-049 | 06-066 | 06-070 | 06-073 |
|--------------------------|--------|--------|--------|--------|--------|
| AGP from Sulphide | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Carbonate/Sulphide ratio | 2.4 | 1.7 | 1.5 | 1.2 | 1.3 |

NP (Neutralization Potential), AGP (Acid Generation)

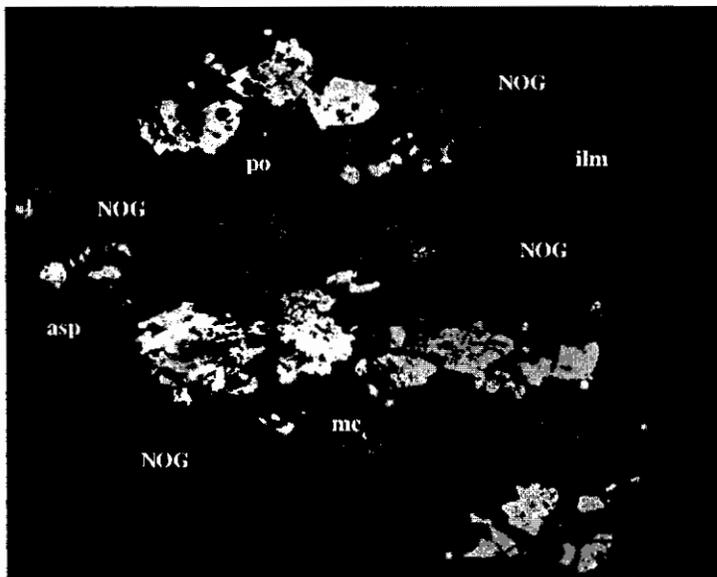
Note: total carbonate values exclude siderite which does not contribute to NP, and all values are disrespective of sulphide/carbonate liberation

- Samples showing carbonate/sulphide ratios >2 (06-034 and 06-066) indicate probable net acid neutralizing conditions. Those samples with ratios between 1 and 2 (06-049, 06-070, and 06-073) also suggest possible neutralizing conditions due to their textural associations among the samples.
- The large grain size and liberated nature of arsenopyrite in samples 06-049, 06-066 and 06-073, coupled with their lower carbonate/sulphide ratios, may indicate a possible concern in highly oxidizing environments for heavy metal contamination (i.e. arsenic).

Appendix 1
Mineralogical Results by Individual Sample

Photomicrographs: 06-034**Figure 5. Sample 06-034 photomicrograph**

Low magnification reflected light (RL) photomicrograph showing a large (~1.0 mm) liberated arsenopyrite grain surrounded by non-opaque minerals

**Figure 6. Sample 06-034 photomicrograph**

Low magnification reflected light (RL) photomicrograph showing abundant sulphides (pyrite and/or marcasite (mc), pyrrhotite (po) and arsenopyrite (asp)) and ilmenite (ilm) as inclusions in silicate non-opaque minerals

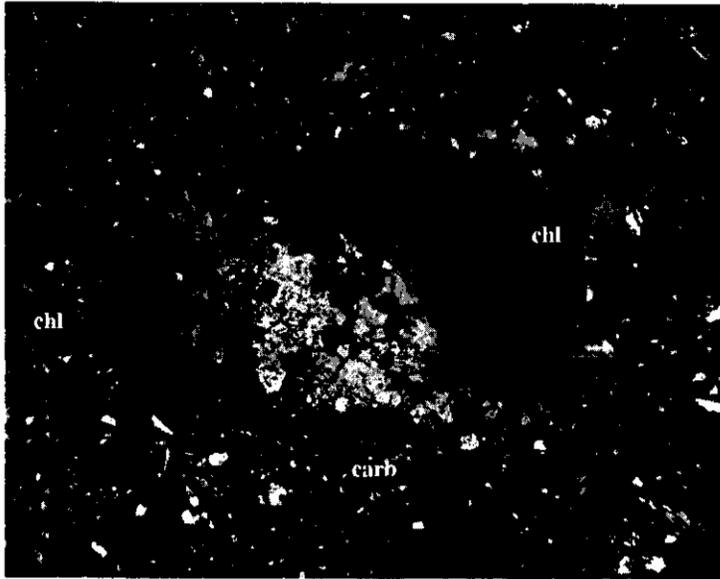


Figure 7. Sample 06-034 photomicrograph

Low magnification transmitted light (RL) photomicrograph showing a large aggregate composed of carbonate (carb) intergrown with chlorite (chl).

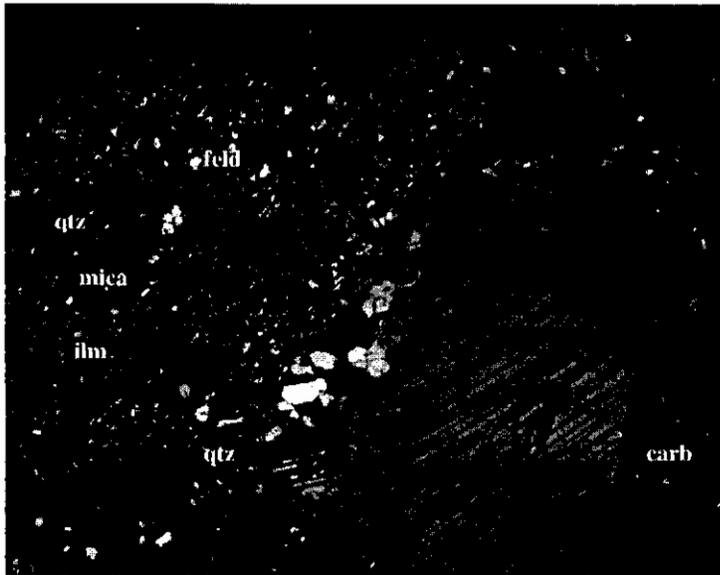


Figure 8. Sample 06-034 photomicrograph

Low magnification reflected light (RL) photomicrograph showing a large grain of carbonate (~ 1.0 mm) exposed and attached to a foliated argillite-type clast composed of quartz, feldspar, micas and Fe-Ti oxides. Note the blocky quartz at the contact between the carbonate

Table 9. Modal abundance and average grain size of sample 06-049

| 06-049 | Formula or chemical composition | wt % | |
|--------|---|------|--|
| | SiO ₂ | | |
| | Al ₂ SiO ₅ | | |
| | Al ₂ Si ₂ O ₇ | | |
| | Al ₂ Si ₄ O ₁₁ | | |
| | Al ₂ Si ₆ O ₁₅ | | |
| | Al ₂ Si ₈ O ₂₁ | | |
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| | Al ₂ Si ₃₉₂ O ₁₁₇₁ | | |
| | Al ₂ Si ₃₉₄ O ₁₁₇₇ | | |
| | Al ₂ Si ₃₉₆ O ₁₁₈₃ | | |
| | Al ₂ Si ₃₉₈ O ₁₁₈₉ | | |
| | Al ₂ Si ₄₀₀ O ₁₁₉₅ | | |
| | Al ₂ Si ₄₀₂ O ₁₂₀₁ | | |
| | Al ₂ Si ₄₀₄ O ₁₂₀₇ | | |
| | Al ₂ Si ₄₀₆ O ₁₂₁₃ | | |
| | Al ₂ Si ₄₀₈ O ₁₂₁₉ | | |
| | Al ₂ Si ₄₁₀ O ₁₂₂₅ | | |
| | Al ₂ Si ₄₁₂ O ₁₂₃₁ | | |
| | Al ₂ Si ₄₁₄ O ₁₂₃₇ | | |
| | Al ₂ Si ₄₁₆ O ₁₂₄₃ | | |
| | Al ₂ Si ₄₁₈ O ₁₂₄₉ | | |
| | Al ₂ Si ₄₂₀ O ₁₂₅₅ | | |
| | Al ₂ Si ₄₂₂ O ₁₂₆₁ | | |
| | Al ₂ Si ₄₂₄ O ₁₂₆₇ | | |
| | Al ₂ Si ₄₂₆ O ₁₂₇₃ | | |
| | Al ₂ Si ₄₂₈ O ₁₂₇₉ | | |
| | Al ₂ Si ₄₃₀ O ₁₂₈₅ | | |
| | Al ₂ Si ₄₃₂ O ₁₂₉₁ | | |
| | Al ₂ Si ₄₃₄ O ₁₂₉₇ | | |
| | Al ₂ Si ₄₃₆ O ₁₃₀₃ | | |
| | Al ₂ Si ₄₃₈ O ₁₃₀₉ | | |
| | Al ₂ Si ₄₄₀ O ₁₃₁₅ | | |
| | Al ₂ Si ₄₄₂ O ₁₃₂₁ | | |
| | Al ₂ Si ₄₄₄ O ₁₃₂₇ | | |
| | Al ₂ Si ₄₄₆ O ₁₃₃₃ | | |
| | Al ₂ Si ₄₄₈ O | | |



Photomicrographs: 06-049

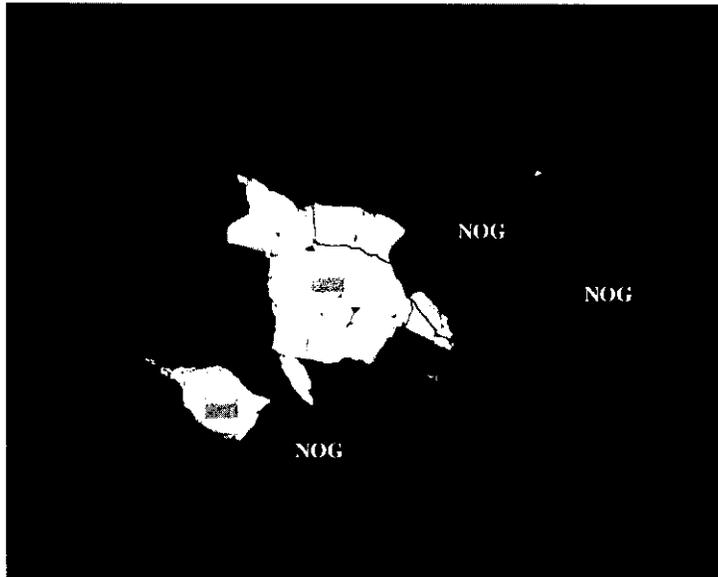


Figure 9. Sample 06-049 photomicrograph

Reflected light (RL) photomicrograph showing liberated grains of arsenopyrite (asp).



Figure 10. Sample 06-049 photomicrograph

Reflected light (RL) photomicrograph showing pyrrhotite (po) intergrown with silicates (indicated by arrows), showing parti

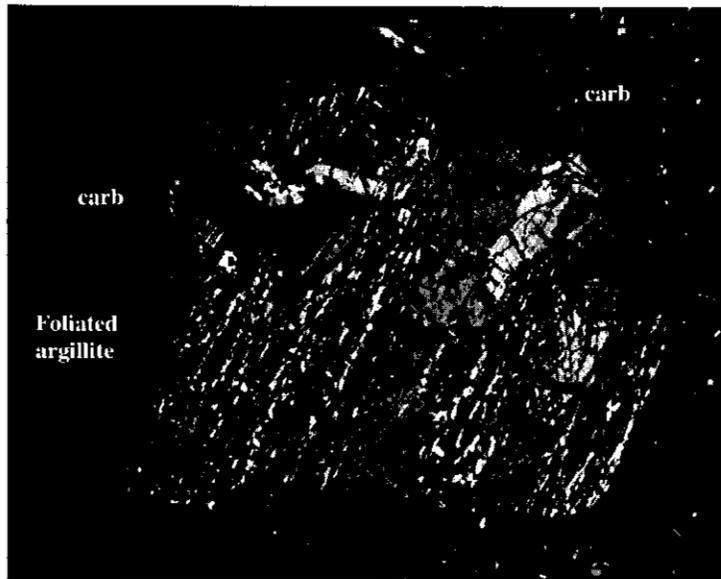


Figure 11. Sample 06-049 photomicrograph

Transmitted light (TL) photomicrograph showing blocky carbonate particles interstitial to foliated argillite-type particles.

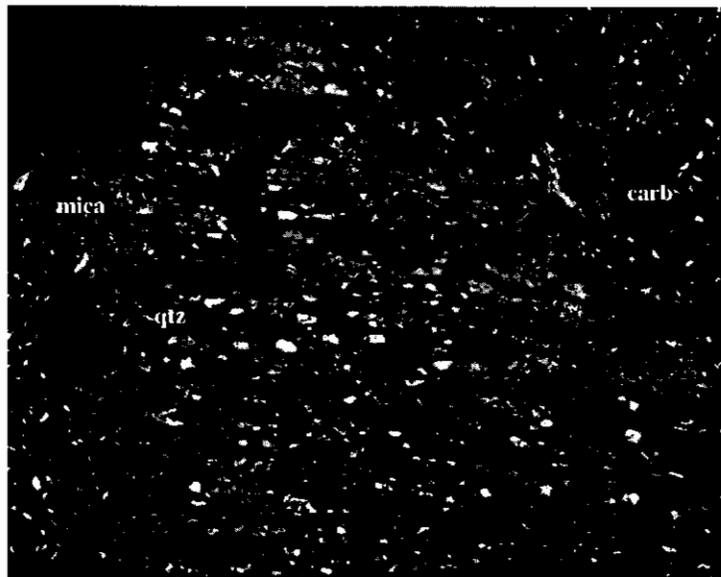


Figure 12. Sample 06-049 photomicrograph

TL photomicrograph (crossed polars) showing a carbonate-rich particle. Carbonate appears to be veining, showing parallel laminae interstitial to micas, quartz and feldspar.

Photomicrographs: 06-066



Figure 13. Sample 06-066 photomicrograph

Reflected light (RL) photomicrograph showing a liberated grain of arsenopyrite (asp).



Figure 14. Sample 06-066 photomicrograph

RL photomicrograph showing exposed and liberated grains of pyrite (py), pyrrothite (po) and arsenopyrite (asp).

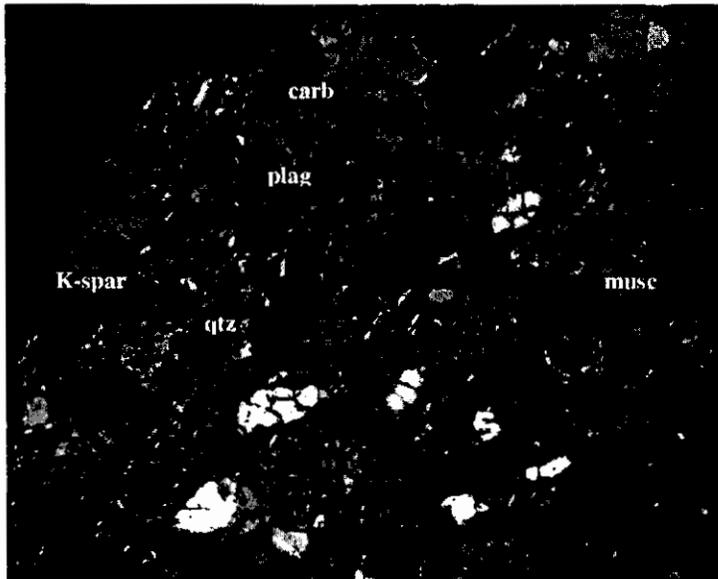


Figure 15. Sample 06-066 photomicrograph

Transmitted light (TL) photomicrograph showing a carbonate-rich particle composed of plagioclase feldspar (plag), K-feldspar (K-spar), muscovite (musc), quartz (qtz) and carbonates (carb).

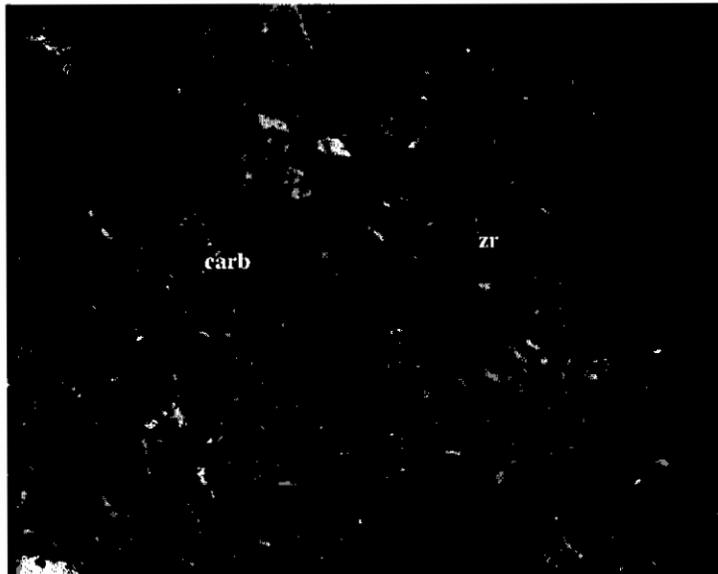


Figure 16. Sample 06-066 photomicrograph

High magnification (TL) photomicrograph showing a zircon inclusion (zr) within carbonate matrix (carb).

Photomicrographs: 06-070



Figure 17. Sample 06-070 photomicrograph

Reflected light (RL) photomicrograph showing both attached (exposed) and liberated pyrite with silicate mineral (dark grey).

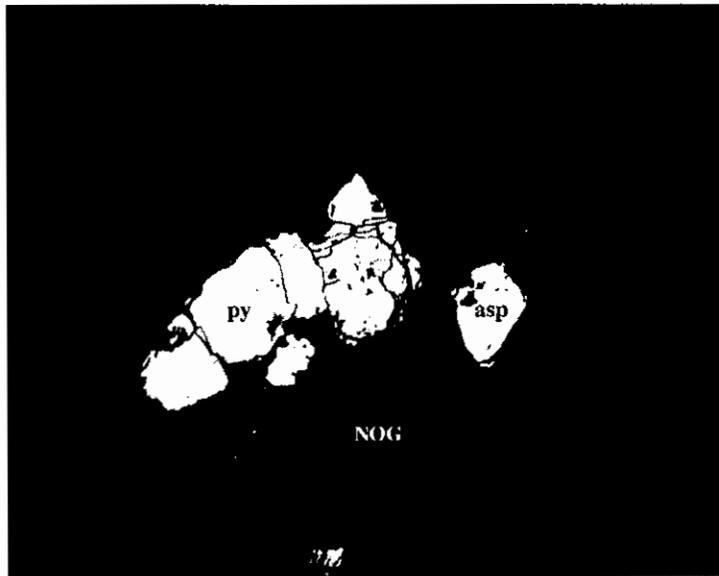


Figure 18. Sample 06-070 photomicrograph

RL photomicrograph showing exposed and liberated grains of pyrite (py) and arsenopyrite (asp).

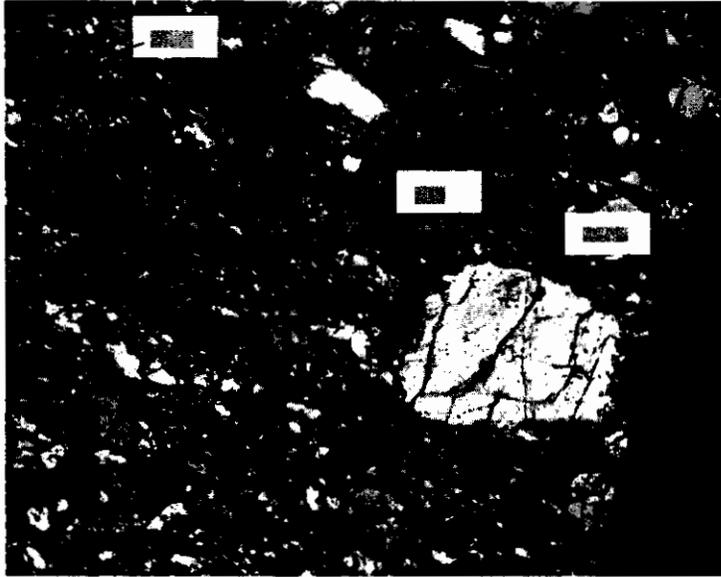


Figure 19. Sample 06-070 photomicrograph

Transmitted light (crossed polars) photomicrograph showing a carbonate-rich particle. Carbonate occurs as veinlets interstitial to silicates, and large exposed grains within this particle.

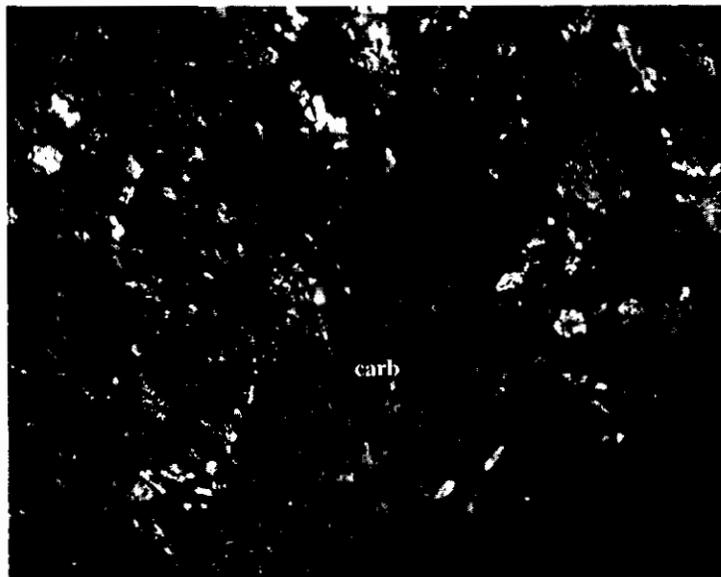


Figure 20. Sample 06-070 photomicrograph

TL photomicrograph (crossed polars) showing an exposed carbonate grain.

Photomicrographs: 06-073

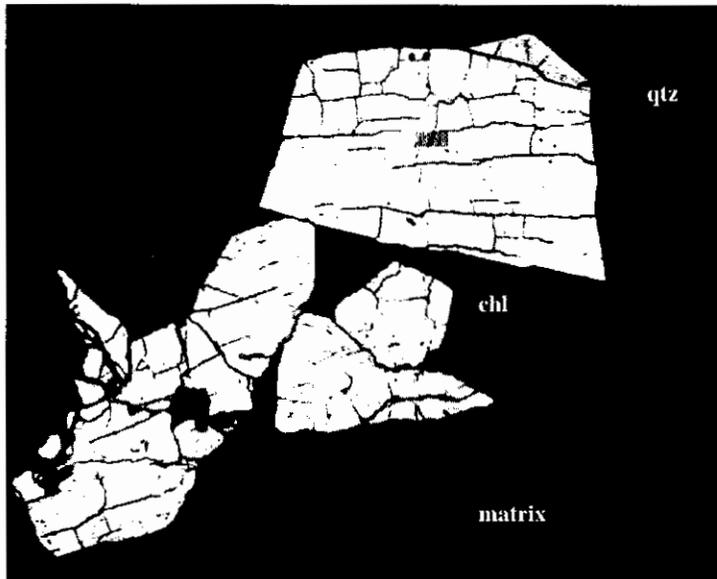


Figure 21. Sample 06-073 photomicrograph

Reflected light (RL) photomicrograph showing large arsenopyrite (asp) with halos of quartz and chlorite within a fine-grained matrix of phyllite-type host rock.



Figure 22. Sample 06-073 photomicrograph

RL photomicrograph showing a liberated coarse grain of pyrite (py) altering to marcasite (mc), showing inclusions of non-opaque gangue minerals (dark).

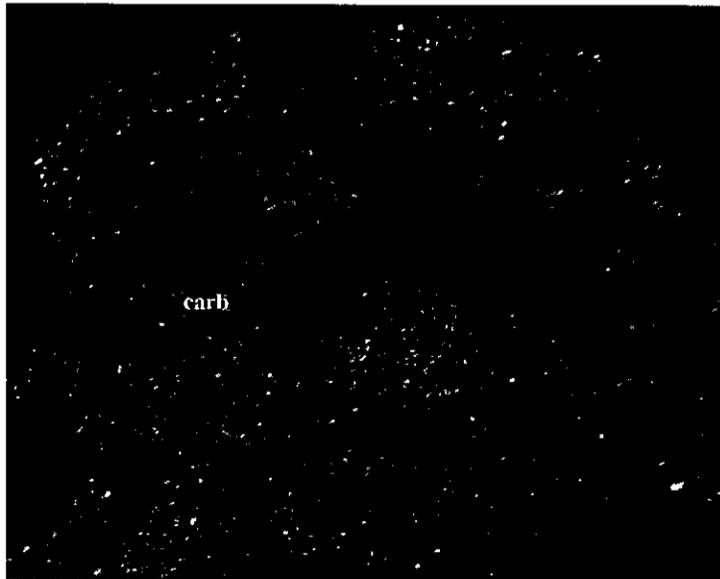


Figure 23. Sample 06-073 photomicrograph

Transmitted light (crossed polars) photomicrograph showing large carbonate (carb) clasts held within a phyllite-type host rock.

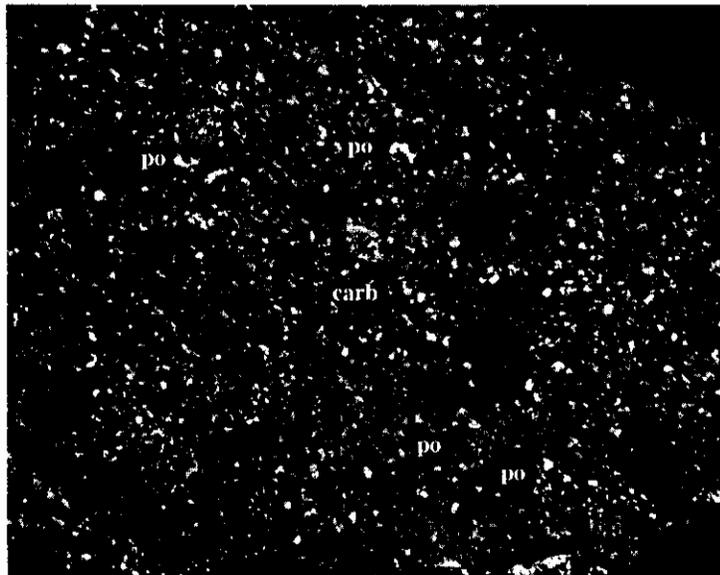


Figure 24. Sample 06-073 photomicrograph

TL photomicrograph (crossed polars) showing a carbonate-rich particle hosting inclusions of pyrrhotite.



Appendix 2
X-ray Diffraction Results

Summary of Qualitative X-ray Diffraction Results

| Sample | Crystalline Mineral Assemblage (relative proportions based on peak height) | | | |
|--------|--|--------------------------------------|-------------------|---|
| | Major | Moderate | Minor | Trace |
| | quartz | plagioclase-feldspar, mica, chlorite | calcite | *rectorite, *mordenite, *pyroxene |
| | quartz | mica, chlorite, plagioclase-feldspar | calcite | *rectorite, *mordenite, *pyroxene |
| | quartz | plagioclase-feldspar, mica, chlorite | calcite | *rectorite, *amphibole, *mordenite, *pyroxene |
| | quartz | mica, chlorite, plagioclase-feldspar | | *calcite, *rectorite, *mordenite, *pyroxene |
| | quartz | mica, chlorite, plagioclase-feldspar | calcite, ankerite | *pyrite, *pyroxene |

*Tentative identification due to low concentrations, diffraction line overlap or poor crystallinity

Instrument: Siemens D5000 diffractometer

Scan Conditions: Co radiation, graphite monochromator, 40 kV, 30 mA, Step:0.02°, Step time:1s

Interpretations: JCPDS / ICDD powder diffraction files. Siemens Search / Match software.

Detection Limit: 0.5-2%. Strongly dependent on crystallinity

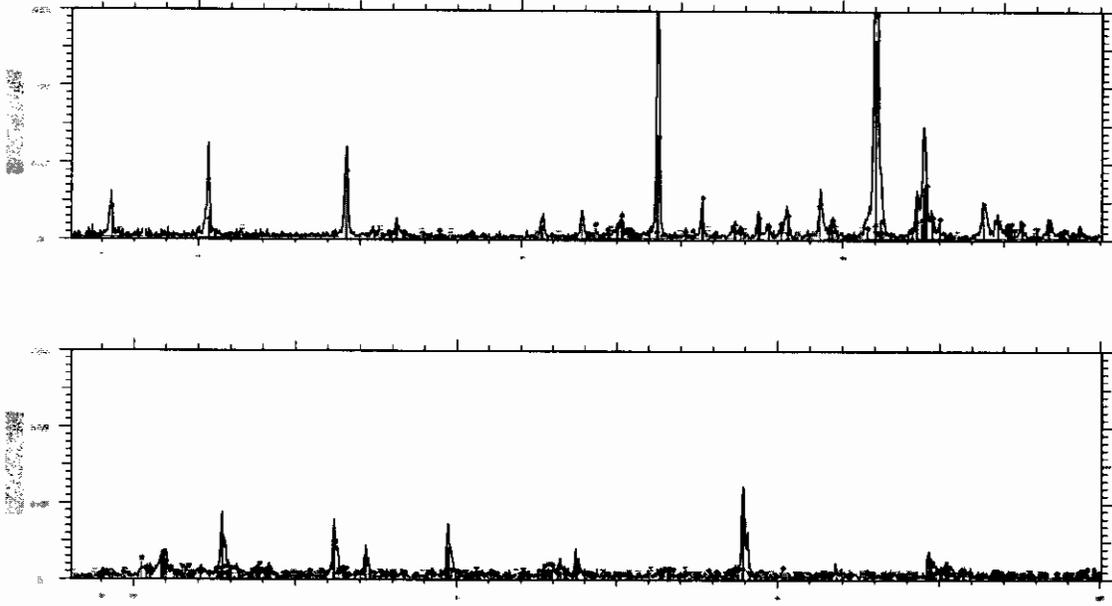
Interpretations do not reflect the presence of non-crystalline / amorphous compounds. Mineral proportions on relative peak heights and may be strongly influenced by crystallinity, structural group or preference

Interpretations and relative proportions should be accompanied by supporting petrographic and geochemical data (WRA, ICP-OES).

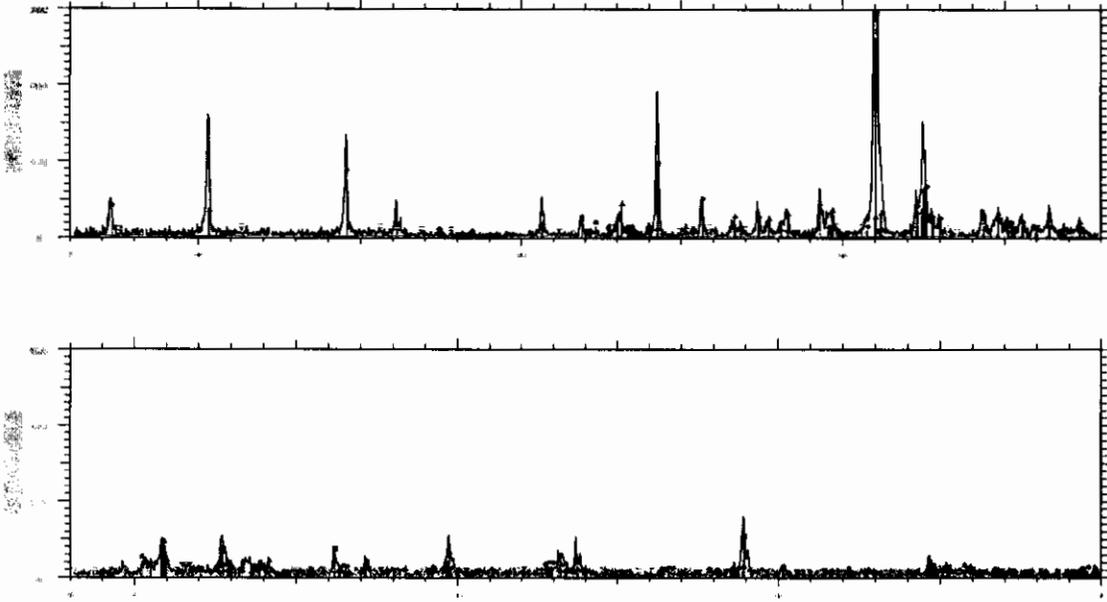
| | |
|----------------------|--|
| Amphibole | (Na,K)Ca ₂ (Mg,Fe)Si ₇ O ₂₂ (OH) ₂ |
| Ankerite | CaFe(CO ₃) ₂ |
| Calcite | CaCO ₃ |
| Chlorite | (Fe,Mg,Mn)Al ₂ (OH) ₂ Si ₄ O ₁₀ |
| Mica | K(Mg,Fe)Al ₃ (OH) ₂ Si ₃ O ₁₀ |
| Mordenite | (Ca, Na)Al ₃ Si ₆ O ₁₄ (OH) ₂ |
| Plagioclase-Feldspar | (NaSi,CaAl)AlSi ₃ O ₈ |
| Pyrite | FeS ₂ |
| Pyroxene | (Ca,Na)(Mg,Fe,Al,Ti)(Si,Al) ₂ O ₆ |
| Quartz | SiO ₂ |
| Rectorite | Na-Ca-K-Al-Si-OH-3H ₂ O |

Huyun Zhou, Ph.D.

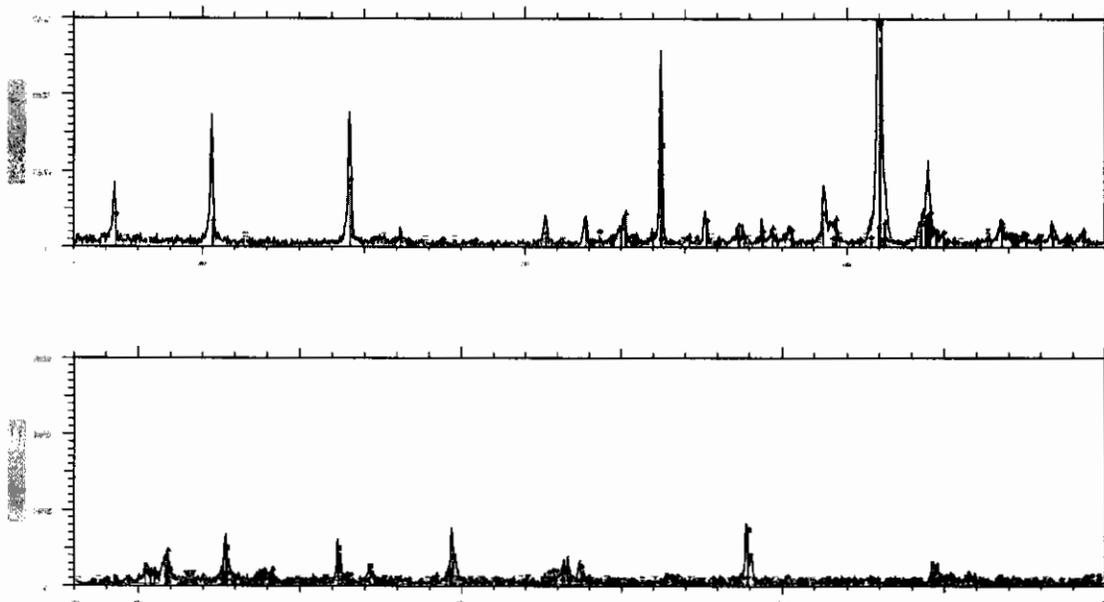
Stephanie Downing, M. Sc.
Project Mineralogist



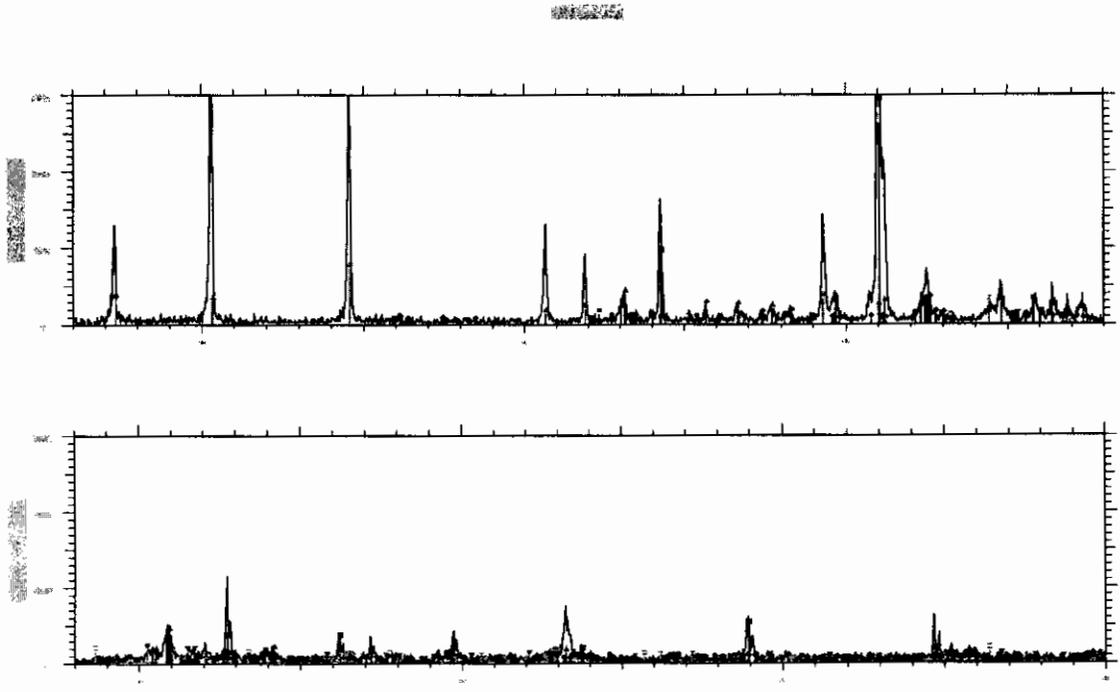
- 06-034 - File: Aug5020-1.raw - Type: 2Th/Th locked 20250147-140009 14-0183 (D) - Rectorite - Na-Ca-K-Al-Si-OH-3H2O
- 06-035 - File: Aug5020-1.raw - Type: 2Th/Th locked 20250147-140009 14-0183 (D) - Rectorite - Na-Ca-K-Al-Si-OH-3H2O
- 85-2153 (C) - Chamosite - (Mg5.036Fe4.964)Al2.724(Si2.000O10(OH)2)
- 83-0104 (C) - Pyroxene - (Mg0.962Fe0.038)(Ca0.999Mg0.001)Si2O6
- 84-1302 (C) - Muscovite - KA3Si3O10(OH)2
- 06-0240 (D) - Mordenite - (Ca.Na2.K2)Al2Si10O24.7H2O



- 06-066 - File: Aug5020-3 RAW - Type: 2Th/Th locked
- 14-0183 (D) - Rectorite - Na-Ca-K-Al-Si-OH-3H2O
- 071-1060 (C) - Homblende - Na.9K.4Ca1.6Mg2.9Fe1.4T
- 65-2163 (C) - Chamosite - (Mg5.036Fe4.964)Al2.724(Si
- 84-1302 (C) - Muscovite - KAl3Si3O10(OH)2
- 83-0104 (C) - Pyroxene - (Mg0.962Fe0.038)(Ca0.999Mg
- 06-0240 (D) - Mordenite - (Ca.Na2.K2)Al2Si10O24.7H2O

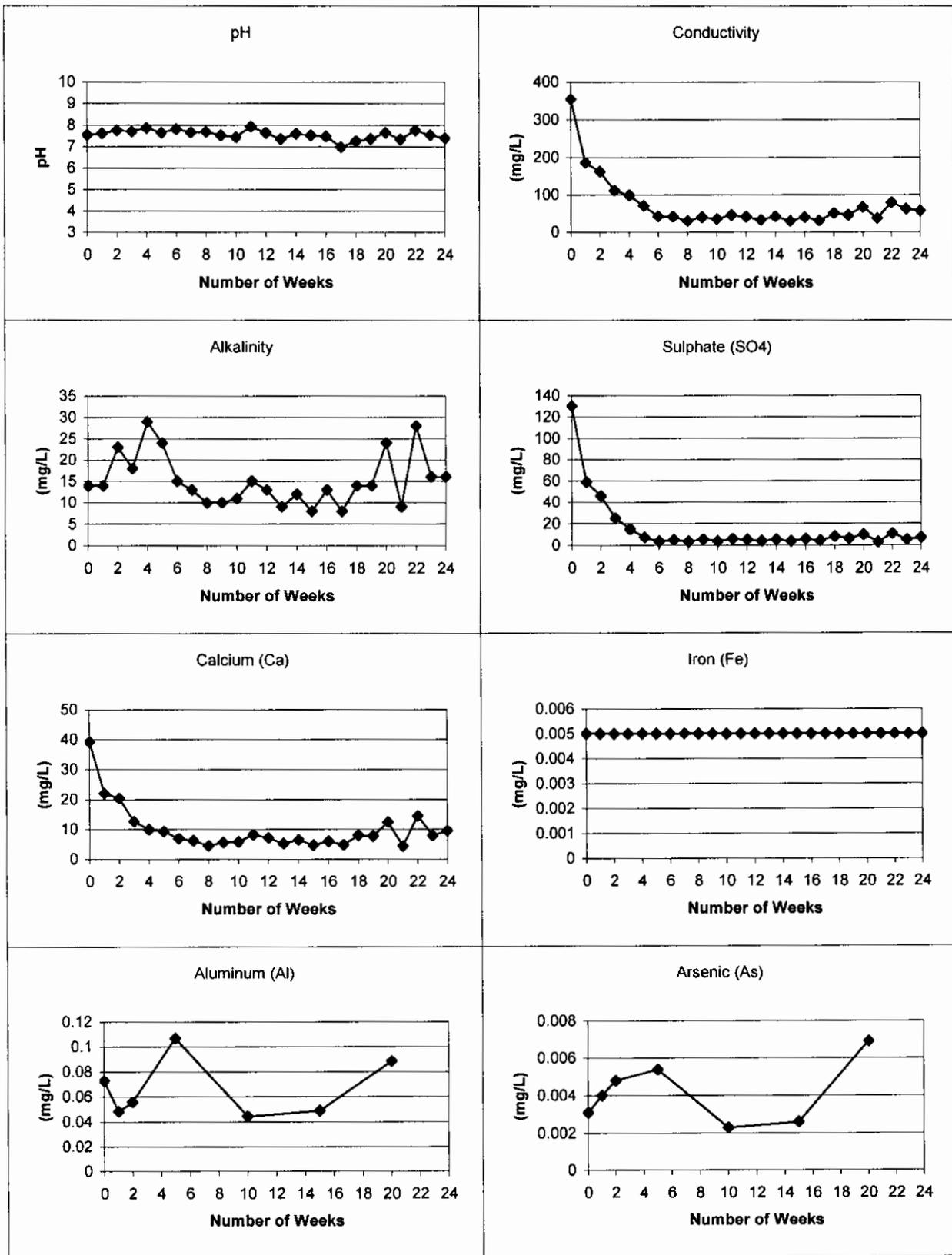


- 06-070 - File: aug5020-4.raw - Type: ZrTh locked 14-0183 (D) - Rectorite - Na-Ca-K-Al-Si-OH-3H2O
- 85-2163 (C) - Chamosite - (Mg5.036Fe4.964)Al2.724(Si10.276O32)2(OH)2
- 84-1302 (C) - Muscovite - KAl3Si3O10(OH)2
- 83-0104 (C) - Pyroxene - (Mg0.962Fe0.038)(Ca0.999Mg0.001)Si2O6
- 06-0240 (D) - Mordenite - (Ca,Na2,K2)Al2Si10O24·7H2O



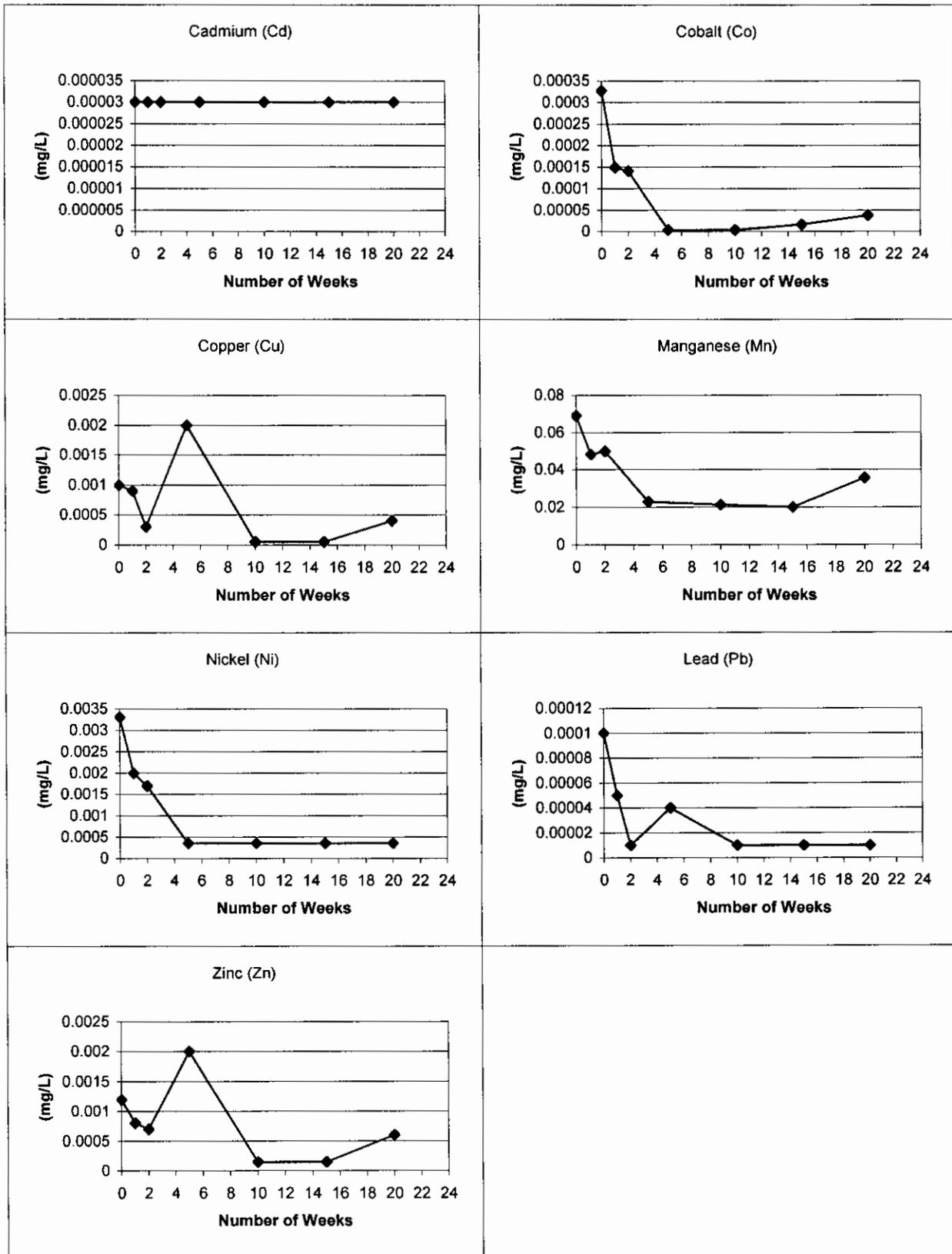
- 06-073 - File: Aug5020-5 RAW - Type: 2ThTh locked
- 85-2163 (C) - Chamosite - $(Mg_{5.036}Fe_{4.964})Al_2Si_2O_{10}(OH)_2$
 - 85-0104 (C) - Pyroxene - $(Mg_{0.962}Fe_{0.038})(Ca_{0.999}Mg_{0.001})Si_2O_6$
 - 64-1302 (C) - Muscovite - $KAl_3Si_3O_{10}(OH)_2$
 - 79-1347 (C) - Ankerite - $Ca_{0.997}(Mg_{0.273}Fe_{0.676}Mn_{0.054})CO_3$

FIGURE 12a
HUMIDITY CELL RESULTS FOR HC 06-051
Composite Material



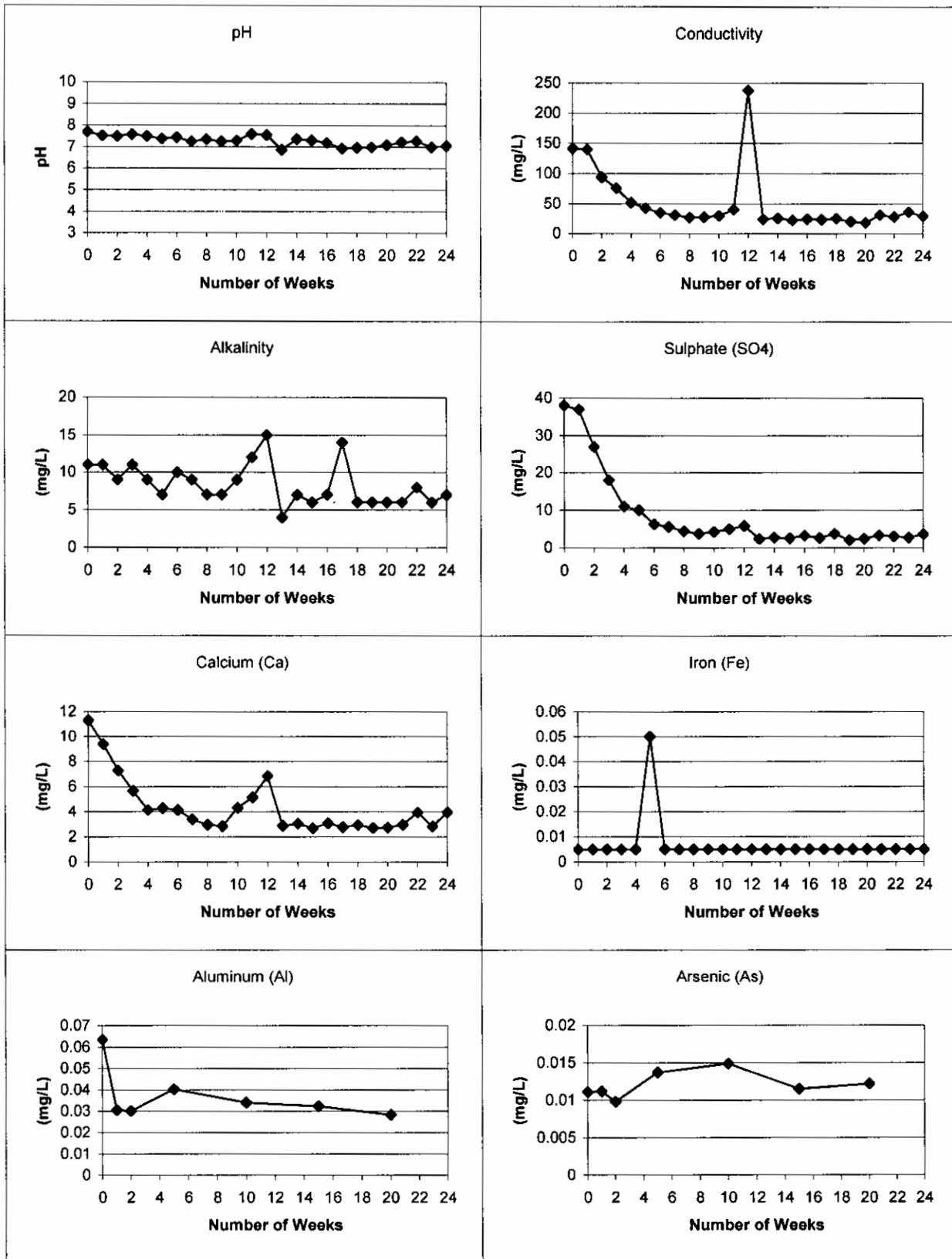
Golder Associates

FIGURE 12a
HUMIDITY CELL RESULTS FOR HC 06-051
Composite Material



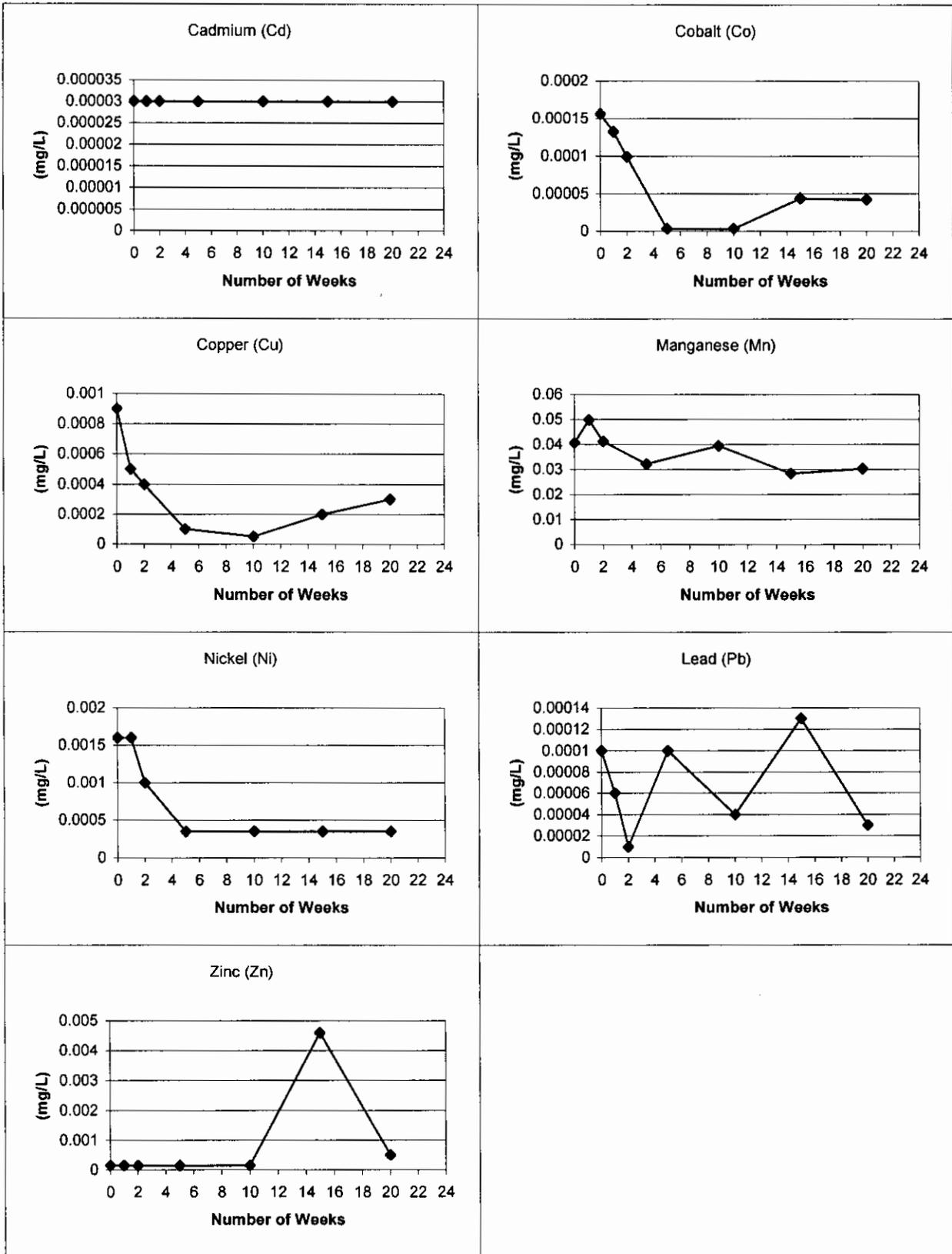
Golder Associates

FIGURE 12b
HUMIDITY CELL RESULTS FOR HC 06-070
Composite Sample



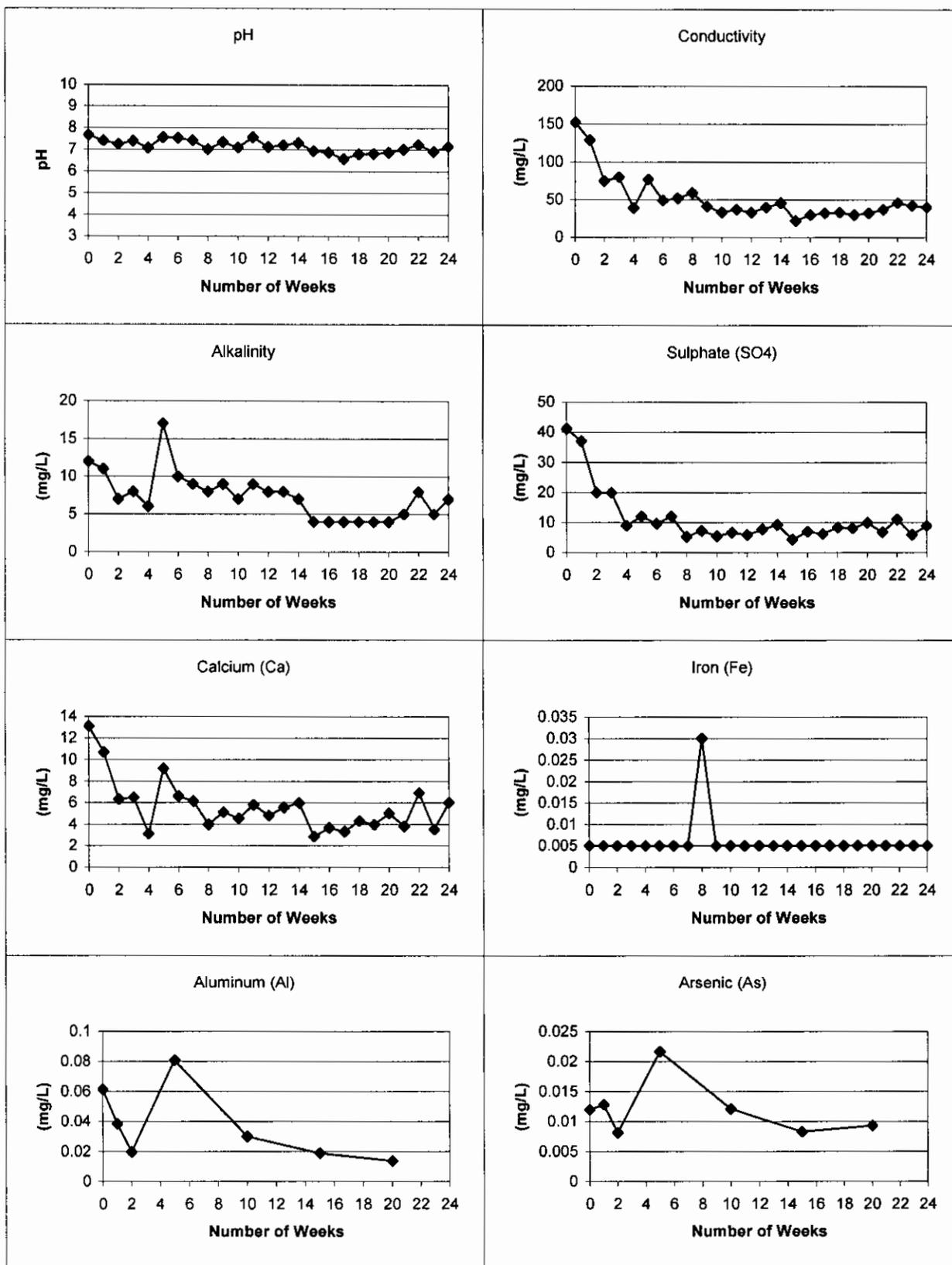
Golder Associates

FIGURE 12b
HUMIDITY CELL RESULTS FOR HC 06-070
Composite Sample



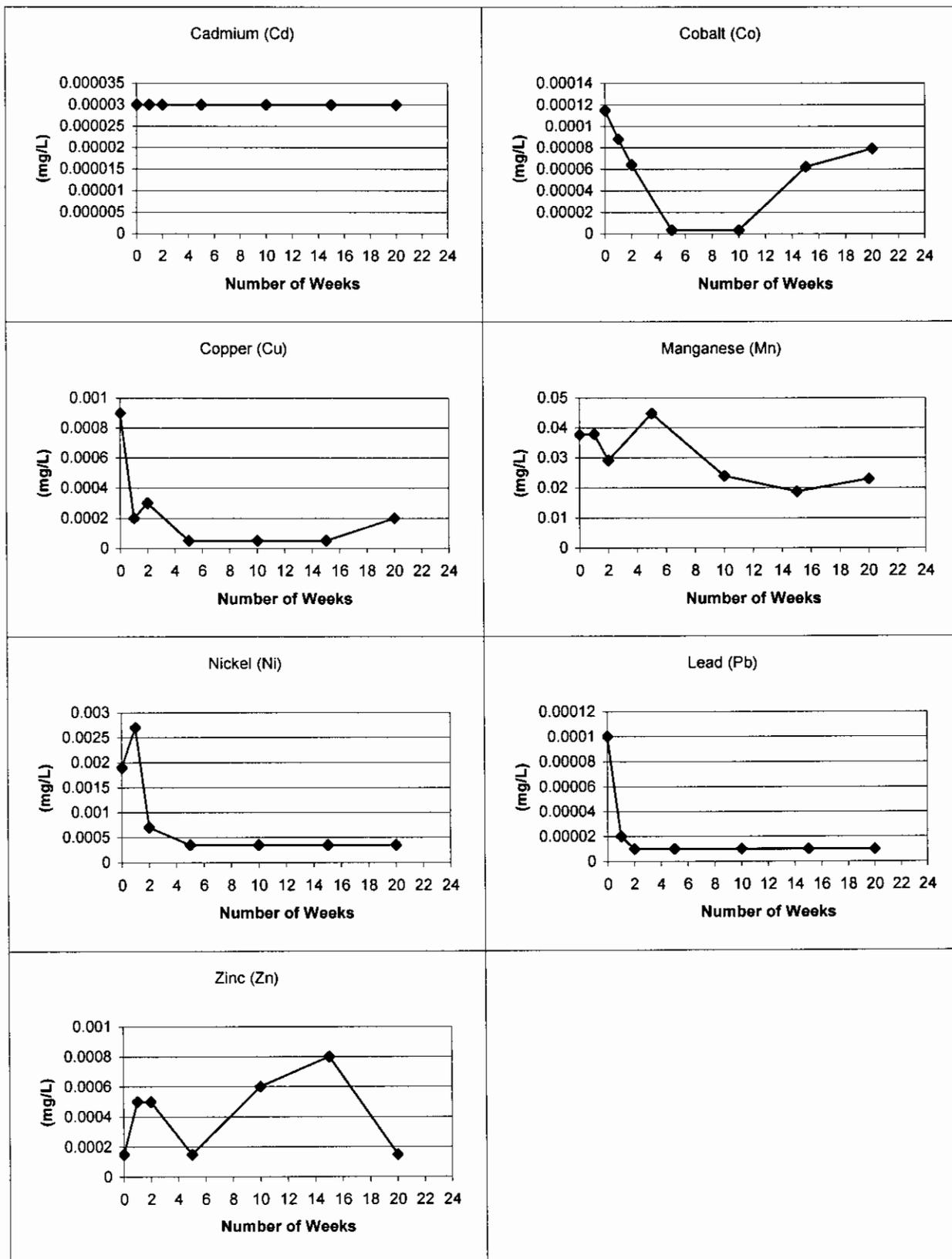
Golder Associates

FIGURE 13
HUMIDITY CELL RESULTS FOR HC 06-085
 Marginal Ore



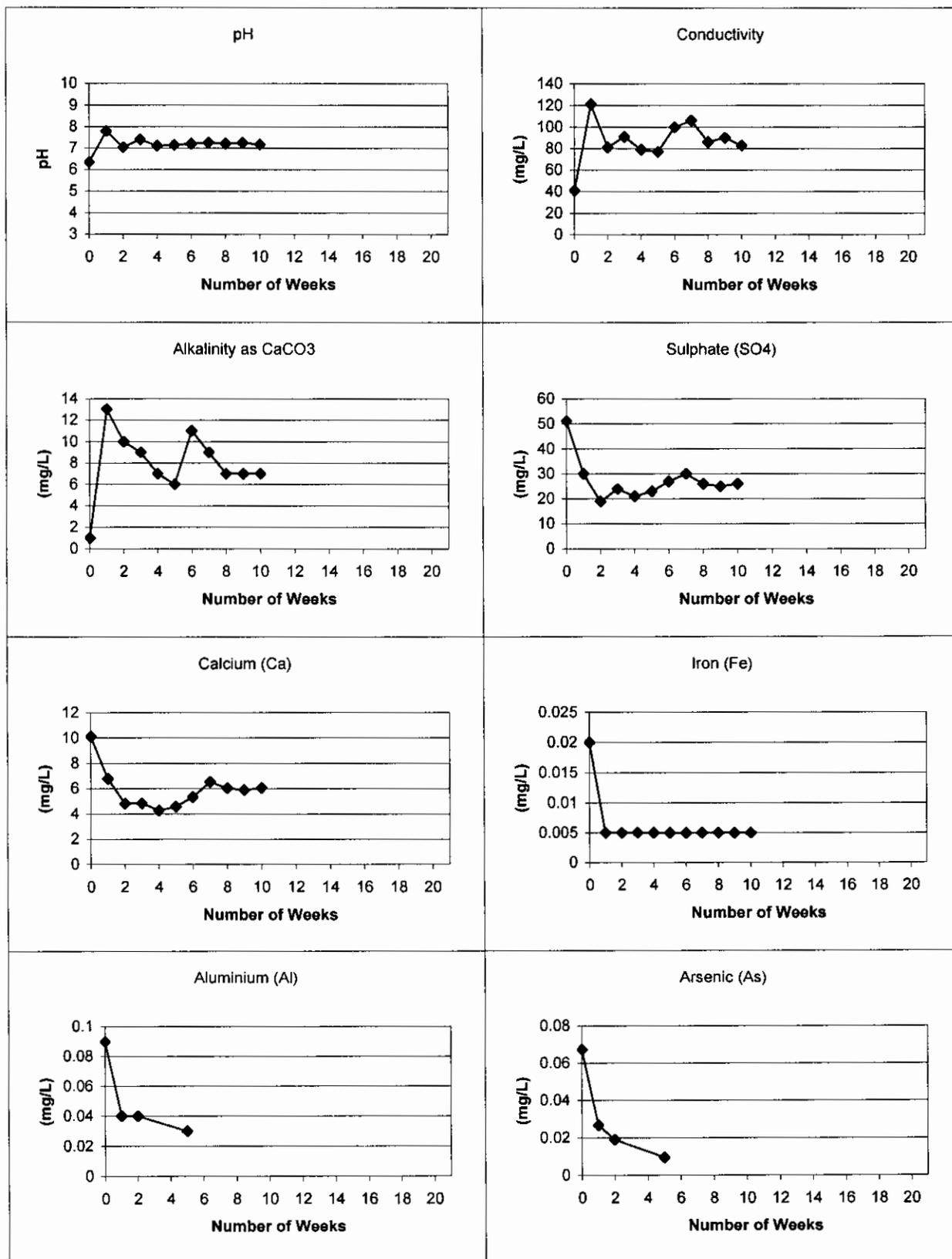
Golder Associates

FIGURE 13
HUMIDITY CELL RESULTS FOR HC 06-085
 Marginal Ore



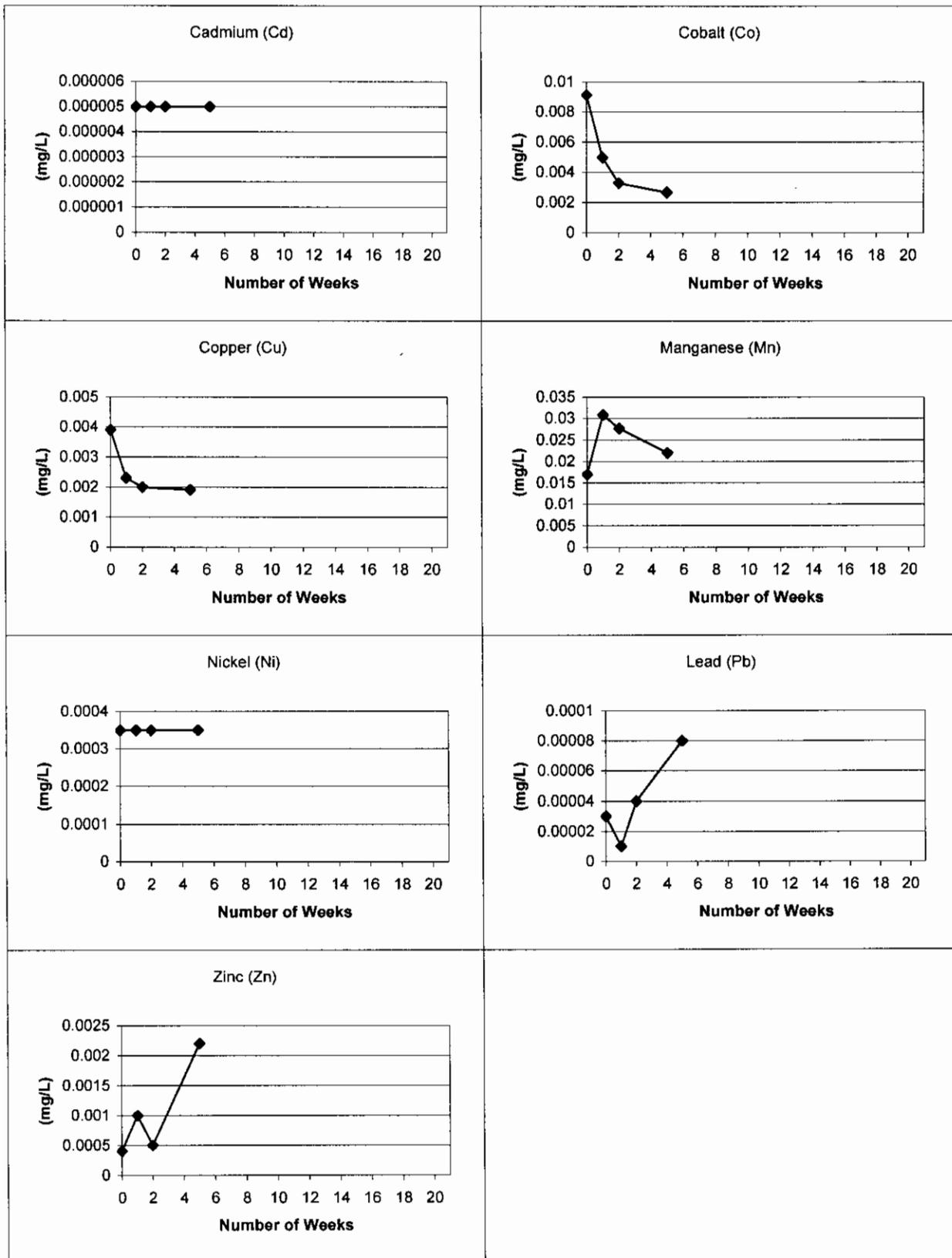
Golder Associates

FIGURE 14
HUMIDITY CELL RESULTS FOR CN 1 CND1-7
Tailings Material



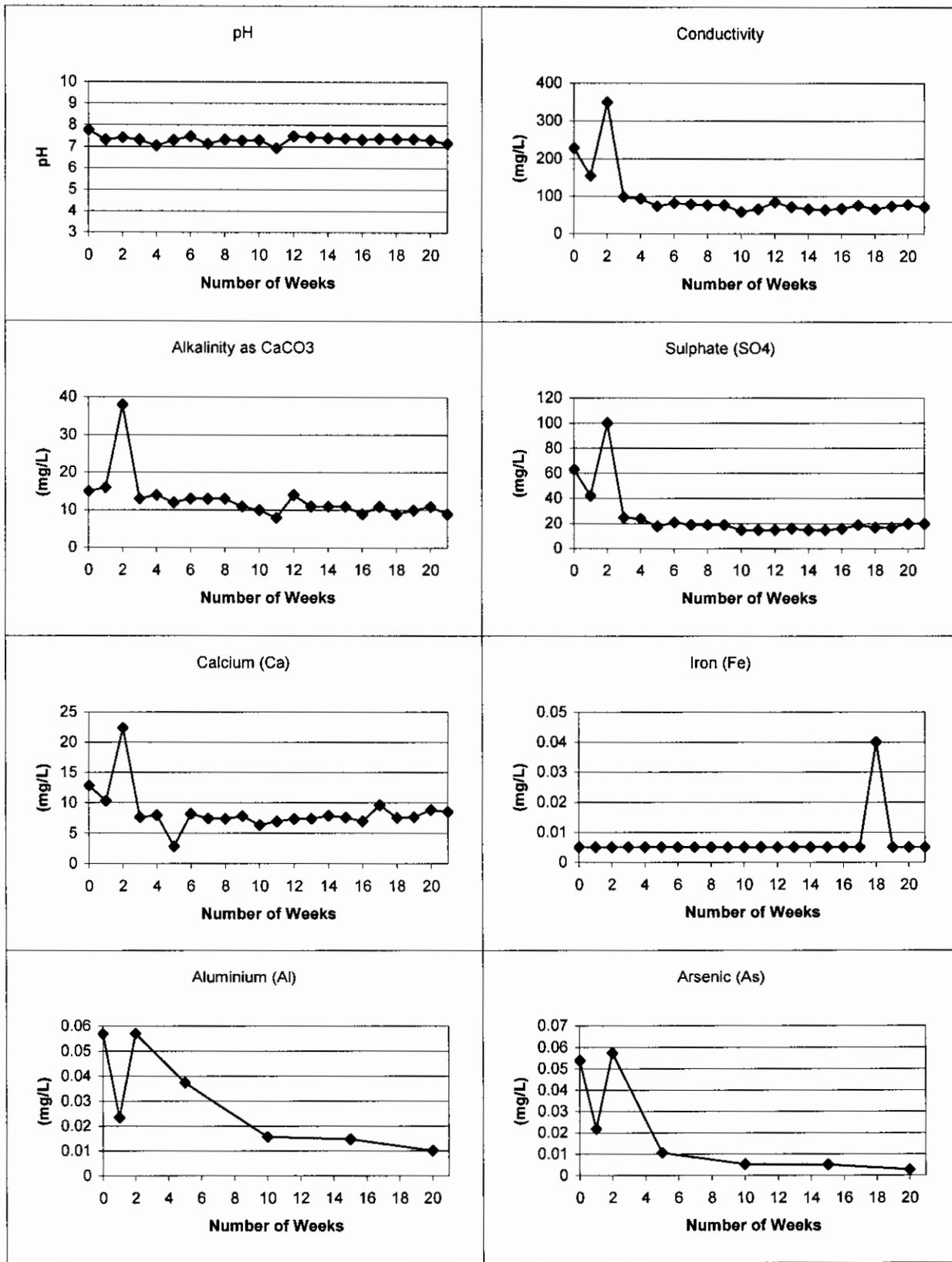
Golder Associates

FIGURE 14
HUMIDITY CELL RESULTS FOR CN 1 CND1-7
Tailings Material



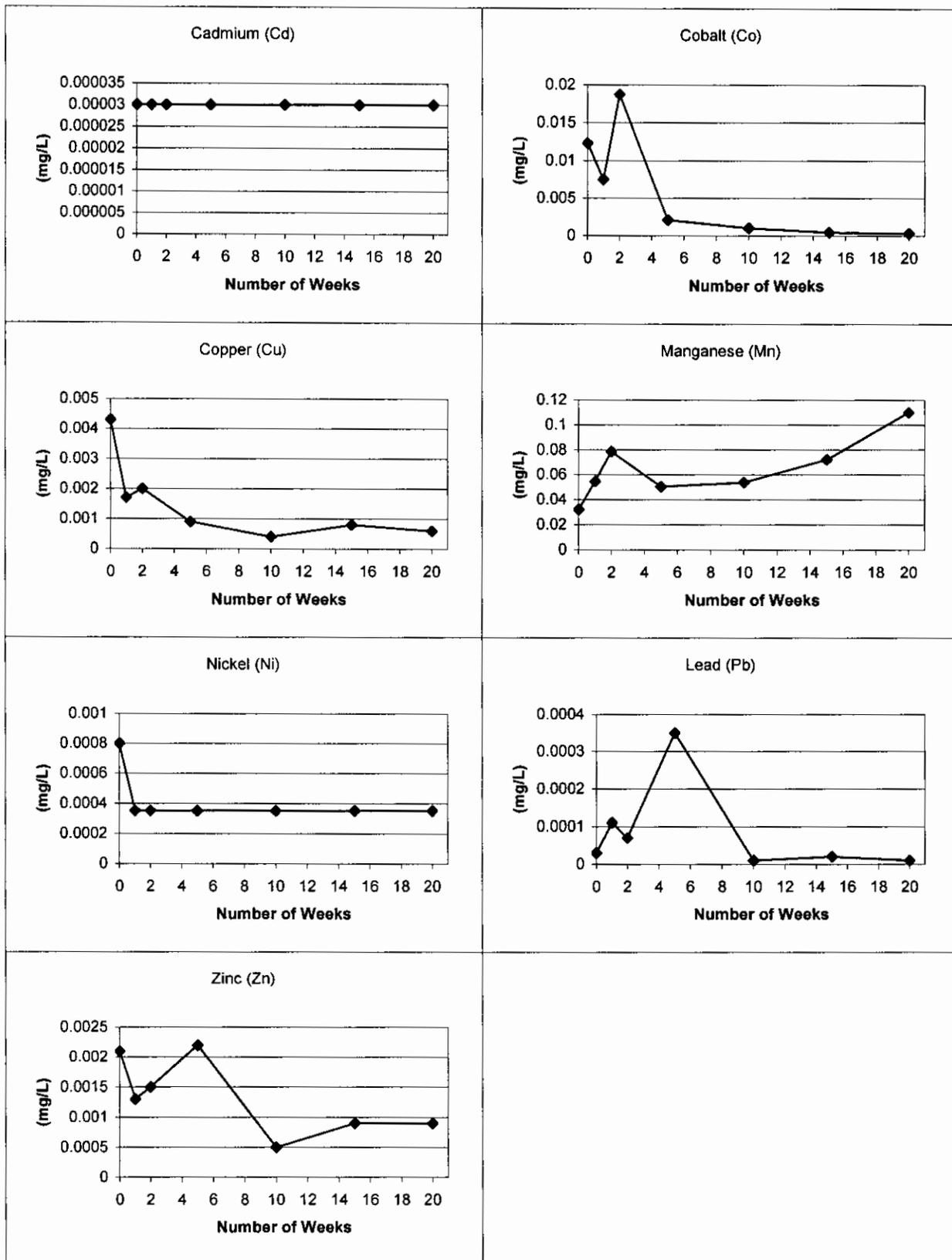
Golder Associates

FIGURE 15
HUMIDITY CELL RESULTS FOR CND 2
Tailings Material



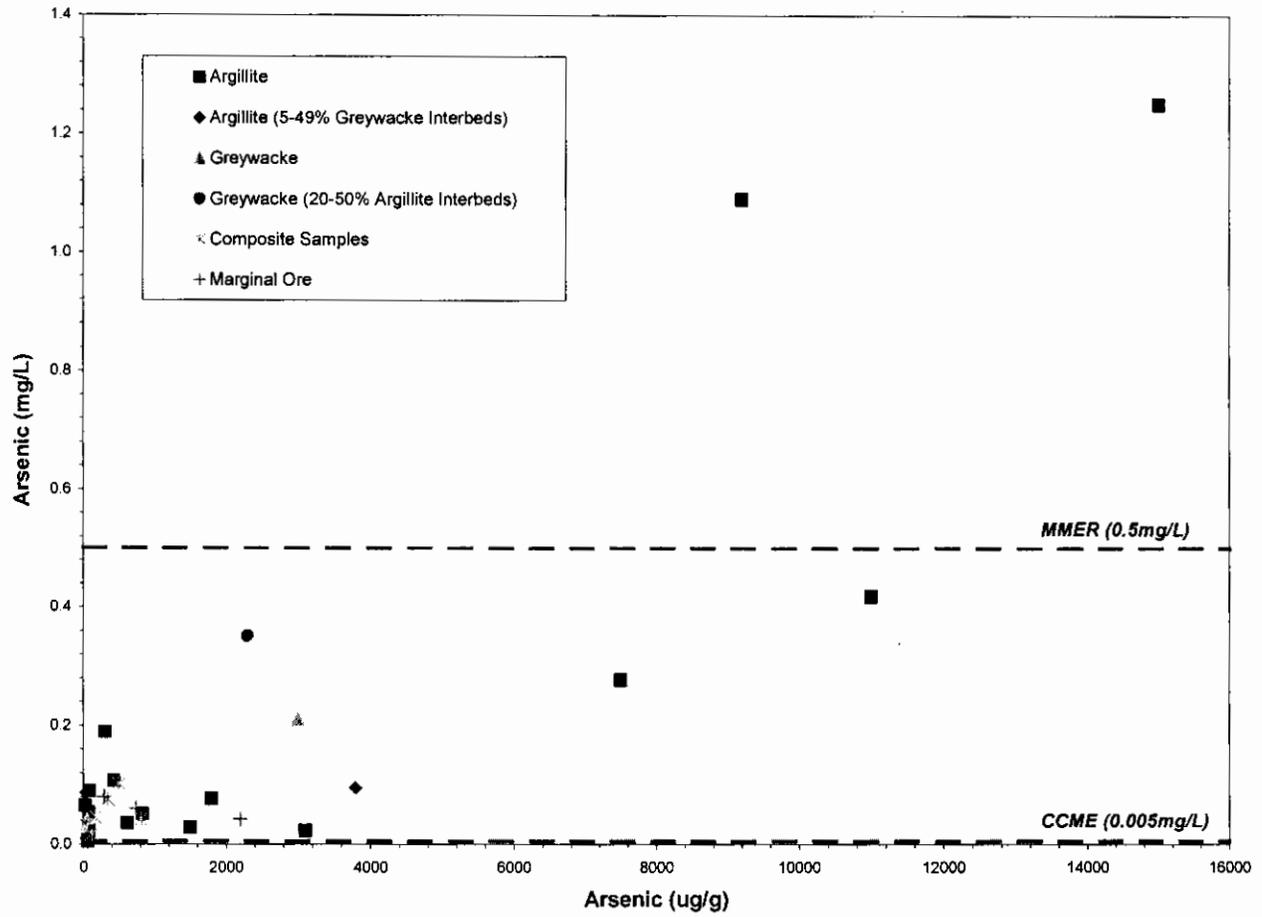
Golder Associates

FIGURE 15
HUMIDITY CELL RESULTS FOR CND 2
Tailings Material



Golder Associates

Figure 16.
Dissolved Arsenic Concentrations vs. Solid Arsenic Concentrations



APPENDIX A
STATIC TEST RESULTS

| Sample # | SiO ₂ (%) | Al ₂ O ₃ (%) | Fe ₂ O ₃ (%) | MgO (%) | CaO (%) | Na ₂ O (%) | K ₂ O (%) | TiO ₂ (%) | P ₂ O ₅ (%) | MnO (%) | Cr ₂ O ₃ (%) | V ₂ O ₅ (%) | LOI (%) | Sum (%) |
|--|----------------------|------------------------------------|------------------------------------|---------|---------|-----------------------|----------------------|----------------------|-----------------------------------|---------|------------------------------------|-----------------------------------|---------|---------|
| ARGILLITE (<49% GREYWACKE) | | | | | | | | | | | | | | |
| 06-012 | 58.10 | 17.40 | 7.23 | 2.30 | 1.72 | 2.07 | 3.27 | 1.06 | 0.12 | 0.12 | 0.01 | 0.01 | 4.78 | 98.20 |
| 06-016 | 63.00 | 15.20 | 6.90 | 1.86 | 2.43 | 1.45 | 2.87 | 0.81 | 0.10 | 0.12 | 0.01 | 0.02 | 4.33 | 99.10 |
| 06-021 | 57.80 | 18.00 | 7.42 | 2.06 | 2.57 | 1.06 | 3.89 | 0.69 | 0.12 | 0.11 | 0.01 | 0.03 | 5.27 | 99.20 |
| 06-040 | 57.10 | 19.50 | 8.36 | 2.51 | 0.87 | 1.14 | 4.18 | 1.01 | 0.15 | 0.10 | 0.02 | <0.01 | 4.43 | 99.40 |
| 06-042 | 60.20 | 16.90 | 7.77 | 2.18 | 1.66 | 1.70 | 3.16 | 0.88 | 0.12 | 0.11 | <0.01 | 0.02 | 4.26 | 98.90 |
| 06-082 | 61.60 | 15.20 | 7.13 | 2.35 | 2.30 | 1.57 | 2.94 | 0.77 | 0.12 | 0.14 | 0.01 | <0.01 | 4.28 | 98.40 |
| ARGILLITE (<5% GREYWACKE) | | | | | | | | | | | | | | |
| 06-004 | 58.20 | 18.80 | 8.21 | 2.49 | 1.06 | 0.87 | 3.98 | 0.88 | 0.12 | 0.09 | <0.01 | 0.01 | 4.44 | 99.10 |
| 06-005 | 57.90 | 18.80 | 9.12 | 2.82 | 1.04 | 0.72 | 4.08 | 0.98 | 0.09 | 0.09 | <0.01 | <0.01 | 4.18 | 99.70 |
| 06-006 | 57.50 | 18.00 | 8.67 | 2.53 | 1.75 | 0.80 | 3.86 | 0.93 | 0.10 | 0.11 | <0.01 | 0.03 | 4.37 | 98.80 |
| 06-009 | 58.90 | 18.00 | 7.64 | 2.40 | 1.99 | 0.74 | 4.18 | 0.90 | 0.10 | 0.10 | <0.01 | 0.03 | 4.40 | 99.00 |
| 06-010 | 55.70 | 18.80 | 7.24 | 2.20 | 2.77 | 0.94 | 4.48 | 0.93 | 0.12 | 0.14 | 0.01 | 0.02 | 5.15 | 98.50 |
| 06-014 | 55.80 | 19.40 | 8.64 | 2.52 | 1.39 | 1.21 | 4.28 | 1.00 | 0.12 | 0.12 | 0.01 | 0.03 | 4.79 | 99.10 |
| 06-017 | 57.80 | 18.30 | 9.40 | 2.53 | 1.07 | 0.81 | 3.78 | 0.89 | 0.13 | 0.10 | <0.01 | 0.02 | 4.39 | 99.00 |
| 06-019 | 56.80 | 18.40 | 8.46 | 2.47 | 1.45 | 0.57 | 4.13 | 0.92 | 0.10 | 0.10 | <0.01 | 0.02 | 4.73 | 98.10 |
| 06-022 | 56.90 | 18.80 | 9.36 | 2.64 | 1.28 | 0.79 | 3.88 | 0.95 | 0.12 | 0.11 | 0.02 | 0.01 | 4.42 | 99.40 |
| 06-025 | 58.20 | 19.50 | 8.83 | 2.48 | 1.15 | 0.70 | 4.28 | 1.00 | 0.13 | 0.11 | <0.01 | <0.01 | 4.52 | 98.80 |
| 06-028 | 54.60 | 20.10 | 9.21 | 2.57 | 0.96 | 0.32 | 4.78 | 1.01 | 0.10 | 0.09 | 0.02 | 0.03 | 4.57 | 98.70 |
| 06-029 | 62.30 | 16.10 | 7.10 | 2.07 | 1.70 | 0.53 | 3.78 | 0.83 | 0.09 | 0.09 | 0.01 | 0.02 | 3.94 | 98.80 |
| 06-030 | 58.90 | 18.70 | 8.88 | 2.65 | 1.19 | 0.59 | 4.20 | 0.97 | 0.11 | 0.08 | 0.01 | 0.02 | 4.46 | 98.60 |
| 06-031 | 56.80 | 19.80 | 7.53 | 2.34 | 2.20 | 0.79 | 4.45 | 0.94 | 0.11 | 0.10 | 0.02 | 0.03 | 4.46 | 98.30 |
| 06-032 | 58.00 | 18.60 | 7.94 | 2.38 | 1.15 | 0.67 | 4.29 | 0.98 | 0.12 | 0.10 | 0.04 | 0.01 | 4.04 | 98.50 |
| 06-033 | 58.80 | 17.30 | 8.11 | 2.45 | 1.91 | 0.98 | 3.63 | 0.94 | 0.12 | 0.11 | 0.03 | <0.01 | 4.36 | 98.80 |
| 06-036 | 53.40 | 19.40 | 8.60 | 2.83 | 1.64 | 0.54 | 4.62 | 1.04 | 0.12 | 0.12 | 0.01 | 0.01 | 5.10 | 97.70 |
| 06-038 | 59.00 | 17.30 | 7.82 | 2.46 | 1.12 | 0.86 | 4.12 | 0.87 | 0.10 | 0.10 | <0.01 | 0.02 | 4.36 | 97.80 |
| 06-041 | 55.80 | 19.70 | 9.17 | 2.74 | 0.93 | 0.94 | 4.11 | 0.97 | 0.13 | 0.10 | <0.01 | 0.02 | 4.61 | 99.20 |
| 06-043 | 58.00 | 18.40 | 7.98 | 2.51 | 1.33 | 0.96 | 3.78 | 0.89 | 0.12 | 0.11 | <0.01 | 0.03 | 4.55 | 98.70 |
| 06-044 | 56.50 | 19.10 | 8.14 | 2.47 | 1.08 | 0.76 | 4.43 | 0.93 | 0.13 | 0.11 | <0.01 | 0.02 | 4.62 | 98.30 |
| 06-046 | 58.20 | 19.00 | 7.88 | 2.53 | 1.02 | 0.84 | 4.30 | 0.92 | 0.11 | 0.10 | <0.01 | <0.01 | 4.30 | 99.20 |
| 06-047 | 58.40 | 18.40 | 8.04 | 2.47 | 1.38 | 0.74 | 4.03 | 0.92 | 0.11 | 0.11 | <0.01 | <0.01 | 4.43 | 99.00 |
| 06-048 | 57.90 | 18.00 | 7.77 | 2.43 | 1.97 | 0.88 | 4.00 | 0.91 | 0.11 | 0.11 | <0.01 | 0.02 | 4.75 | 98.80 |
| 06-049 | 58.30 | 18.00 | 7.93 | 2.51 | 1.52 | 0.79 | 4.03 | 0.86 | 0.11 | 0.12 | <0.01 | 0.02 | 4.24 | 98.40 |
| 06-050 | 57.40 | 18.20 | 8.30 | 2.44 | 1.77 | 0.87 | 4.01 | 0.97 | 0.11 | 0.12 | <0.01 | 0.01 | 4.44 | 98.70 |
| 06-053 | 57.00 | 18.80 | 8.58 | 2.37 | 1.80 | 1.16 | 3.99 | 0.94 | 0.10 | 0.11 | <0.01 | 0.02 | 4.21 | 98.90 |
| 06-054 | 56.90 | 19.90 | 8.11 | 2.67 | 2.10 | 1.58 | 3.10 | 0.94 | 0.11 | 0.15 | <0.01 | <0.01 | 4.88 | 99.30 |
| 06-067 | 62.80 | 15.10 | 7.32 | 2.09 | 0.31 | 0.18 | 3.79 | 0.74 | 0.12 | 0.08 | <0.01 | <0.01 | 3.80 | 97.30 |
| 06-071 | 58.20 | 19.80 | 8.20 | 2.72 | 1.35 | 0.11 | 4.08 | 0.89 | 0.13 | 0.15 | 0.02 | <0.01 | 4.37 | 98.10 |
| 06-073 | 54.80 | 18.30 | 8.46 | 2.75 | 2.17 | 0.87 | 4.42 | 0.93 | 0.11 | 0.13 | <0.01 | <0.01 | 4.77 | 97.70 |
| 06-074 | 56.20 | 18.80 | 8.58 | 2.45 | 1.56 | 0.84 | 4.43 | 0.99 | 0.11 | 0.11 | <0.01 | 0.02 | 4.18 | 98.20 |
| 06-076 | 63.00 | 16.20 | 7.84 | 2.74 | 0.30 | 0.15 | 3.99 | 0.88 | 0.10 | 0.07 | <0.01 | 0.01 | 3.88 | 98.30 |
| 06-077 | 56.90 | 19.00 | 8.72 | 2.48 | 1.03 | 0.63 | 4.53 | 0.95 | 0.11 | 0.09 | 0.01 | 0.03 | 3.94 | 98.30 |
| 06-078 | 58.70 | 18.20 | 7.89 | 2.27 | 1.70 | 1.06 | 4.12 | 0.97 | 0.12 | 0.10 | <0.01 | <0.01 | 3.94 | 99.10 |
| 06-079 | 56.00 | 17.70 | 8.49 | 3.21 | 1.18 | 0.98 | 4.36 | 0.90 | 0.10 | 0.09 | 0.02 | <0.01 | 4.93 | 97.70 |
| 06-080 | 55.70 | 17.80 | 8.05 | 3.17 | 0.85 | 0.51 | 4.58 | 0.87 | 0.09 | 0.09 | 0.01 | 0.02 | 5.37 | 97.10 |
| 06-083 | 52.50 | 19.60 | 8.99 | 3.32 | 1.11 | 0.57 | 5.06 | 0.98 | 0.09 | 0.11 | 0.02 | 0.02 | 5.95 | 98.00 |
| 06-084 | 56.60 | 19.00 | 8.75 | 2.51 | 1.01 | 0.86 | 4.40 | 0.97 | 0.11 | 0.10 | <0.01 | <0.01 | 3.92 | 98.30 |
| COMPOSITE | | | | | | | | | | | | | | |
| 06-007 | 58.90 | 17.90 | 7.26 | 2.25 | 2.93 | 1.20 | 3.78 | 0.91 | 0.11 | 0.12 | 0.01 | 0.01 | 5.07 | 98.40 |
| 06-018 | 58.60 | 17.20 | 7.47 | 2.02 | 2.81 | 1.21 | 3.45 | 0.94 | 0.12 | 0.12 | <0.01 | 0.02 | 5.05 | 99.00 |
| 06-023 | 59.20 | 16.70 | 8.17 | 2.36 | 2.16 | 1.00 | 3.43 | 0.90 | 0.12 | 0.13 | <0.01 | <0.01 | 4.78 | 98.90 |
| 06-027 | 59.50 | 17.40 | 7.60 | 2.27 | 1.74 | 1.23 | 3.51 | 0.95 | 0.13 | 0.10 | <0.01 | 0.01 | 4.39 | 98.90 |
| 06-035 | 59.20 | 16.80 | 6.20 | 1.92 | 3.24 | 1.56 | 3.28 | 0.90 | 0.10 | 0.12 | 0.03 | 0.03 | 4.94 | 98.30 |
| 06-045 | 58.40 | 18.30 | 7.54 | 2.30 | 1.65 | 1.28 | 3.83 | 0.96 | 0.11 | 0.10 | <0.01 | 0.01 | 4.45 | 98.90 |
| 06-051 | 58.00 | 18.10 | 7.96 | 2.48 | 1.71 | 1.53 | 3.57 | 1.00 | 0.12 | 0.12 | <0.01 | <0.01 | 4.29 | 98.90 |
| 06-052 | 62.90 | 17.20 | 7.13 | 2.21 | 1.51 | 1.73 | 3.35 | 0.90 | 0.12 | 0.10 | <0.01 | 0.03 | 3.71 | 100.00 |
| 06-055 | 60.30 | 18.30 | 7.37 | 2.17 | 0.50 | 1.44 | 3.97 | 0.95 | 0.11 | 0.08 | <0.01 | <0.01 | 3.89 | 98.90 |
| 06-058 | 61.80 | 17.30 | 6.72 | 2.48 | 1.36 | 1.78 | 3.66 | 0.99 | 0.10 | 0.09 | <0.01 | 0.03 | 3.88 | 99.70 |
| 06-059 | 58.00 | 14.40 | 5.08 | 1.93 | 8.69 | 2.32 | 2.57 | 0.72 | 0.16 | 0.21 | 0.02 | <0.01 | 7.29 | 99.40 |
| 06-082 | 60.80 | 18.20 | 7.47 | 2.27 | 0.74 | 1.50 | 3.80 | 0.97 | 0.12 | 0.09 | <0.01 | 0.01 | 3.86 | 99.80 |
| 06-084 | 59.10 | 17.90 | 7.66 | 2.29 | 1.35 | 1.84 | 3.69 | 0.99 | 0.10 | 0.13 | 0.03 | 0.02 | 3.98 | 98.80 |
| 06-089 | 60.40 | 15.90 | 6.89 | 2.01 | 3.20 | 1.50 | 3.19 | 0.91 | 0.13 | 0.15 | <0.01 | 0.01 | 5.02 | 99.10 |
| 06-070 | 65.10 | 14.60 | 6.13 | 1.91 | 1.40 | 1.84 | 2.91 | 0.79 | 0.08 | 0.12 | <0.01 | 0.01 | 3.82 | 98.80 |
| GREYWACKE (20%-50% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | |
| 06-001 | 60.30 | 16.80 | 7.34 | 2.14 | 1.55 | 1.87 | 3.40 | 0.90 | 0.10 | 0.11 | 0.02 | 0.03 | 4.07 | 98.40 |
| 06-002 | 55.50 | 19.50 | 9.06 | 2.57 | 1.18 | 0.87 | 4.23 | 0.99 | 0.11 | 0.11 | <0.01 | 0.01 | 4.61 | 98.60 |
| 06-003 | 59.90 | 17.10 | 7.40 | 2.07 | 1.84 | 1.41 | 3.63 | 0.93 | 0.12 | 0.13 | 0.01 | 0.02 | 4.55 | 99.00 |
| 06-011 | 63.40 | 15.50 | 6.22 | 1.86 | 1.66 | 2.15 | 2.89 | 0.98 | 0.14 | 0.12 | <0.01 | 0.03 | 4.00 | 98.90 |
| 06-013 | 70.80 | 11.70 | 3.65 | 0.95 | 2.55 | 2.77 | 1.88 | 0.78 | 0.10 | 0.09 | 0.01 | <0.01 | 3.44 | 98.80 |
| 06-015 | 68.40 | 12.90 | 4.97 | 1.56 | 1.54 | 2.46 | 2.04 | 0.77 | 0.09 | 0.12 | 0.02 | <0.01 | 3.41 | 98.40 |
| 06-020 | 84.90 | 13.40 | 6.22 | 1.56 | 3.33 | 1.58 | 2.33 | 0.74 | 0.09 | 0.15 | <0.01 | 0.02 | 4.65 | 99.00 |
| 06-024 | 66.20 | 14.60 | 5.83 | 1.59 | 2.05 | 2.07 | 2.51 | 0.78 | 0.10 | 0.09 | <0.01 | 0.02 | 3.63 | 99.50 |
| 06-026 | 60.80 | 17.20 | 6.80 | 1.89 | 1.80 | 1.31 | 3.56 | 0.98 | 0.14 | 0.09 | <0.01 | 0.02 | 4.22 | 98.80 |
| 06-034 | 66.50 | 13.10 | 5.04 | 1.82 | 2.02 | 2.33 | 2.16 | 0.84 | 0.09 | 0.10 | 0.01 | 0.01 | 3.69 | 98.40 |
| 06-039 | 60.60 | 16.80 | 6.42 | 2.22 | 1.94 | 2.28 | 3.28 | 0.91 | 0.12 | 0.10 | <0.01 | 0.02 | 3.87 | 98.80 |
| 06-057 | 64.00 | 14.40 | 4.83 | 1.40 | 3.89 | 2.32 | 2.88 | 0.88 | 0.08 | 0.15 | 0.01 | 0.01 | 4.92 | 99.70 |
| GREYWACKE (<20% ARGILLITE INTERBEDS) | | | | | | | | | | | | | | |
| 06-056 | 68.50 | 12.60 | 3.95 | 1.11 | 4.08 | 2.59 | 2.02 | 0.71 | 0.07 | 0.13 | <0.01 | 0.02 | 4.51 | 100.30 |
| 06-060 | 66.90 | 12.40 | 4.53 | 1.85 | 3.59 | 2.83 | 1.56 | 0.84 | 0.14 | 0.11 | <0.01 | <0.01 | 4.38 | 98.70 |
| 06-061 | 70.70 | 11.80 | 3.94 | 1.45 | 2.13 | 3.14 | 1.31 | 0.60 | 0.14 | 0.11 | <0.01 | 0.02 | 3.16 | 98.30 |
| 06-063 | 68.80 | 12.80 | 3.87 | 1.08 | 2.86 | 2.52 | 2.18 | 0.75 | 0.08 | 0.10 | <0.01 | <0.01 | 3.85 | 98.80 |
| 06-066 | 63.10 | 14.40 | 5.44 | 1.64 | 2.76 | 1.99 | 2.51 | 0.89 | 0.13 | 0.12 | <0.01 | 0.02 | 4.21 | 97.20 |
| 06-068 | 84.70 | 15.30 | 5.26 | 1.79 | 1.80 | 2.89 | 2.91 | 0.87 | 0.12 | 0.10 | 0.01 | 0.01 | 3.45 | 99.00 |
| 06-068 | 88.10 | 13.80 | 4.46 | 1.28 | 1.98 | 2.51 | 2.36 | 0.84 | 0.07 | 0.08 | 0.01 | 0.01 | 3.38 | 98.90 |
| 06-072 | 71.00 | 12.70 | 4.54 | 1.84 | 1.30 | 3.14 | 1.56 | 0.58 | 0.14 | 0.09 | 0.01 | 0.01 | 2.65 | 99.80 |
| 06-075 | 67.20 | 14.10 | 5.88 | 2.33 | 1.57 | & | | | | | | | | |

| Sample # | Paste pH | NP (CaCO ₃ /1000) | AP (CaCO ₃ *1000) | Net NP (CaCO ₃ /1000) | NP/AP ratio | S | Acid Leachable SO ₄ -S % | Sulphide-S % | C | Carbonate % | TIC % | Carb-AP (CaCO ₃ /1000) | Carb-NP/AP ratio |
|--|----------|---------------------------------|---------------------------------|-------------------------------------|----------------|-------|--|-----------------|------|----------------|----------|--------------------------------------|---------------------|
| ARGILLITE (8-9% GREYWACKE) | | | | | | | | | | | | | |
| 06-012 | 9.4 | 41.40 | 2.5 | 38.9 | 16.6 | 0.11 | 0.02 | 0.05 | 0.59 | 1.92 | 0.38 | 32.0 | 12.8 |
| 06-016 | 9.3 | 45.00 | 6.9 | 38.1 | 16.24 | 0.02 | 0.22 | 0.61 | 2.35 | 2.47 | 0.30 | 38.7 | 5.7 |
| 06-021 | 9.4 | 48.70 | 0.9 | 47.8 | 49.8 | 0.05 | 0.02 | 0.03 | 0.62 | 2.18 | 0.43 | 36.0 | 40.0 |
| 06-040 | 8.8 | 21.20 | 3.1 | 18.0 | 6.8 | 0.13 | 0.03 | 0.10 | 0.41 | 1.31 | 0.26 | 21.8 | 7.0 |
| 06-042 | 8.8 | 37.10 | 3.8 | 33.4 | 9.8 | 0.34 | 0.22 | 0.12 | 0.57 | 1.93 | 0.30 | 33.2 | 8.5 |
| 06-062 | 8.8 | 41.80 | 11.9 | 30.0 | 3.5 | 0.96 | 0.28 | 0.38 | 0.95 | 2.82 | 0.58 | 48.7 | 4.1 |
| DA 7357 | 8.8 | 115.07 | 3.5 | 111.6 | 32.8 | 0.11 | 0.01 | 0.10 | 6.11 | - | - | 101.9 | 29.1 |
| ARGILLITE (<5% GREYWACKE) | | | | | | | | | | | | | |
| 06-004 | 9.4 | 25.30 | 2.2 | 23.1 | 11.5 | 0.07 | <0.01 | 0.07 | 0.34 | 1.24 | 0.25 | 20.7 | 9.4 |
| 06-006 | 9.4 | 22.10 | 4.4 | 17.7 | 5.0 | 0.17 | 0.03 | 0.14 | 0.23 | 0.77 | 0.15 | 12.8 | 2.9 |
| 06-008 | 9.4 | 33.00 | 5.8 | 27.4 | 5.9 | 0.22 | 0.04 | 0.18 | 0.38 | 1.48 | 0.30 | 24.7 | 4.4 |
| 06-009 | 9.4 | 31.40 | 8.4 | 22.9 | 3.7 | 0.30 | 0.03 | 0.37 | 0.42 | 1.52 | 0.30 | 25.4 | 3.0 |
| 06-010 | 9.3 | 51.80 | 7.8 | 44.0 | 6.8 | 0.28 | 0.04 | 0.25 | 0.85 | 2.54 | 0.51 | 42.4 | 5.4 |
| 06-014 | 9.2 | 33.80 | 8.1 | 24.8 | 3.7 | 0.32 | 0.04 | 0.29 | 0.49 | 2.00 | 0.40 | 33.4 | 3.7 |
| 06-017 | 9.4 | 20.10 | 0.9 | 19.1 | 21.4 | 0.03 | <0.01 | 0.03 | 0.24 | 0.92 | 0.19 | 15.3 | 17.0 |
| 06-019 | 9.4 | 31.80 | 3.8 | 28.7 | 6.3 | 0.25 | 0.06 | 0.19 | 0.40 | 1.40 | 0.28 | 23.4 | 4.0 |
| 06-022 | 9.4 | 22.80 | 1.2 | 21.6 | 18.3 | 0.07 | 0.03 | 0.04 | 0.28 | 1.18 | 0.24 | 19.7 | 18.4 |
| 06-025 | 9.2 | 22.30 | 1.8 | 20.7 | 14.3 | 0.10 | 0.05 | 0.05 | 0.28 | 1.08 | 0.21 | 17.7 | 11.0 |
| 06-029 | 9.3 | 18.60 | 5.0 | 13.6 | 3.7 | 0.30 | 0.14 | 0.16 | 0.25 | 1.12 | 0.22 | 18.7 | 3.7 |
| 06-030 | 9.3 | 23.20 | 2.2 | 21.0 | 10.6 | 0.10 | 0.03 | 0.20 | 0.48 | 0.91 | 0.18 | 15.2 | 2.4 |
| 06-031 | 9.4 | 37.70 | 4.7 | 33.0 | 10.40 | 0.02 | 0.05 | 0.07 | 0.27 | 1.85 | 0.39 | 32.5 | 14.8 |
| 06-032 | 9.5 | 21.70 | 3.4 | 18.2 | 6.3 | 0.19 | 0.08 | 0.11 | 0.28 | 2.04 | 0.41 | 34.0 | 10.0 |
| 06-033 | 9.5 | 33.80 | 3.8 | 30.1 | 9.0 | 0.27 | 0.15 | 0.12 | 0.43 | 1.67 | 0.34 | 27.9 | 7.3 |
| 06-038 | 9.4 | 42.00 | 14.7 | 27.4 | 2.9 | 1.14 | 0.67 | 0.47 | 0.71 | 3.05 | 0.81 | 50.9 | 3.6 |
| 06-041 | 8.9 | 32.50 | 3.8 | 28.7 | 4.2 | 0.98 | 0.33 | 0.25 | 0.51 | 1.91 | 0.38 | 31.9 | 4.1 |
| 06-043 | 8.8 | 22.30 | 3.8 | 18.6 | 6.0 | 0.16 | 0.04 | 0.12 | 0.33 | 1.04 | 0.21 | 17.3 | 4.8 |
| 06-043 | 8.8 | 30.30 | 1.9 | 28.4 | 18.2 | 0.13 | 0.07 | 0.08 | 0.48 | 2.10 | 0.42 | 35.0 | 18.4 |
| 06-044 | 9.4 | 27.70 | 2.8 | 24.9 | 9.9 | 0.17 | 0.08 | 0.09 | 0.40 | 1.28 | 0.26 | 21.3 | 7.8 |
| 06-046 | 9.4 | 22.90 | 2.8 | 20.1 | 8.1 | 0.18 | 0.07 | 0.09 | 0.34 | 1.34 | 0.27 | 22.3 | 8.0 |
| 06-047 | 9.3 | 28.20 | 3.4 | 24.8 | 8.2 | 0.18 | 0.07 | 0.11 | 0.38 | 1.88 | 0.34 | 28.0 | 8.2 |
| 06-048 | 9.4 | 34.20 | 2.5 | 31.7 | 13.7 | 0.13 | 0.06 | 0.08 | 0.43 | 1.87 | 0.37 | 31.3 | 12.5 |
| 06-049 | 9.4 | 29.20 | 6.9 | 22.3 | 4.2 | 0.29 | 0.07 | 0.22 | 0.38 | 1.51 | 0.30 | 25.2 | 3.7 |
| 06-050 | 9.5 | 30.60 | 4.4 | 26.2 | 7.0 | 0.19 | 0.05 | 0.14 | 0.46 | 1.91 | 0.38 | 31.9 | 7.2 |
| 06-053 | 9.5 | 32.50 | 5.0 | 27.5 | 8.5 | 0.25 | 0.08 | 0.16 | 0.31 | 1.19 | 0.24 | 19.8 | 4.0 |
| 06-054 | 9.8 | 32.00 | 1.2 | 30.8 | 25.8 | 0.06 | 0.02 | 0.04 | 0.42 | 1.85 | 0.37 | 30.9 | 25.7 |
| 06-067 | 8.9 | 7.90 | 21.2 | -13.3 | 0.4 | 0.92 | 0.24 | 0.58 | 0.37 | 0.16 | 5.0 | 0.2 | |
| 06-071 | 9.4 | 33.20 | 14.4 | 18.8 | 2.3 | 0.48 | 0.02 | 0.46 | 0.39 | 1.82 | 0.32 | 27.0 | 1.9 |
| 06-073 | 9.2 | 48.80 | 17.2 | 31.8 | 2.8 | 1.19 | 0.84 | 0.56 | 0.97 | 3.75 | 0.75 | 62.5 | 3.6 |
| 06-074 | 9.5 | 27.50 | 4.7 | 22.8 | 5.9 | 0.47 | 0.32 | 0.15 | 0.45 | 1.50 | 0.30 | 25.0 | 5.3 |
| 06-076 | 9.0 | 7.10 | 8.1 | -1.0 | 9.8 | 0.38 | 0.30 | 0.29 | 0.17 | 0.50 | 0.10 | 8.3 | 0.9 |
| 06-077 | 9.4 | 19.30 | 5.0 | 14.3 | 3.8 | 0.42 | 0.25 | 0.16 | 0.62 | 1.17 | 0.11 | 13.7 | 2.7 |
| 06-078 | 9.8 | 30.10 | 2.5 | 27.6 | 12.0 | 0.33 | 0.25 | 0.08 | 0.47 | 1.56 | 0.32 | 26.4 | 10.5 |
| 06-079 | 9.4 | 28.50 | 15.9 | 12.7 | 1.8 | 1.20 | 0.89 | 0.51 | 0.49 | 1.98 | 0.39 | 32.7 | 2.1 |
| 06-080 | 9.3 | 21.40 | 24.4 | -3.0 | 0.9 | 1.32 | 0.54 | 0.78 | 0.62 | 2.08 | 0.42 | 34.7 | 1.4 |
| 06-083 | 9.0 | 25.80 | 28.2 | -2.4 | 10.0 | 0.52 | 0.78 | 0.84 | 0.73 | 2.77 | 0.56 | 46.2 | 1.8 |
| 06-084 | 8.7 | 19.00 | 4.4 | 14.6 | 4.3 | 0.35 | 0.21 | 0.14 | 0.37 | 1.18 | 0.24 | - | 4.5 |
| DA 0423 | 8.8 | 73.43 | 4.7 | 68.8 | 15.8 | 0.149 | 0.01 | 0.14 | 2.43 | - | - | 40.5 | 8.7 |
| DA 0562 | 7.7 | 50.24 | 5.5 | 44.8 | 9.2 | 0.175 | 0.02 | 0.16 | 1.80 | - | - | 30.0 | 5.5 |
| DA 1893 | 8.8 | 30.48 | 3.2 | 27.3 | 9.7 | 0.101 | 0.00 | 0.10 | 0.94 | - | - | 15.7 | 5.0 |
| DA 8107 | 9.7 | 48.31 | 5.1 | 43.3 | 9.5 | 0.162 | 0.02 | 0.14 | 1.88 | - | - | 31.3 | 8.2 |
| COMPOSITE | | | | | | | | | | | | | |
| 06-007 | 9.4 | 54.20 | 6.2 | 48.0 | 8.7 | 0.23 | 0.03 | 0.20 | 0.85 | 2.53 | 0.51 | 42.2 | 6.8 |
| 06-019 | 9.3 | 50.20 | 4.1 | 46.2 | 12.4 | 0.18 | 0.05 | 0.13 | 0.88 | 2.47 | 0.50 | 41.2 | 10.0 |
| 06-023 | 9.3 | 41.50 | 5.0 | 36.5 | 8.3 | 0.13 | <0.01 | 0.16 | 0.45 | 1.99 | 0.40 | 33.2 | 6.6 |
| 06-027 | 9.4 | 33.50 | 2.8 | 30.7 | 11.9 | 0.10 | 0.02 | 0.06 | 0.38 | 1.29 | 0.26 | 21.5 | 7.7 |
| 06-035 | 9.2 | 57.70 | 7.5 | 50.2 | 7.7 | 0.45 | 0.21 | 0.24 | 0.87 | 3.43 | 0.89 | 57.3 | 7.8 |
| 06-045 | 9.4 | 30.60 | 2.8 | 27.8 | 10.9 | 0.14 | 0.04 | 0.09 | 0.48 | 1.73 | 0.35 | 28.9 | 10.3 |
| 06-051 | 9.2 | 29.30 | 4.7 | 24.6 | 6.3 | 0.23 | 0.06 | 0.15 | 0.41 | 1.49 | 0.30 | 24.9 | 5.3 |
| 06-052 | 9.5 | 26.50 | 4.1 | 22.4 | 8.5 | 0.31 | 0.18 | 0.13 | 0.37 | 1.33 | 0.27 | 22.2 | 5.4 |
| 06-055 | 9.1 | 8.90 | 1.2 | 7.5 | 7.0 | 0.06 | 0.02 | 0.04 | 0.13 | 0.45 | 0.06 | 7.5 | 6.3 |
| 06-058 | 9.5 | 23.00 | 3.1 | 19.9 | 7.4 | 0.15 | 0.05 | 0.10 | 0.31 | 1.05 | 0.21 | 17.7 | 8.7 |
| 06-059 | 9.4 | 120.00 | 1.8 | 118.0 | 83.7 | 0.05 | 0.02 | 0.06 | 1.44 | 6.64 | 1.33 | 110.7 | 58.3 |
| 06-062 | 9.2 | 13.50 | 2.2 | 11.3 | 6.1 | 0.08 | <0.01 | 0.07 | 0.16 | 0.58 | 0.12 | 9.7 | 4.4 |
| 06-064 | 9.3 | 25.30 | 3.4 | 21.8 | 7.3 | 0.17 | 0.08 | 0.11 | 0.31 | 1.10 | 0.22 | 19.3 | 5.4 |
| 06-068 | 9.3 | 56.50 | 5.8 | 51.7 | 10.6 | 0.20 | 0.03 | 0.17 | 0.57 | 2.83 | 0.57 | 47.2 | 8.9 |
| 06-070 | 9.5 | 27.80 | 11.8 | 16.3 | 2.4 | 0.34 | <0.01 | 0.37 | 0.36 | 1.27 | 0.25 | 21.2 | 1.8 |
| GREYWACKE (20% ARGILLITE INTERBEDS) | | | | | | | | | | | | | |
| 06-001 | 9.3 | 38.00 | 8.8 | 30.3 | 4.4 | 0.39 | 0.11 | 0.29 | 0.99 | 1.69 | 0.34 | 28.2 | 3.2 |
| 06-002 | 9.4 | 28.20 | 4.1 | 24.2 | 6.9 | 0.18 | 0.05 | 0.13 | 0.44 | 1.70 | 0.34 | 28.4 | 6.9 |
| 06-003 | 9.4 | 44.30 | 8.1 | 36.2 | 8.5 | 0.26 | <0.01 | 0.25 | 0.73 | 2.25 | 0.45 | 37.5 | 4.8 |
| 06-011 | 9.3 | 38.40 | 0.6 | 37.8 | 81.4 | 0.18 | 0.14 | 0.02 | 0.52 | 2.05 | 0.41 | 34.2 | 57.0 |
| 06-013 | 9.4 | 47.20 | 2.8 | 44.4 | 18.8 | 0.11 | 0.02 | 0.09 | 0.95 | 2.07 | 0.41 | 34.5 | 12.3 |
| 06-015 | 9.5 | 40.80 | 4.7 | 36.2 | 8.7 | 0.15 | <0.01 | 0.15 | 0.50 | 1.88 | 0.34 | 28.0 | 6.8 |
| 06-020 | 9.3 | 58.20 | 2.5 | 55.7 | 23.3 | 0.08 | <0.01 | 0.08 | 0.71 | 2.98 | 0.80 | 49.7 | 19.8 |
| 06-024 | 9.4 | 35.80 | 1.9 | 33.9 | 19.1 | 0.07 | 0.01 | 0.05 | 0.44 | 1.82 | 0.38 | 32.0 | 16.9 |
| 06-026 | 9.4 | 31.20 | 2.8 | 28.4 | 11.1 | 0.15 | 0.06 | 0.08 | 0.51 | 2.09 | 0.42 | 34.0 | 12.4 |
| 06-034 | 9.7 | 50.50 | 2.5 | 48.0 | 20.2 | 0.16 | 0.08 | 0.08 | 0.67 | 2.85 | 0.57 | 47.5 | 19.0 |
| 06-039 | 9.3 | 32.70 | 15.3 | 17.4 | 2.1 | 0.58 | 0.09 | 0.49 | 0.78 | 2.90 | 0.60 | 49.9 | 3.3 |
| 06-047 | 9.5 | 67.50 | 2.5 | 65.0 | 27.0 | 0.12 | 0.04 | 0.09 | 0.83 | 3.62 | 0.73 | 80.4 | 24.2 |
| DA 0472 | 7.4 | 48.53 | 4.0 | 40.5 | 7.8 | 0.19 | 0.01 | 0.19 | 0.99 | - | - | 16.4 | 4.7 |
| GREYWACKE (<20% ARGILLITE INTERBEDS) | | | | | | | | | | | | | |
| 06-058 | 9.5 | 70.50 | 2.5 | 68.1 | 28.2 | 0.11 | 0.03 | 0.08 | 0.82 | 3.77 | 0.75 | 82.9 | 25.2 |
| 06-060 | 9.5 | 63.20 | 0.9 | 62.3 | 67.4 | 0.06 | 0.03 | 0.03 | 0.72 | 3.38 | 0.68 | 56.4 | 62.6 |
| 06-061 | 9.8 | 42.00 | 0.9 | 41.1 | 44.8 | 0.05 | 0.02 | 0.03 | 0.45 | 2.10 | 0.42 | 35.0 | 38.9 |
| 06-063 | 9.8 | 52.00 | 1.2 | 48.8 | 42.0 | 0.08 | 0.02 | 0.04 | 0.80 | 2.75 | 0.55 | | |

APPENDIX B
KINETIC TEST RESULTS

Appendix B4
 MINORITY CELL RESULTS FOR MC-46
 Aquifer (4% Drawdown)

0.25%
 0.7%
 29 X (C600/100)
 25 X (C600/100)
 6.5 (C600/100)
 1000 g

| Well ID | MC-46 | 06-Jan-07 | 13-Feb-07 | 20-Mar-07 | 27-Apr-07 | 04-May-07 | 11-Jun-07 | 18-Jul-07 | 25-Aug-07 | 01-Sep-07 | 08-Oct-07 | 15-Nov-07 | 22-Dec-07 | 29-Jan-08 | 05-Feb-08 | 12-Mar-08 | 19-Apr-08 | 26-May-08 | 02-Jun-08 | 09-Jul-08 | 16-Aug-08 | 23-Sep-08 | 30-Oct-08 | 06-Nov-08 | 13-Dec-08 | 20-Jan-09 | 27-Feb-09 | 05-Mar-09 | 12-Apr-09 | 19-May-09 | 26-Jun-09 | 03-Jul-09 | 10-Aug-09 | 17-Sep-09 | 24-Oct-09 | 31-Nov-09 | 07-Dec-09 | 14-Jan-10 | 21-Feb-10 | 28-Mar-10 | 05-Apr-10 | 12-May-10 | 19-Jun-10 | 26-Jul-10 | 02-Aug-10 | 09-Sep-10 | 16-Oct-10 | 23-Nov-10 | 30-Dec-10 | 06-Jan-11 | 13-Feb-11 | 20-Mar-11 | 27-Apr-11 | 04-May-11 | 11-Jun-11 | 18-Jul-11 | 25-Aug-11 | 01-Sep-11 | 08-Oct-11 | 15-Nov-11 | 22-Dec-11 | 29-Jan-12 | 05-Feb-12 | 12-Mar-12 | 19-Apr-12 | 26-May-12 | 02-Jun-12 | 09-Jul-12 | 16-Aug-12 | 23-Sep-12 | 30-Oct-12 | 06-Nov-12 | 13-Dec-12 | 20-Jan-13 | 27-Feb-13 | 05-Mar-13 | 12-Apr-13 | 19-May-13 | 26-Jun-13 | 03-Jul-13 | 10-Aug-13 | 17-Sep-13 | 24-Oct-13 | 31-Nov-13 | 07-Dec-13 | 14-Jan-14 | 21-Feb-14 | 28-Mar-14 | 05-Apr-14 | 12-May-14 | 19-Jun-14 | 26-Jul-14 | 02-Aug-14 | 09-Sep-14 | 16-Oct-14 | 23-Nov-14 | 30-Dec-14 | 06-Jan-15 | 13-Feb-15 | 20-Mar-15 | 27-Apr-15 | 04-May-15 | 11-Jun-15 | 18-Jul-15 | 25-Aug-15 | 01-Sep-15 | 08-Oct-15 | 15-Nov-15 | 22-Dec-15 | 29-Jan-16 | 05-Feb-16 | 12-Mar-16 | 19-Apr-16 | 26-May-16 | 02-Jun-16 | 09-Jul-16 | 16-Aug-16 | 23-Sep-16 | 30-Oct-16 | 06-Nov-16 | 13-Dec-16 | 20-Jan-17 | 27-Feb-17 | 05-Mar-17 | 12-Apr-17 | 19-May-17 | 26-Jun-17 | 03-Jul-17 | 10-Aug-17 | 17-Sep-17 | 24-Oct-17 | 31-Nov-17 | 07-Dec-17 | 14-Jan-18 | 21-Feb-18 | 28-Mar-18 | 05-Apr-18 | 12-May-18 | 19-Jun-18 | 26-Jul-18 | 02-Aug-18 | 09-Sep-18 | 16-Oct-18 | 23-Nov-18 | 30-Dec-18 | 06-Jan-19 | 13-Feb-19 | 20-Mar-19 | 27-Apr-19 | 04-May-19 | 11-Jun-19 | 18-Jul-19 | 25-Aug-19 | 01-Sep-19 | 08-Oct-19 | 15-Nov-19 | 22-Dec-19 | 29-Jan-20 | 05-Feb-20 | 12-Mar-20 | 19-Apr-20 | 26-May-20 | 02-Jun-20 | 09-Jul-20 | 16-Aug-20 | 23-Sep-20 | 30-Oct-20 | 06-Nov-20 | 13-Dec-20 | 20-Jan-21 | 27-Feb-21 | 05-Mar-21 | 12-Apr-21 | 19-May-21 | 26-Jun-21 | 03-Jul-21 | 10-Aug-21 | 17-Sep-21 | 24-Oct-21 | 31-Nov-21 | 07-Dec-21 | 14-Jan-22 | 21-Feb-22 | 28-Mar-22 | 05-Apr-22 | 12-May-22 | 19-Jun-22 | 26-Jul-22 | 02-Aug-22 | 09-Sep-22 | 16-Oct-22 | 23-Nov-22 | 30-Dec-22 | 06-Jan-23 | 13-Feb-23 | 20-Mar-23 | 27-Apr-23 | 04-May-23 | 11-Jun-23 | 18-Jul-23 | 25-Aug-23 | 01-Sep-23 | 08-Oct-23 | 15-Nov-23 | 22-Dec-23 | 29-Jan-24 | 05-Feb-24 | 12-Mar-24 | 19-Apr-24 | 26-May-24 | 02-Jun-24 | 09-Jul-24 | 16-Aug-24 | 23-Sep-24 | 30-Oct-24 | 06-Nov-24 | 13-Dec-24 | 20-Jan-25 | 27-Feb-25 | 05-Mar-25 | 12-Apr-25 | 19-May-25 | 26-Jun-25 | 03-Jul-25 | 10-Aug-25 | 17-Sep-25 | 24-Oct-25 | 31-Nov-25 | 07-Dec-25 | 14-Jan-26 | 21-Feb-26 | 28-Mar-26 | 05-Apr-26 | 12-May-26 | 19-Jun-26 | 26-Jul-26 | 02-Aug-26 | 09-Sep-26 | 16-Oct-26 | 23-Nov-26 | 30-Dec-26 | 06-Jan-27 | 13-Feb-27 | 20-Mar-27 | 27-Apr-27 | 04-May-27 | 11-Jun-27 | 18-Jul-27 | 25-Aug-27 | 01-Sep-27 | 08-Oct-27 | 15-Nov-27 | 22-Dec-27 | 29-Jan-28 | 05-Feb-28 | 12-Mar-28 | 19-Apr-28 | 26-May-28 | 02-Jun-28 | 09-Jul-28 | 16-Aug-28 | 23-Sep-28 | 30-Oct-28 | 06-Nov-28 | 13-Dec-28 | 20-Jan-29 | 27-Feb-29 | 05-Mar-29 | 12-Apr-29 | 19-May-29 | 26-Jun-29 | 03-Jul-29 | 10-Aug-29 | 17-Sep-29 | 24-Oct-29 | 31-Nov-29 | 07-Dec-29 | 14-Jan-30 | 21-Feb-30 | 28-Mar-30 | 05-Apr-30 | 12-May-30 | 19-Jun-30 | 26-Jul-30 | 02-Aug-30 | 09-Sep-30 | 16-Oct-30 | 23-Nov-30 | 30-Dec-30 | 06-Jan-31 | 13-Feb-31 | 20-Mar-31 | 27-Apr-31 | 04-May-31 | 11-Jun-31 | 18-Jul-31 | 25-Aug-31 | 01-Sep-31 | 08-Oct-31 | 15-Nov-31 | 22-Dec-31 | 29-Jan-32 | 05-Feb-32 | 12-Mar-32 | 19-Apr-32 | 26-May-32 | 02-Jun-32 | 09-Jul-32 | 16-Aug-32 | 23-Sep-32 | 30-Oct-32 | 06-Nov-32 | 13-Dec-32 | 20-Jan-33 | 27-Feb-33 | 05-Mar-33 | 12-Apr-33 | 19-May-33 | 26-Jun-33 | 03-Jul-33 | 10-Aug-33 | 17-Sep-33 | 24-Oct-33 | 31-Nov-33 | 07-Dec-33 | 14-Jan-34 | 21-Feb-34 | 28-Mar-34 | 05-Apr-34 | 12-May-34 | 19-Jun-34 | 26-Jul-34 | 02-Aug-34 | 09-Sep-34 | 16-Oct-34 | 23-Nov-34 | 30-Dec-34 | 06-Jan-35 | 13-Feb-35 | 20-Mar-35 | 27-Apr-35 | 04-May-35 | 11-Jun-35 | 18-Jul-35 | 25-Aug-35 | 01-Sep-35 | 08-Oct-35 | 15-Nov-35 | 22-Dec-35 | 29-Jan-36 | 05-Feb-36 | 12-Mar-36 | 19-Apr-36 | 26-May-36 | 02-Jun-36 | 09-Jul-36 | 16-Aug-36 | 23-Sep-36 | 30-Oct-36 | 06-Nov-36 | 13-Dec-36 | 20-Jan-37 | 27-Feb-37 | 05-Mar-37 | 12-Apr-37 | 19-May-37 | 26-Jun-37 | 03-Jul-37 | 10-Aug-37 | 17-Sep-37 | 24-Oct-37 | 31-Nov-37 | 07-Dec-37 | 14-Jan-38 | 21-Feb-38 | 28-Mar-38 | 05-Apr-38 | 12-May-38 | 19-Jun-38 | 26-Jul-38 | 02-Aug-38 | 09-Sep-38 | 16-Oct-38 | 23-Nov-38 | 30-Dec-38 | 06-Jan-39 | 13-Feb-39 | 20-Mar-39 | 27-Apr-39 | 04-May-39 | 11-Jun-39 | 18-Jul-39 | 25-Aug-39 | 01-Sep-39 | 08-Oct-39 | 15-Nov-39 | 22-Dec-39 | 29-Jan-40 | 05-Feb-40 | 12-Mar-40 | 19-Apr-40 | 26-May-40 | 02-Jun-40 | 09-Jul-40 | 16-Aug-40 | 23-Sep-40 | 30-Oct-40 | 06-Nov-40 | 13-Dec-40 | 20-Jan-41 | 27-Feb-41 | 05-Mar-41 | 12-Apr-41 | 19-May-41 | 26-Jun-41 | 03-Jul-41 | 10-Aug-41 | 17-Sep-41 | 24-Oct-41 | 31-Nov-41 | 07-Dec-41 | 14-Jan-42 | 21-Feb-42 | 28-Mar-42 | 05-Apr-42 | 12-May-42 | 19-Jun-42 | 26-Jul-42 | 02-Aug-42 | 09-Sep-42 | 16-Oct-42 | 23-Nov-42 | 30-Dec-42 | 06-Jan-43 | 13-Feb-43 | 20-Mar-43 | 27-Apr-43 | 04-May-43 | 11-Jun-43 | 18-Jul-43 | 25-Aug-43 | 01-Sep-43 | 08-Oct-43 | 15-Nov-43 | 22-Dec-43 | 29-Jan-44 | 05-Feb-44 | 12-Mar-44 | 19-Apr-44 | 26-May-44 | 02-Jun-44 | 09-Jul-44 | 16-Aug-44 | 23-Sep-44 | 30-Oct-44 | 06-Nov-44 | 13-Dec-44 | 20-Jan-45 | 27-Feb-45 | 05-Mar-45 | 12-Apr-45 | 19-May-45 | 26-Jun-45 | 03-Jul-45 | 10-Aug-45 | 17-Sep-45 | 24-Oct-45 | 31-Nov-45 | 07-Dec-45 | 14-Jan-46 | 21-Feb-46 | 28-Mar-46 | 05-Apr-46 | 12-May-46 | 19-Jun-46 | 26-Jul-46 | 02-Aug-46 | 09-Sep-46 | 16-Oct-46 | 23-Nov-46 | 30-Dec-46 | 06-Jan-47 | 13-Feb-47 | 20-Mar-47 | 27-Apr-47 | 04-May-47 | 11-Jun-47 | 18-Jul-47 | 25-Aug-47 | 01-Sep-47 | 08-Oct-47 | 15-Nov-47 | 22-Dec-47 | 29-Jan-48 | 05-Feb-48 | 12-Mar-48 | 19-Apr-48 | 26-May-48 | 02-Jun-48 | 09-Jul-48 | 16-Aug-48 | 23-Sep-48 | 30-Oct-48 | 06-Nov-48 | 13-Dec-48 | 20-Jan-49 | 27-Feb-49 | 05-Mar-49 | 12-Apr-49 | 19-May-49 | 26-Jun-49 | 03-Jul-49 | 10-Aug-49 | 17-Sep-49 | 24-Oct-49 | 31-Nov-49 | 07-Dec-49 | 14-Jan-50 | 21-Feb-50 | 28-Mar-50 | 05-Apr-50 | 12-May-50 | 19-Jun-50 | 26-Jul-50 | 02-Aug-50 | 09-Sep-50 | 16-Oct-50 | 23-Nov-50 | 30-Dec-50 | 06-Jan-51 | 13-Feb-51 | 20-Mar-51 | 27-Apr-51 | 04-May-51 | 11-Jun-51 | 18-Jul-51 | 25-Aug-51 | 01-Sep-51 | 08-Oct-51 | 15-Nov-51 | 22-Dec-51 | 29-Jan-52 | 05-Feb-52 | 12-Mar-52 | 19-Apr-52 | 26-May-52 | 02-Jun-52 | 09-Jul-52 | 16-Aug-52 | 23-Sep-52 | 30-Oct-52 | 06-Nov-52 | 13-Dec-52 | 20-Jan-53 | 27-Feb-53 | 05-Mar-53 | 12-Apr-53 | 19-May-53 | 26-Jun-53 | 03-Jul-53 | 10-Aug-53 | 17-Sep-53 | 24-Oct-53 | 31-Nov-53 | 07-Dec-53 | 14-Jan-54 | 21-Feb-54 | 28-Mar-54 | 05-Apr-54 | 12-May-54 | 19-Jun-54 | 26-Jul-54 | 02-Aug-54 | 09-Sep-54 | 16-Oct-54 | 23-Nov-54 | 30-Dec-54 | 06-Jan-55 | 13-Feb-55 | 20-Mar-55 | 27-Apr-55 | 04-May-55 | 11-Jun-55 | 18-Jul-55 | 25-Aug-55 | 01-Sep-55 | 08-Oct-55 | 15-Nov-55 | 22-Dec-55 | 29-Jan-56 | 05-Feb-56 | 12-Mar-56 | 19-Apr-56 | 26-May-56 | 02-Jun-56 | 09-Jul-56 | 16-Aug-56 | 23-Sep-56 | 30-Oct-56 | 06-Nov-56 | 13-Dec-56 | 20-Jan-57 | 27-Feb-57 | 05-Mar-57 | 12-Apr-57 | 19-May-57 | 26-Jun-57 | 03-Jul-57 | 10-Aug-57 | 17-Sep-57 | 24-Oct-57 | 31-Nov-57 | 07-Dec-57 | 14-Jan-58 | 21-Feb-58 | 28-Mar-58 | 05-Apr-58 | 12-May-58 | 19-Jun-58 | 26-Jul-58 | 02-Aug-58 | 09-Sep-58 | 16-Oct-58 | 23-Nov-58 | 30-Dec-58 | 06-Jan-59 | 13-Feb-59 | 20-Mar-59 | 27-Apr-59 | 04-May-59 | 11-Jun-59 | 18-Jul-59 | 25-Aug-59 | 01-Sep-59 | 08-Oct-59 | 15-Nov-59 | 22-Dec-59 | 29-Jan-60 | 05-Feb-60 | 12-Mar-60 | 19-Apr-60 | 26-May-60 | 02-Jun-60 | 09-Jul-60 | 16-Aug-60 | 23-Sep-60 | 30-Oct-60 | 06-Nov-60 | 13-Dec-60 | 20-Jan-61 | 27-Feb-61 | 05-Mar-61 | 12-Apr-61 | 19-May-61 | 26-Jun-61 | 03-Jul-61 | 10-Aug-61 | 17-Sep-61 | 24-Oct-61 | 31-Nov-61 | 07-Dec-61 | 14-Jan-62 | 21-Feb-62 | 28-Mar-62 | 05-Apr-62 | 12-May-62 | 19-Jun-62 | 26-Jul-62 | 02-Aug-62 | 09-Sep-62 | 16-Oct-62 | 23-Nov-62 | 30-Dec-62 | 06-Jan-63 | 13-Feb-63 | 20-Mar-63 | 27-Apr-63 | 04-May-63 | 11-Jun-63 | 18-Jul-63 | 25-Aug-63 | 01-Sep-63 | 08-Oct-63 | 15-Nov-63 | 22-Dec-63 | 29-Jan-64 | 05-Feb-64 | 12-Mar-64 | 19-Apr-64 | 26-May-64 | 02-Jun-64 | 09-Jul-64 | 16-Aug-64 | 23-Sep-64 | 30-Oct-64 | 06-Nov-64 | 13-Dec-64 | 20-Jan-65 | 27-Feb-65 | 05-Mar-65 | 12-Apr-65 | 19-May-65 | 26-Jun-65 | 03-Jul-65 | 10-Aug-65 | 17-Sep-65 | 24-Oct-65 | 31-Nov-65 | 07-Dec-65 | 14-Jan-66 | 21-Feb-66 | 28-Mar-66 | 05-Apr-66 | 12-May-66 | 19-Jun-66 | 26-Jul-66 | 02-Aug-66 | 09-Sep-66 | 16-Oct-66 | 23-Nov-66 | 30-Dec-66 | 06-Jan-67 | 13-Feb-67 | 20-Mar-67 | 27-Apr-67 | 04-May-67 | 11-Jun-67 | 18-Jul-67 | 25-Aug-67 | 01-Sep-67 | 08-Oct-67 | 15-Nov-67 | 22-Dec-67 | 29-Jan-68 | 05-Feb-68 | 12-Mar-68 | 19-Apr-68 | 26-May-68 | 02-Jun-68 | 09-Jul-68 | 16-Aug-68 | 23-Sep-68 | 30-Oct-68 | 06-Nov-68 | 13-Dec-68 | 20-Jan-69 | 27-Feb-69 | 05-Mar-69 | 12-Apr-69 | 19-May-69 | 26-Jun-69 | 03-Jul-69 | 10-Aug-69 | 17-Sep-69 | 24-Oct-69 | 31-Nov-69 | 07-Dec-69 | 14-Jan-70 | 21-Feb-70 | 28-Mar-70 | 05-Apr-70 | 12-May-70 | 19-Jun-70 | 26-Jul-70 | 02-Aug-70 | 09-Sep-70 | 16-Oct-70 | 23-Nov-70 | 30-Dec-70 | 06-Jan-71 | 13-Feb-71 | 20-Mar-71 | 27-Apr-71 | 04-May-71 | 11-Jun-71 | 18-Jul-71 | 25-Aug-71 | 01-Sep-71 | 08-Oct-71 | 15-Nov-71 | 22-Dec-71 | 29-Jan-72 | 05-Feb-72 | 12-Mar-72 | 19-Apr-72 | 26-May-72 | 02-Jun-72 | 09-Jul-72 | 16-Aug-72 | 23-Sep-72 | 30-Oct-72 | 06-Nov-72 | 13-Dec-72 | 20-Jan-73 | 27-Feb-73 | 05-Mar-73 | 12-Apr-73 | 19-May-73 | 26-Jun-73 | 03-Jul-73 | 10-Aug-73 | 17-Sep-73 | 24-Oct-73 | 31-Nov-73 | 07-Dec-73 | 14-Jan-74 | 21-Feb-74 | 28-Mar-74 | 05-Apr-74 | 12-May-74 | 19-Jun-74 | 26-Jul-74 | 02-Aug-74 | 09-Sep-74 | 16-Oct-74 | 23-Nov-74 | 30-Dec-74 | 06-Jan-75 | 13-Feb-75 | 20-Mar-75 | 27-Apr-75 | 04-May-75 | 11-Jun-75 | 18-Jul-75 | 25-Aug-75 | 01-Sep-75 | 08-Oct-75 | 15-Nov-75 | 22-Dec-75 | 29-Jan-76 | 05-Feb-76 | 12-Mar-76 | 19-Apr-76 | 26-May-76 | 02-Jun-76 | 09-Jul-76 | 16-Aug-76 | 23-Sep-76 | 30-Oct-76 | 06-Nov-76 | 13-Dec-76 | 20-Jan-77 | 27-Feb-77 | 05-Mar-77 | 12-Apr-77 | 19-May-77 | 26-Jun-77 | 03-Jul-77 | 10-Aug-77 | 17-Sep-77 | 24-Oct-77 | 31-Nov-77 | 07-Dec-77 | 14-Jan-78 | 21-Feb-78 | 28-Mar-78 | 05-Apr-78 | 12-May-78 | 19-Jun-78 | 26-Jul-78 | 02-Aug-78 | 09-Sep-78 | 16-Oct-78 | 23-Nov-78 | 30-Dec-78 | 06-Jan-79 | 13-Feb-79 | 20-Mar-79 | 27-Apr-79 | 04-May-79 | 11-Jun-79 | 18-Jul-79 | 25-Aug-79 | 01-Sep-79 | 08-Oct-79 | 15-Nov-79 | 22-Dec-79 | 29-Jan-80 | 05-Feb-80 | 12-Mar-80 | 19-Apr-80 | 26-May-80 | 02-Jun-80 | 09-Jul-80 | 16-Aug-80 | 23-Sep-80 | 30-Oct-80 | 06-Nov-80 | 13-Dec-80 | 20-Jan-81 | 27-Feb-81 | 05-Mar-81 | 12-Apr-81 | 19-May-81 | 26-Jun-81 | 03-Jul-81 | 10-Aug-81 | 17-Sep-81 | 24-Oct-81 | 31-Nov-81 | 07-Dec-81 | 14-Jan-82 | 21-Feb-82 | 28-Mar-82 | 05-Apr-82 | 12-May-82 | 19-Jun-82 | 26-Jul-82 | 02-Aug-82 | 09-Sep-82 | 16-Oct-82 | 23-Nov-82 | 30-Dec-82 | 06-Jan-83 | 13-Feb-83 | 20-Mar-83 | 27-Apr-83 | 04-May-83 | 11-Jun-83 | 18-Jul-83 | 25-Aug-83 | 01-Sep-83 | 08-Oct-83 | 15-Nov-83 | 22-Dec-83 | 29-Jan-84 | 05-Feb-84 | 12-Mar-84 | 19-Apr-84 | 26-May-84 | 02-Jun-84 | 09-Jul-84 | 16-Aug-84 | 23-Sep-84 | 30-Oct-84 | 06-Nov-84 | 13-Dec-84 | 20-Jan-85 | 27-Feb-85 | 05-Mar-85 | 12-Apr-85 | 19-May-85 | 26-Jun-85 | 03-Jul-85 | 10-Aug-85 | 17-Sep-85 | 24-Oct-85 | 31-Nov-85 | 07-Dec-85 | 14-Jan-86 | 21-Feb-86 | 28-Mar-86 | 05-Apr-86 | 12-May-86 | 19-Jun-86 | 26-Jul-86 | 02-Aug-86 | 09-Sep-86 | 16-Oct-86 | 23-Nov-86 | 30-Dec-86 | 06-Jan-87 | 13-Feb-87 | 20-Mar-87 | 27-Apr-87 | 04-May-87 | 11-Jun-87 | 18-Jul-87 | 25-Aug-87 | 01-Sep-87 | 08-Oct-87 | 15-Nov-87 | 22-Dec-87 | 29-Jan-88 | 05-Feb-88 | 12-Mar-88 | 19-Apr-88 | 26-May-88 | 02-Jun-88 | 09-Jul-88 | 16-Aug-88 | 23-Sep-88 | 30-Oct-88 | 06-Nov-88 | 13-Dec-88 | 20-Jan-89 | 27-Feb-89 | 05-Mar-89 | 12-Apr-89 | 19-May-89 | 26-Jun-89 | 03-Jul-89 | 10-Aug-89 | 17-Sep-89 | 24-Oct-89 | 31-Nov-89 | 07-Dec-89 | 14-Jan-90 | 21-Feb-90 | 28-Mar-90 | 05-Apr-90 | 12-May-90 | 19-Jun-90 | 26-Jul-90 | 02-Aug-90 | 09-Sep-90 | 16-Oct-90 | 23-Nov-90 | 30-Dec |
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Appendix B-8
HUMIDITY CELL RESULTS FOR CNT CHD 1-7 (TWB)
Tailings Material

S-Total: 0.23 %
S²⁻: 0.20 %
NFI: 20.80 t CaCO₃/1000 t
CaMP: 12.10 t CaCO₃/1000 t
AP: 6.30 t CaCO₃/1000 t
Weight: 1000 g

| Weeks Date | # | CCME Guideline * | MMER Guideline ** | 24-Apr-07 | 01-May-07 | 08-May-07 | 15-May-07 | 22-May-07 | 29-May-07 | 05-Jun-07 | 12-Jun-07 | 19-Jun-07 | 26-Jun-07 | 03-Jul-07 |
|---------------------------------------|---------------------------|------------------|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| Leachate | ml | | | 770 | 952 | 884 | 922 | 886 | 888 | 885 | 850 | 817 | 888 | 889 |
| pH | | | | 6.34 | 7.79 | 7.03 | 7.4 | 7.11 | 7.15 | 7.2 | 7.26 | 7.21 | 7.25 | 7.17 |
| Conductivity | µS/cm | | | 41 | 121 | 81 | 91 | 79 | 77 | 100 | 106 | 86 | 90 | 83 |
| Alkalinity | mg/L as CaCO ₃ | 6.0 - 9.5 | | <2 | 13 | 10 | 9 | <2 | 6 | <2 | <2 | <2 | <2 | <2 |
| Acidity | mg/L as CaCO ₃ | | | 7 | <2 | <2 | <2 | <2 | <2 | <2 | <2 | <2 | <2 | <2 |
| Sulphate (SO ₄) | mg/L | | | 51 | 30 | 19 | 24 | 21 | 23 | 27 | 30 | 26 | 25 | 26 |
| Calcium (Ca) | mg/L | | | 10.1 | 6.78 | 4.81 | 4.84 | 4.26 | 4.58 | 5.32 | 6.53 | 6.03 | 5.89 | 6.05 |
| Iron (Fe) | mg/L | 0.3 | | 0.02 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 |
| NH ₃ -NH ₄ as N | mg/L | | | 0.6 | 1.6 | 0.8 | 0.6 | 0.3 | 0.3 | | | | | |
| NO ₂ as N | mg/L | | | 0.16 | <0.05 | <0.05 | <0.05 | 0.12 | 0.07 | | | | | |
| Mercury (Hg) | mg/L | | | <0.0001 | <0.0001 | <0.0001 | <0.0001 | | <0.0001 | | | | | |
| Silver (Ag) | mg/L | 0.001 | | <0.0003 | <0.0003 | <0.0003 | | | <0.0003 | | | | | |
| Aluminum (Al) | mg/L | 0.1 | | 0.59 | 0.4 | 0.4 | | | 0.3 | | | | | |
| Arsenic (As) | mg/L | 0.005 | | 0.0673 | 0.0267 | 0.019 | | | 0.0094 | | | | | |
| Barium (Ba) | mg/L | | | 0.00093 | 0.00071 | 0.00045 | | | 0.00045 | | | | | |
| Beryllium (Be) | mg/L | | | <0.00004 | <0.00004 | <0.00004 | | | <0.00004 | | | | | |
| Boron (B) | mg/L | | | 0.006 | 0.022 | 0.001 | | | 0.002 | | | | | |
| Bismuth (Bi) | mg/L | | | <0.00002 | <0.00002 | <0.00002 | | | <0.00002 | | | | | |
| Cadmium (Cd) | mg/L | 0.00017 | | 0.00914 | 0.00499 | 0.00327 | | | 0.00266 | | | | | |
| Cobalt (Co) | mg/L | | | <0.00003 | <0.00003 | <0.00003 | | | <0.00003 | | | | | |
| Chromium (Cr) | mg/L | 0.0089 | | 0.0039 | 0.0023 | 0.002 | | | 0.0019 | | | | | |
| Copper (Cu) | mg/L | 0.002 | 0.6 | 2.66 | 1.59 | 0.99 | | | 1.01 | | | | | |
| Potassium (K) | mg/L | | | 0.0016 | 0.0016 | 0.0011 | | | 0.0015 | | | | | |
| Lithium (Li) | mg/L | | | 0.532 | 0.583 | 0.4 | | | 0.385 | | | | | |
| Magnesium (Mg) | mg/L | | | 0.017 | 0.0305 | 0.0276 | | | 0.022 | | | | | |
| Manganese (Mn) | mg/L | | | 0.00284 | 0.00152 | 0.00143 | | | 0.001 | | | | | |
| Molybdenum (Mo) | mg/L | 0.073 | | | | | | | | | | | | |
| Sodium (Na) | mg/L | | | 22.8 | 13 | 7.81 | | | 8.34 | | | | | |
| Nickel (Ni) | mg/L | 0.025 | | <0.0007 | <0.0007 | <0.0007 | | | <0.0007 | | | | | |
| Lead (Pb) | mg/L | 0.001 | 0.4 | 0.00033 | <0.0002 | 0.0004 | | | 0.00038 | | | | | |
| Phosphorus (P) | mg/L | | | 0.01 | 0.01 | 0.01 | | | 0.01 | | | | | |
| Antimony (Sb) | mg/L | | | 0.0258 | 0.0014 | 0.0012 | | | 0.0011 | | | | | |
| Selenium (Se) | mg/L | | | <0.001 | <0.001 | <0.001 | | | <0.001 | | | | | |
| Strontium (Sr) | mg/L | 0.001 | | 0.0022 | 0.001 | 0.001 | | | <0.0003 | | | | | |
| Thallium (Tl) | mg/L | | | 0.0216 | 0.0152 | 0.0106 | | | 0.0117 | | | | | |
| Titanium (Ti) | mg/L | | | 0.0003 | 0.0002 | 0.0004 | | | 0.0002 | | | | | |
| Vanadium (V) | mg/L | | | <0.0001 | <0.0001 | <0.0001 | | | <0.0001 | | | | | |
| Uranium (U) | mg/L | | | 0.00011 | 0.0001 | 0.00005 | | | 0.00003 | | | | | |
| Zinc (Zn) | mg/L | 0.03 | | 0.00229 | 0.00113 | 0.00072 | | | 0.00067 | | | | | |
| | mg/L | | | <0.000005 | <0.000005 | 0.000005 | | | <0.000005 | | | | | |
| | mg/L | | | 0.0004 | 0.001 | 0.0005 | | | 0.0002 | | | | | |

* - Canadian Water Quality Guidelines for the Protection of Aquatic Life, Canadian Council of Environmental Ministers (CCME), Canadian Environmental Quality Guidelines, 1999.

** - Federal Canadian Metal Mining Effluent Regulations, Canada Gazette Part II, 2002.

Value is above CCME Guidelines

Value is above MMER Guidelines